

**ПРИЛОЖЕНИЕ № 5 –  
Приложения към приложение № 2**

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за участие в открита процедура за възлагане на обществена поръчка с предмет:

„Подмяна на маслонапълнена кабелна електропроводна линия 110 kV „Зенит“ от линеен ножов разединител 110 kV на ПС „Хаджи Димитър“ до линеен ножов разединител 110 kV в ПС „Подуяне“, реф. № РРС 17 – 169



## Техническо предложение



### Техническа документация

Приложение № 1 към Предложение за изпълнение на поръчката по т.15.1. от Техническото предложение – Заверени копия на документи за Ограничител на пренапрежение (вентилен отвод) за нова КЕЛ 110 kV:

- Приложение № 1.1. към т.15.1.1. от Техническото предложение – Заверено/и копие/я на протокол/и от типови изпитвания, проведени от независима изпитвателна лаборатория, с приложен списък на отделните изпитвания на български език

000118

# ABB Power Technology Products

Författare - Author

Lennart Stenström *LS*  
Godkännare - Approved by

Gunnar Persson *GP*

Uppdragsgivare - Requested by

Titel - Title

Moisture ingress test on surge  
arresters PEXLIM P120-XH145

## Rapport Report

Från - From  
PTHVP/AKB

Datum - Date  
2001-12-20

R HVP/AK 01-06 rev.1

Reg.

Sida - Page

1(3)

Ordernr - Ref. No.

Debiteras ordernr - Debit Order No.

PkUAK

Antal textsidor - No. of text pages

3

Antal bilagesidor - No. of supplm. pages

4

Utredning teoretisk  
undersökning - Analysis,  
theoretical investigation

Provnig, experim. under-  
sökning - Test experi-  
mental investigation

Delrapport  
Partial report

Slutrapport  
Final report

Provnig/undersökning avslutad  
Test/investigation finished  
01-11-19

Sammanfattning - Summary

### TEST METHOD

Moisture ingress test in accordance with IEC 60099-4, Amendment 2 of 2001-10, Clause 9.7.9 (Same requirements as per earlier IEC Committee Draft for Vote 37/231/CDV, Clause 9.7.8)

### TEST OBJECT

Surge arresters PEXLIM P120-XH145 according to dimension drawing 1HSA303 000-CA (enclosed)

### TEST PROCEDURE

Initial measurements of power losses, residual voltage and partial discharge level according to Clause 9.7.9.1 as well as check of reference voltage.

Preconditioning according to Clause 9.7.9.2

Water immersion according to Clause 9.7.9.3

Verification tests including visual inspection, measurements of power losses, residual voltage and partial discharges according to Clause 9.7.9.4 as well as check of reference voltage.

### TEST RESULT

The surge arresters passed the test successfully.

*LS*  
Ludvika 2001-12-20

ABB Power Technology Products AB  
High Voltage Products/Surge Arresters  
Quality Department

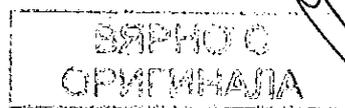
на основании чл. 2 от 33ЛД

Kurt Jansson



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**1. TEST METHOD**

Moisture ingress test in accordance IEC 60099-4, Amendment 2 of 2001-10, Clause 9.7.9 (Same requirements as per earlier IEC Committee Draft for Vote 37/231/CDV, Clause 9.7.8)

**2. TEST OBJECT**

Two surge arresters PEXLIM P120-XH145 serial No. P-X16 and P-X17 according to dimension drawing 1HSA303 000-CA (enclosed)

**3. TEST PROCEDURE**

**3.1**

Initial measurements of power losses, residual voltage and partial discharge level (PD) according to Clause 9.7.9.1 as well as check of reference voltage with results as follows:

Test object	P-X16	P-X17	
Reference voltage-kVrms	129.6	129.4	at 3 mA resistive current
Residual voltage-kVpeak	254.8	254.9	at 3 kApeak
PD level-pC	0.3	0.4	at 108 kVrms
Power losses-W	4.1	4.1	at 92 kVrms

**3.2**

Preconditioning according to Clause 9.7.9.2

(Performed by ABB Power Technology Products, Dept. ASS/SPL. See enclosed test report SPL 01-226)

Bending moment 2500 Nm

Load direction no. 1 for 24 hours in +60 °C

Load direction no. 2 for 24 hours in -25 °C

Load direction no. 3 for 24 hours in +45 °C

Load direction no. 4 for 24 hours in -40 °C

**3.3**

Water immersion according to Clause 9.7.9.3

(Performed by ABB Power Technology Products, Dept. ASS/SPL. See enclosed test report SPL 01-226)

Immersion in boiling water with 1 g NaCl per liter for 42 h from 01-11-16 to 01-11-18. Thereafter the arrester remained in the water, which was cooled down to 50 °C, until 8 o'clock in the morning of 01-11-19.

3.4

Verification tests including visual inspection, measurements of power losses, residual voltage and partial discharges according to Clause 9.7.9.4 as well as check of reference voltage.

Test object	P-X16	P-X17	
Reference voltage-kVrms	129.1	129.0	at 3 mA resistive current
Residual voltage-kVpeak	254.3	254.1	at 3 kApeak
PD level-pC	0.4	0.5	at 108 kVrms
Power losses-W	4.0	4.0	at 92 kVrms

Verification tests were finished 01-11-19 at 3 o'clock p.m. within 8 hours after the arresters were taken out of the water at 50 °C.

4. TEST RESULTS

The surge arresters passed the test successfully.

The permanent deflection after the thermomechanical conditioning was 3 mm in load direction no. 1 for P-X16 and 1 mm for P-X17

(See enclosed test report SPL 01-226)

Deviation in electrical data before and after the test:

P-X16

	<u>Before</u>	<u>After</u>	<u>Deviation</u>
Reference voltage	129.6 kVrms	129.1 kVrms	-0.4 %
Residual voltage	254.8 kVpeak	254.3 kVpeak	-0.2 %
PD level	0.3 pC	0.4 pC	+0.1 pC
Power losses	4.1 W	4.0 W	-2.4 %

P-X17

	<u>Before</u>	<u>After</u>	<u>Deviation</u>
Reference voltage	129.4 kVrms	129.0kVrms	-0.3 %
Residual voltage	254.9 kVpeak	254.1 kVpeak	-0.3 %
PD level	0.4 pC	0.5pC	+0.1pC
Power losses	4.1 W	4.0 W	-2.4 %

Report

R SPL 01-226

Author  
M.Lausch  
Approved by  
H.Persson  
Requested by  
PTHVP/AKK

From  
PTASS/SPL  
Date  
01-12-03  
Test performed by  
T.Lillqvist

Reg  
5680  
Page  
1  
Ref.No.  
L.15151814  
Project account

Title  
Conditioning for moisture ingress test on  
surge arrester units type PEXLIM P120-XH145.  
Serial number P-X16 and P-X17.

Interim Report  
 Final Report

Pkl/Akl  
No. of pages of text  
2  
No. of appendix  
1

Analysis/test finished  
01-11-18

Summary

**PURPOSE** Thermomechanical preconditioning and water immersion of surge arrester units prior to moisture ingress test.

**TEST OBJECTS**

Two surge arrester units type PEXLIM P120-XH145 with serial number P-X16 and P-X17.

**TEST PROCEDURE**

Test procedure according to IEC Committee Draft for Vote 37/231/CDV, clause 9.7.8.2 precondition and 9.7.8.3 water immersion test.

**Terminal torque preconditioning, clause 9.7.8.2.1.**

The terminal was subjected to a torque of 100 Nm during 30 s.

**Thermomechanical preconditioning, clause 9.7.8.2.2.**

The test object was subjected to a bending moment of 2 500 Nm in four perpendicular directions at different ambient temperatures. The bending direction was changed at +20°C.

Load direction no.	Temperature °C
1	+60
2	-25
3	+45
4	-40

Each load direction was tested 24 hours.

Distribution  
SPL-arkiv, PTHVP/AKK, Roger Siljeholm

Page 1 only  
SPL-arkiv,

Keywords  
Conditioning  
Surge arrester units type PEXLIM P-X

Other references

File  
 1 year  
 2 year  
 > 3 years

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ВЕРНО С  
ОРИГИНАЛА



The temperatures during the test are shown in appendix 1.

The permanent deflection in load direction number 1 was measured.

Water immersion test, clause 9.7.8.3.

The test object was immersed in boiling deionized water with 1 g/l of NaCl for 42 hours.

The test was finished at 17.00, 2001-11-18. Thereafter the surge arresters remained in the water, which was cooled down to 50 °C, until 8.00, 2001-11-19.

**TEST RESULTS**

There was no visual damage on the test objects.

After the thermomechanical test, the permanent deflection in load direction number 1 was 3 mm on P-X16 and 1 mm on P-X17.

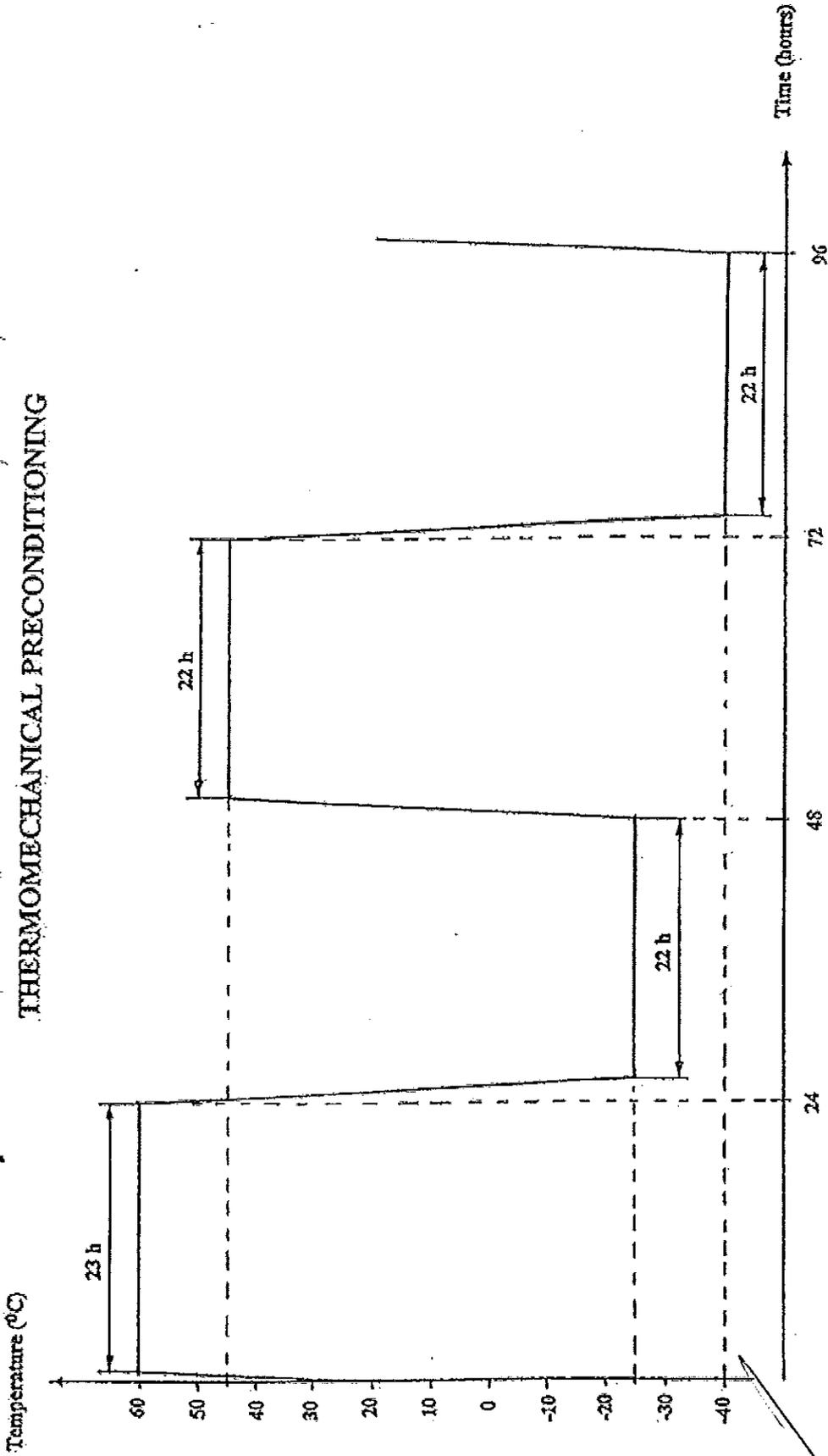
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SPL01-226  
Appendix 1

THERMOMECHANICAL PRECONDITIONING



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ВЕРНО С  
ОРИГИНАЛОМ



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1 2 3 4 5 6

# Surge arrester type PEXLIM P-X

System voltage range 12 - 170 kV

Rated voltage kV	System voltage kV	A mm	B mm	C mm	D mm	Creepage distance mm	Mass kg	fig.
012-018	XV 012	481				1363	19	1
021-024	XV 024	481				1363	18	1
030-036	XV 036	481				1363	18	1
039		736				2270	29	1
042-072	XV 052	736				2270	29	1
054-072	XV 072	736				2270	28	1
075-084		1080				3625	43	
075-096	XV 100	1080				3625	43	1
090-120	XH	1080				3625	42	1
090-144	XV 123	1397				4540	53	
150		1486				4988	54	2
108-120	XH	1080				3625	41	1
108-144		1397				4540	52	
150	XV 145	1486				4988	54	2
162-168		1741				5895	65	
132-144	XH 170	1417				4540	52	
150		1506	400		160	4988	56	3
132-192	XV	1761				5895	69	

## DRILLING PLAN

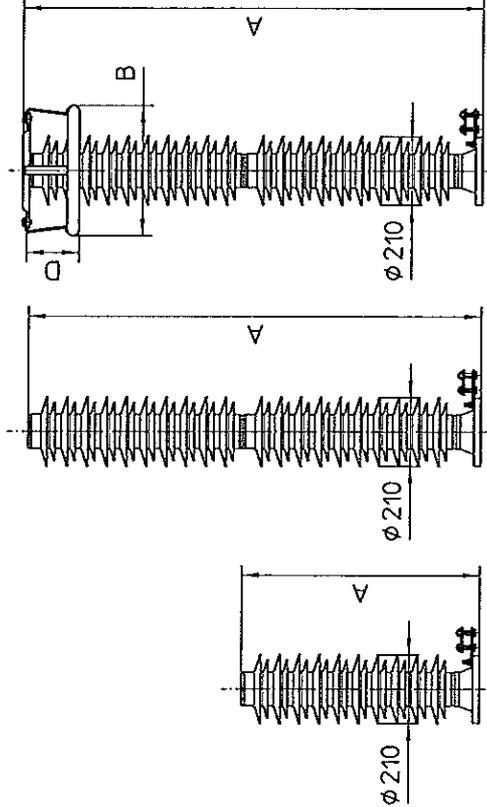
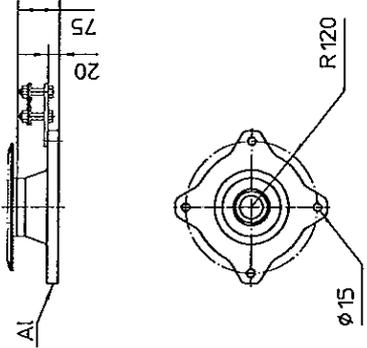


fig. 1

fig. 2

fig. 3

1) Including line terminal, earth terminal and grading ring arrangement.

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ОРИГИНАЛ



Prepared J. Dahlbom	Responsible department PTHVP/AKK	Title DIMENSION DRAWING
Approved R. Siljeholm	Task, sub department PTHVP/AF	SURGE ARRESTER
Revision		
ABB Power Technology Products		Document no. 1HSA303 000-CA
		Cont. -

Accessories on drawing 1HSA301 000-D  
Surge counter on drawing 1HSA440 000-A  
Surge arrester monitor on drawing 1HSA440 000-B

1 2 3 4 5 6

**ABB Power Technology Products AB**

**Rapport  
Report**

**R HVP/AK 01-07**

Författare - Author

Roger Silieholm  
Godkännare - Approved by

Iennart Stenstrom

Uppdragsgivare - Requested by

Gunnar Persson

Titel - Title

Bending fatigue test on surge arrester type

PEXLIM P120-XH145

Från - From

HVP/AK

Datum - Date

2001-12-10

Reg.

Sida - Page

1

Utredning teoretisk undersökning - Analysis, theoretical investigation

Proving, experim. undersökning - Test experimental investigation

Delrapport Partial report

Slutrapport Final report

Proving/undersökning avslutad  
Test/investigation finished

Ordernr - Ref. No.

Debiteras ordernr - Debit Order No.

Pkt/Akt

Antal textsidor - No. of text pages

1

Antal bilagesidor - No. of supplm. pages

4

**PURPOSE**

The purpose was to verify the bending fatigue strength of the arrester type PEXLIM P-X.

**TEST OBJECT**

Two arresters of type PEXLIM P120-XH145 with rated voltage 120 kV, serial numbers P-X22 and P-X24 were tested. The arresters comprise the longest mechanical sections used for the arrester type PEXLIM P-X.

**TEST PERFORMED**

The modules were subjected to a cyclic bending test consisting of 1000 cycles at a bending moment level of 2500 Nm at the frequency 0.3 Hz. See report SPL 01-218.

**RESULT**

The test objects withstood the test without any damage. See report SPL 01-218.

Before and after the mechanical test the modules were electrically routine tested, result as per Table 1. No significant changes in the electrical characteristics were observed.

Arrester	Reference Voltage (Uref) at 3 mA resistive current		Partial discharge level at 0.9*Uref		Power losses at 0.8*Uref	
	Before test kV	After test kV	Before test pC	After test pC	Before test W	After test W
P-X22	129.5	129.2	<5	<5	4.2	4.0
P-X24	128.9	128.8	<5	<5	4.4	4.2

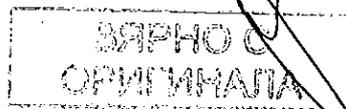
Table 1. Electrical routine tests.

Ludvika 2001-12-10

ABB Power Technology Products AB  
High Voltage Products/Surge Arresters  
Quality Department

на основании чл. 2 от 33ЛД

Kurt Jansson



000126

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# ABB Power Technology Products AB

## Report

**R SPL 01-218**

Author  
M.Lausch  
Approved by  
H.Persson  
Requested by  
PTHVP/AKK  
Title

From  
SEASS/SPL  
Test performed by  
T.Lillqvist

Date  
01-12-03  
Reg.  
5680  
Ref. No.  
L-15151814  
Project account

Page  
1

Bending fatigue test of surge arrester units  
type PEXLIM P120-XH145

Interim report

Pkl/Akl

Final report

No. of pages of text

Analysis/test finished  
01-11-16

1  
No. of appendix  
4

### Summary

### PURPOSE

To test the ability of PEXLIM P120-XH145 modules to withstand 1 000 cycles at a load of 2 500 Nm, with a frequency of 0,3 Hz.

### TEST OBJECTS

Two PEXLIM P120-XH145 modules with serial number P-X22 and P-X24, see drawing appendix 1.

### TEST PROCEDURE

The PEXLIM modules were mounted in a universal-testing machine. The load was applied by a hydraulic cylinder connected to the top of the module (see appendix 2). The horizontal displacement at a height of 1 100 mm was registered by a position transducer connected to a strip chart recorder. The module was subjected to an alternating bending load of 2 500 Nm, referred to the foundation, at the frequency of 0,3 Hz.

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### TEST RESULTS

The PEXLIM modules withstood 1 000 cycles of 2 500 Nm at 0,3 Hz without visible damage.

The measurement of the horizontal displacements is shown in appendix 3.

Distribution  
SPL-arkiv, PTHVP/AKK

Page 1 only  
SPL-arkiv,

Keywords  
Bending fatigue test  
Surge arrester units

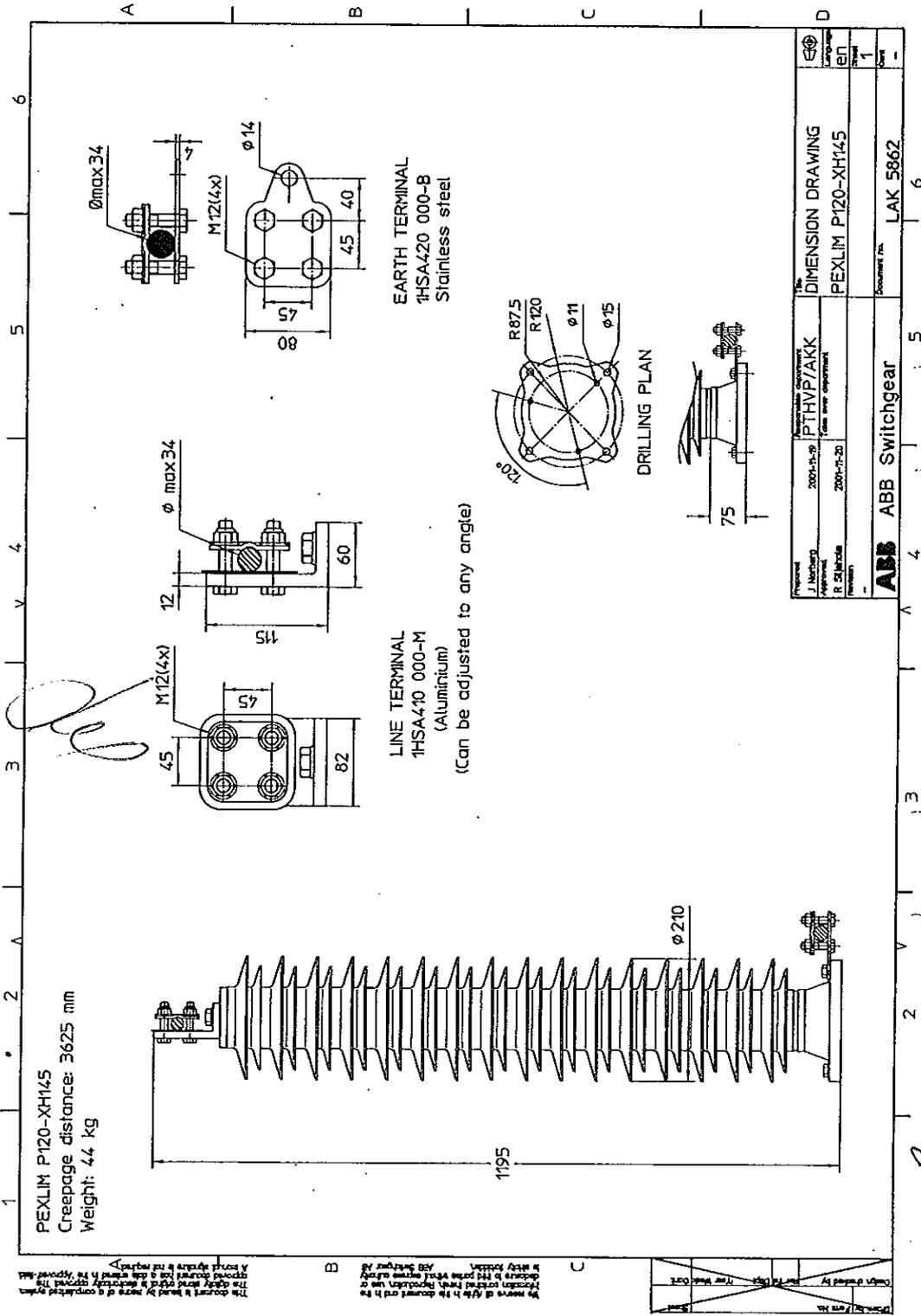
Other references

File  
 1 year  
 2 years  
 > 3 years

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ВАРНО  
ОРИГИНАЛ





PEXLIM P120-XH145  
Creepage distance: 3625 mm  
Weight: 44 kg

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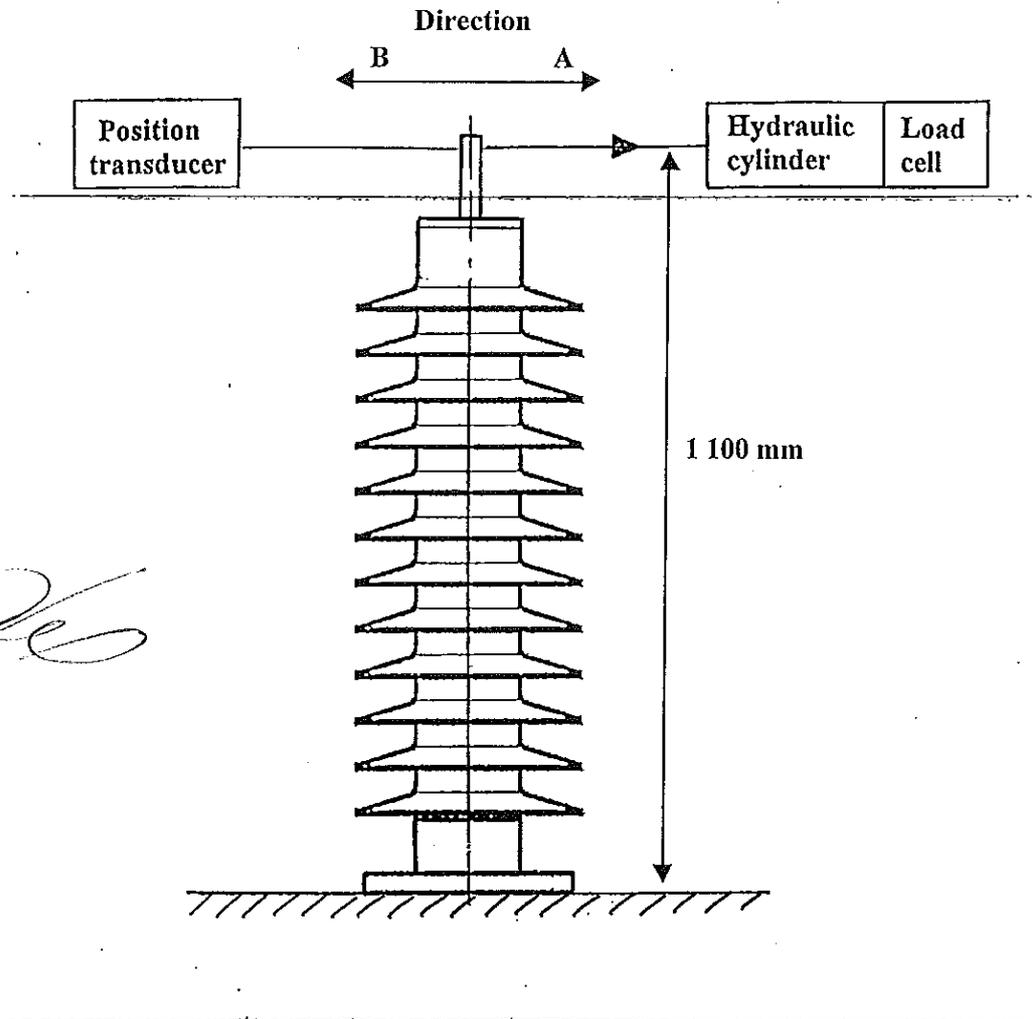
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ОРИГИНАЛА



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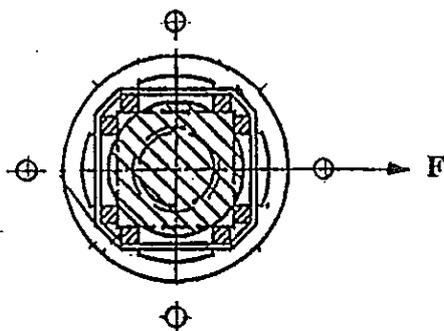
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**BENDING DIRECTION.**



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~~ВЯРНО С  
ОРИГИНАЛА~~



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P-X22

Bending moment (Nm)	Number of cycles	Displacement dir. A (mm)	Displacement dir. B (mm)
2 500	0	26,3	25,8
2 500	50	26,8	26,1
2 500	100	26,9	26,2
2 500	200	27,0	26,3
2 500	300	27,0	26,3
2 500	400	27,0	26,5
2 500	500	27,0	26,8
2 500	600	27,0	27,0
2 500	700	27,0	27,0
2 500	800	27,1	27,1
2 500	900	27,3	27,2
2 500	1 000	27,7	27,3

P-X24

Bending moment (Nm)	Number of cycles	Displacement dir. A (mm)	Displacement dir. B (mm)
2 500	0	25,9	29,2
2 500	50	26,3	30,0
2 500	100	26,5	30,1
2 500	200	26,9	30,2
2 500	300	27,0	30,8
2 500	400	27,0	30,9
2 500	500	27,0	30,9
2 500	600	27,2	31,0
2 500	700	27,4	31,0
2 500	800	27,5	31,0
2 500	900	27,8	31,3
2 500	1 000	28,0	31,3

000130

БЯРНО С  
ОРИГИНАЛА



# ABB Power Technology Products AB

Författare - Author

Roger Silieholm  
Godkännare - Approved by

I ennart Stenstrom

Uppdragsgivare - Requested by

Gunnar Persson

Titel - Title

Bending strength test on surge arrester type  
PEXLIM P120-XH145

## Rapport Report

Från - From

HVP/AK

Datum - Date

2001-12-10

Reg.

Sida - Page

1

R HVP/AK 01-09

Ordernr - Ref. No.

Debiteras ordernr - Debit Order No.

Pk/Ak

Antal textsidor - No. of text pages

1

Antal bilagesidor - No. of supplem. pages

5

Utredning teoretisk  
undersökning - Analysis,  
theoretical investigation

Proving, experim. under-  
sökning - Test experi-  
mental investigation

Delrapport  
Partial report

Slutrapport  
Final report

Proving/undersökning avslutad  
Test/investigation finished

### PURPOSE

The purpose was to verify a bending strength of 4000 Nm of the arrester type PEXLIM P-X.

### TEST OBJECT

Two arresters of type PEXLIM P120-XH145 with rated voltage 120 kV, serial numbers P-X28 and P-X29 were tested. The arresters comprise the longest mechanical sections used for the arrester type PEXLIM P-X.

### TEST PERFORMED

The arresters were loaded until failure with rate of 2500 Nm/min. The deflection was measured during the test. See report SPL 01-220.

### RESULT

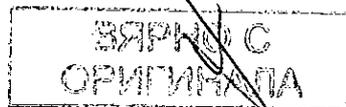
The two arresters failed at 6020 Nm and 5870 Nm respectively. See report SPL 01-220.

Ludvika 2001-12-10

ABB Power Technology Products AB  
High Voltage Products/Surge Arresters  
Quality Department

на основании чл. 2 от 33ЛД

Kurt Jansson



000131

# ABB Power Technology Products AB

## Report

**R SPL 01-220**

Author  
M.Lausch  
Approved by  
H.Persson  
Requested by  
PTHVP/AKK

From SEASS/SPL  
Date 01-12-03  
Test performed by  
T.Lillqvist

Reg. 5680  
Page 1  
Ref. No. L-15151814  
Project account

Title  
Bending strength test of surge arrester units  
type PEXLIM P120-XH145

Interim report

Pkl/Akl

Final report

No. of pages of text

Analysis/test finished  
01-11-16

1  
No. of appendix  
4

### Summary

### PURPOSE

To determine the bending strength of PEXLIM P120-XH145 arresters.

### TEST OBJECTS

Two PEXLIM P120-XH145 arresters with serial number P-X28 and P-X29, see drawing appendix 1.

### TEST PROCEDURE

The PEXLIM arresters were mounted in a universal-testing and loaded until break with a loading rate of 2 500 Nm/min machine (see appendix 2).

The deflection, at a height of 1 100 mm from the foundation, was registered by a position transducer connected to a strip chart recorder.

### TEST RESULTS

Test object	Bending strength (kNm)	Deflection at break (mm)	Load/deflection
P-X28	6,02	108,5	Appendix 3
P-X29	5,87	110,4	Appendix 4

### Distribution

SPL-arkiv, PTHVP/AKK

### Page 1 only

SPL-arkiv,

### Keywords

Bending strength test  
Surge arrester units

### Other references

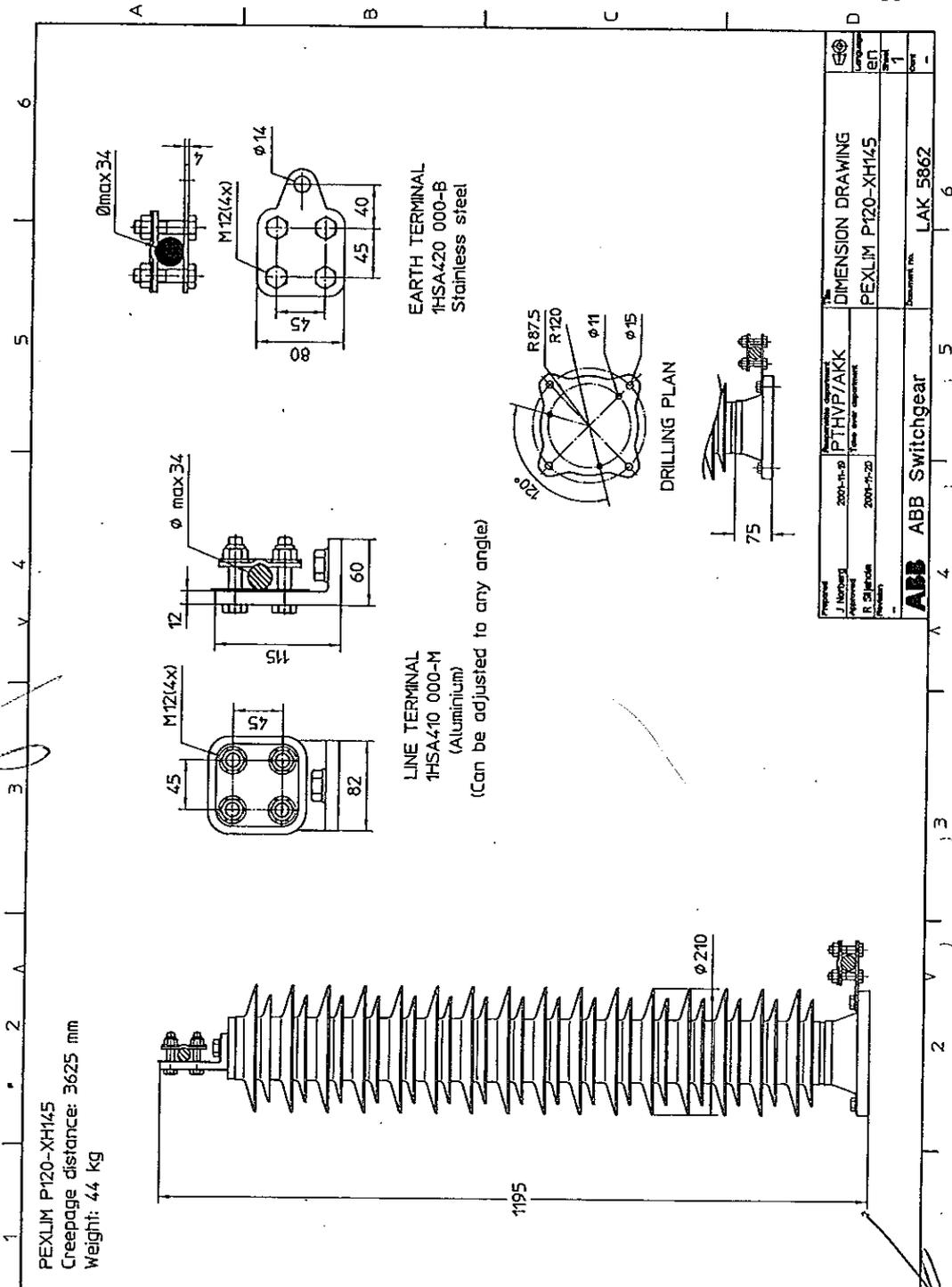
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ВЯРНО  
ОРИГИНАЛ





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ABB Switchgear AB

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ВАЖНО С  
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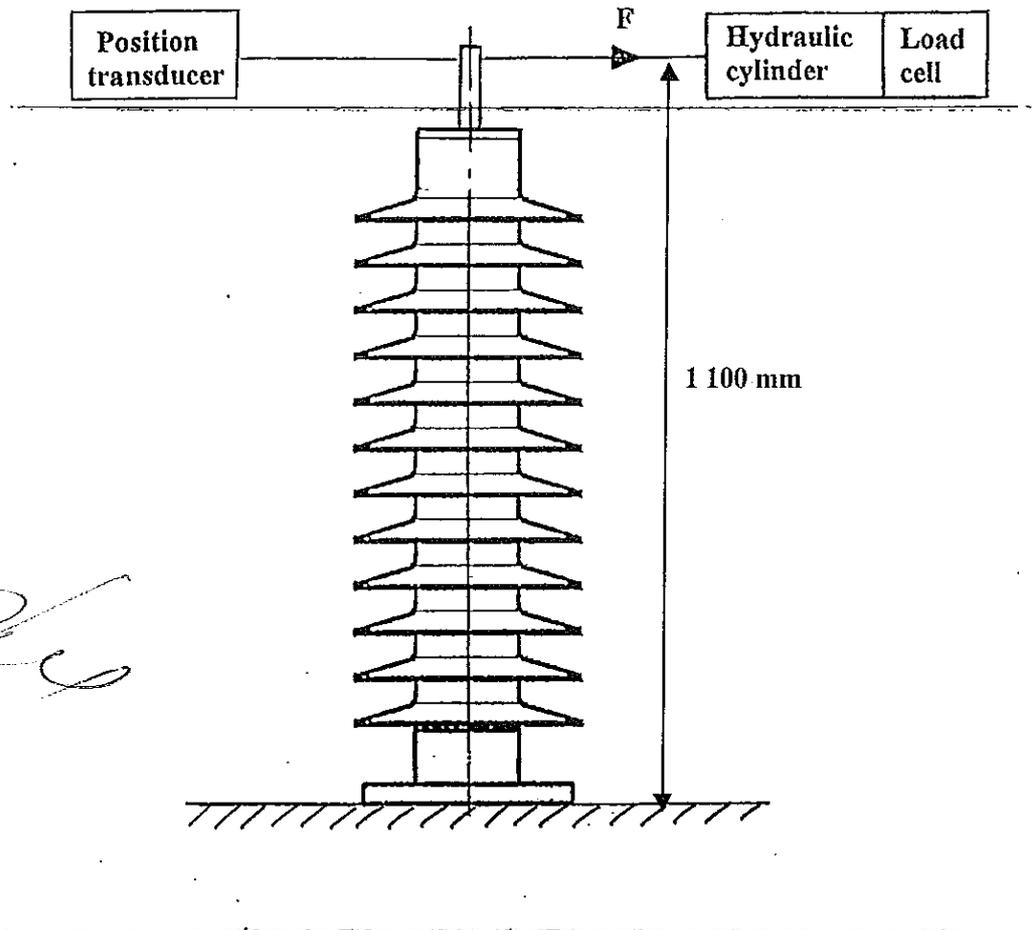


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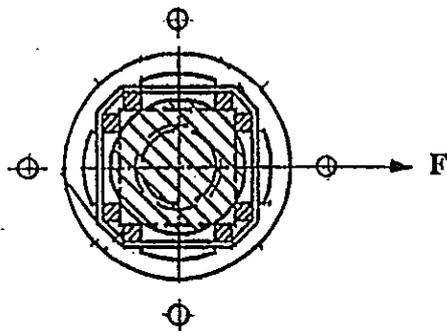
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Appendix 2



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**BENDING DIRECTION**



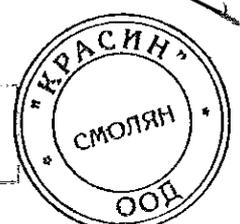
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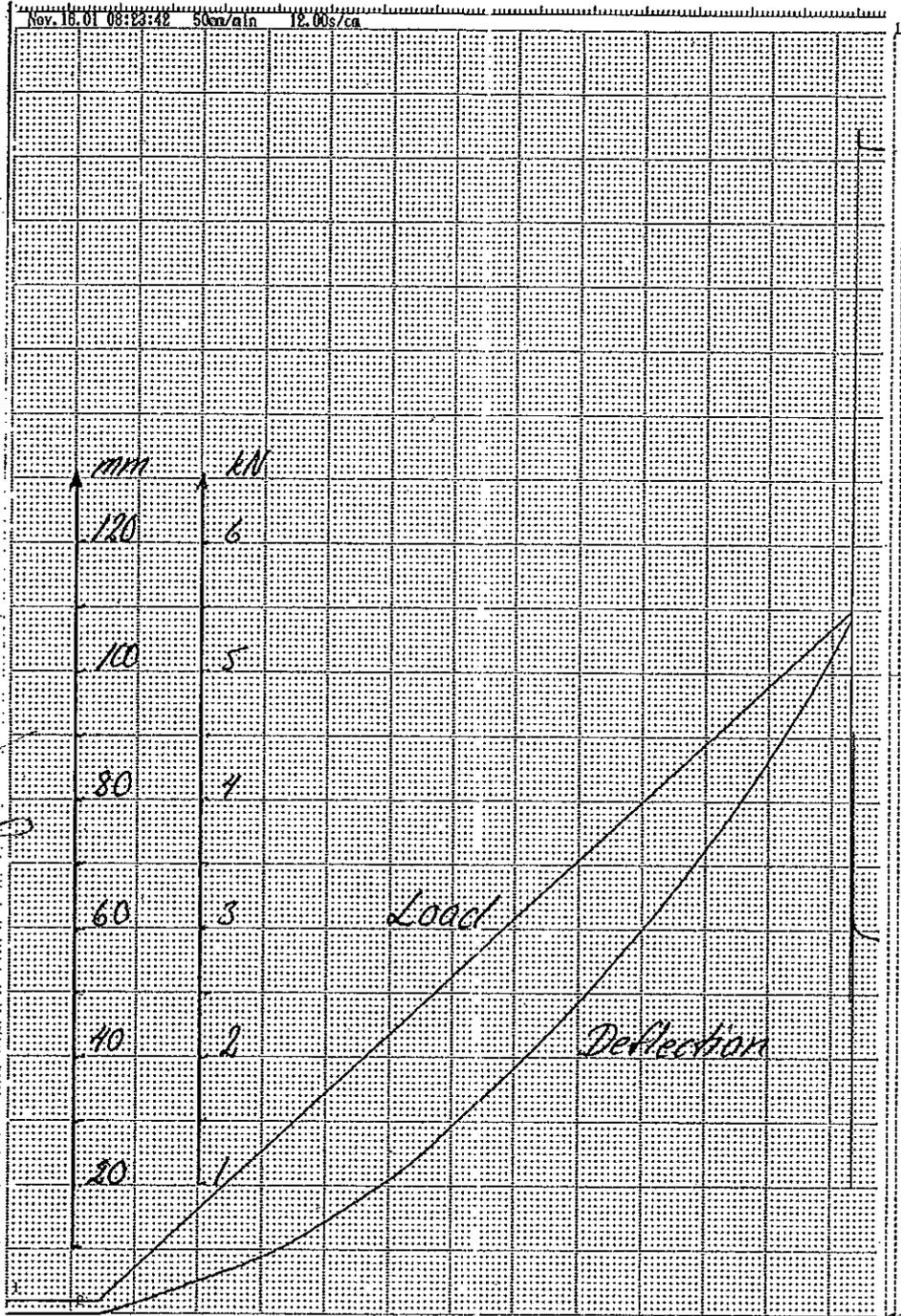
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ВАЖНО С  
ОРИГИНАЛА



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P-X28



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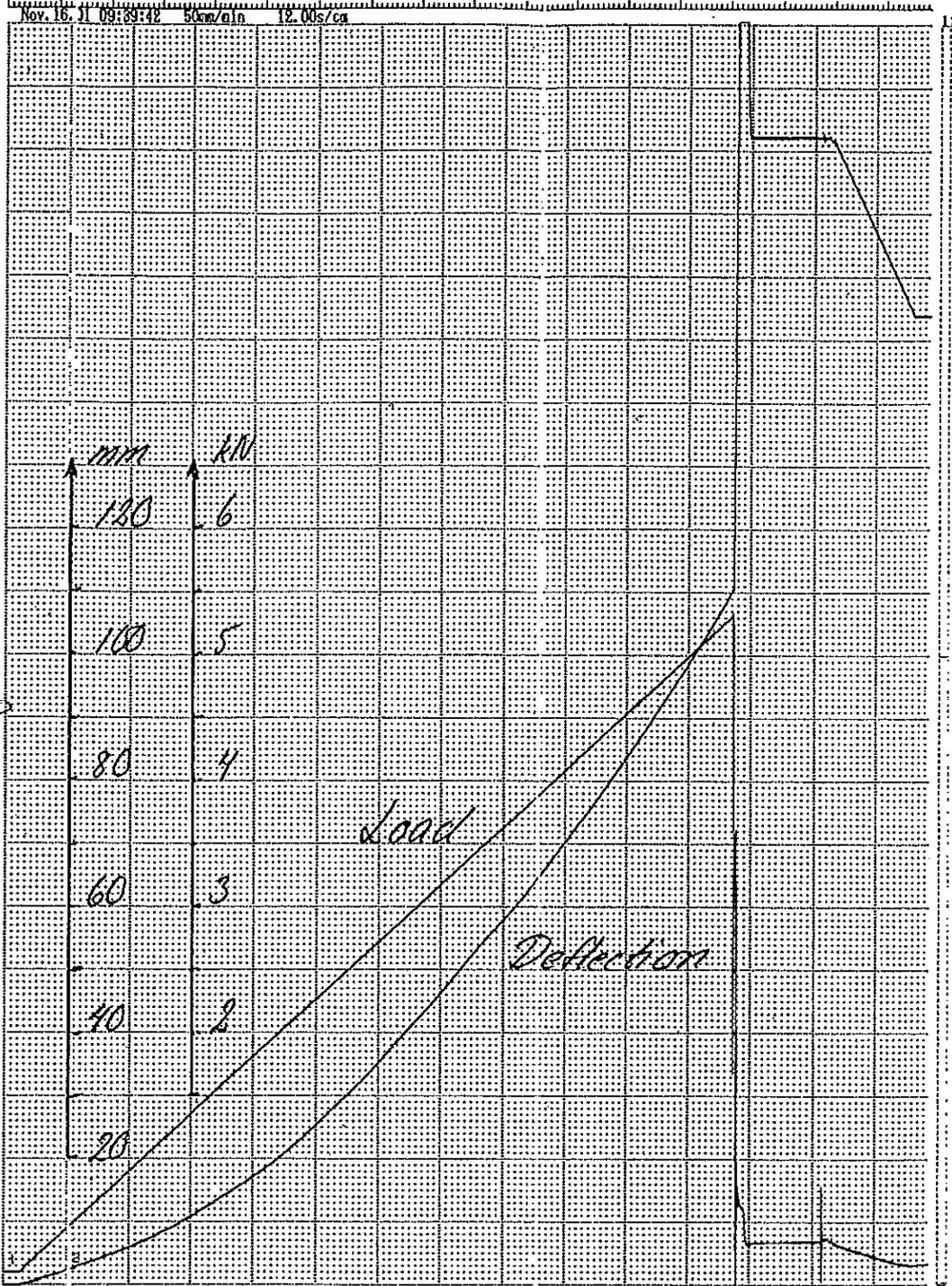
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ОРИГИНАЛА



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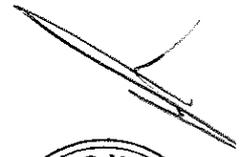
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P-X29



Ref

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ВЕРНО С  
ОРИГИНАЛА





### Type tests on PEXLIM P Surge Arresters

Test objects: Surge arresters of type PEXLIM P120-XH145 with rated voltage 120 kV.

Standards: IEC 60099-4, Amendment 2 (Annex O) of October 2001 (Same requirements as per earlier IEC document 37/231/CDV)

Tests performed: Pressure relief tests

<u>Current</u>	<u>Report</u>
65 kA	KEMA 566-01 *
25 kA	KEMA 566-01
12 kA	KEMA 566-01
600 A	KEMA 566-01

\*) First current peak  $\geq$  2.5 times 65 kA

Validation: The test objects represent the longest electrical and mechanical sections used for PEXLIM P-X arresters. The tests therefore verify the performance of all arresters of type PEXLIM P-X.

Tests completed: 2001-11-22

Tests performed at: KEMA Arnhem - High Power Laboratory

Report consists of: 46 pages (KEMA 566-01, 45 pages)

We hereby certify that the objects specified above have successfully passed the test herein reported, thereby verifying guaranteed data.

Ludvika 2002-01-08

ABB Power Technology Products AB  
 High Voltage Products/ Surge Arresters  
 Quality Department

на основание чл. 2 от ЗЗЛД

Kurt Jansson



ABB Power Technology Products AB

000137



ВЪРХУ С ОРИГИНАЛА

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## REPORT OF PERFORMANCE

CLIENT ABB Switchgear AB,  
Ludvika, Sweden  
MANUFACTURER ABB Switchgear AB,  
Ludvika, Sweden  
APPARATUS One unit of an outdoor metal-oxide polymeric surge arrester  
DESIGNATION PEXLIM P120-XH145

### RATINGS ASSIGNED BY THE MANUFACTURER

Prospective fault current 163 kA<sub>peak</sub> - 65 kA<sub>rms</sub> during 0.2 s  
Voltage 120 kV  
Frequency 50 Hz

The tests have been carried out in accordance with the client's instructions.  
Test procedure and test parameters were based on IEC Draft 37/231/CDV.

Date of tests 22nd November 2001

The performance of the apparatus tested and the observations made during the tests have been recorded in the tables with test results and the oscillograms

### THIS REPORT CONSISTS OF:

Pages	12 (including this front page)
Circuit diagrams	2
Oscillograms	17
Drawings	1
Photographs	12
Information sheet	B70E

This report falls under the scope of the accreditation certificate L020 of the Dutch Council for Accreditation.  
(Information sheet B70E at the back of this document)

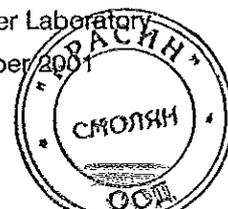
© Copyright: Publication or reproduction of the contents of this report in any other form than a complete copy to the letter, is not allowed without our written consent.

KEMA Nederland B.V.

P.G.A. Bus  
Manager High-Power Laboratory  
Arnhem, 6th December 2001

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ВЯНО С  
ОРИГИНАЛА



TYPE OF TEST	TYPE	PAGE
High-current pressure relief test at rated short-circuit current	P-X4	5
High-current pressure relief test at reduced short-circuit current	P-X5	7
High-current pressure relief test at reduced short-circuit current	P-X6	9
Low-current pressure relief test	P-X8	11

*The tests were witnessed by:*

**Name**

Ekeröth Reljm, K.

**Company**

ABB High Voltage Products,  
Ludvika, Sweden

Andersson, C.  
Olofson, M.

BMB Composites  
Sweden

*The tests were observed by:*

**Name**

Heuts, J.P.

**Company**

KEMA,  
Arnhem, The Netherlands

*Drawing*

The following drawing has been included on request of the client.  
KEMA has not verified this drawing.

LAK 5869 Rev. 0

*Photographs*

1415201  
1415202  
1415203  
1415204  
1415205  
1415206  
1415207  
1415210  
1415211  
1415212  
1415214  
1415215

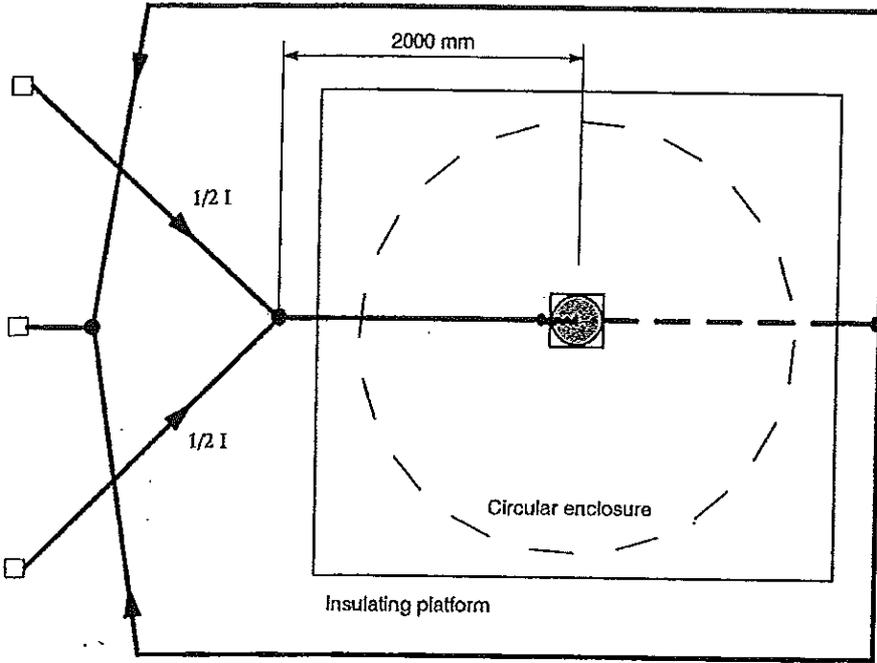
B10E

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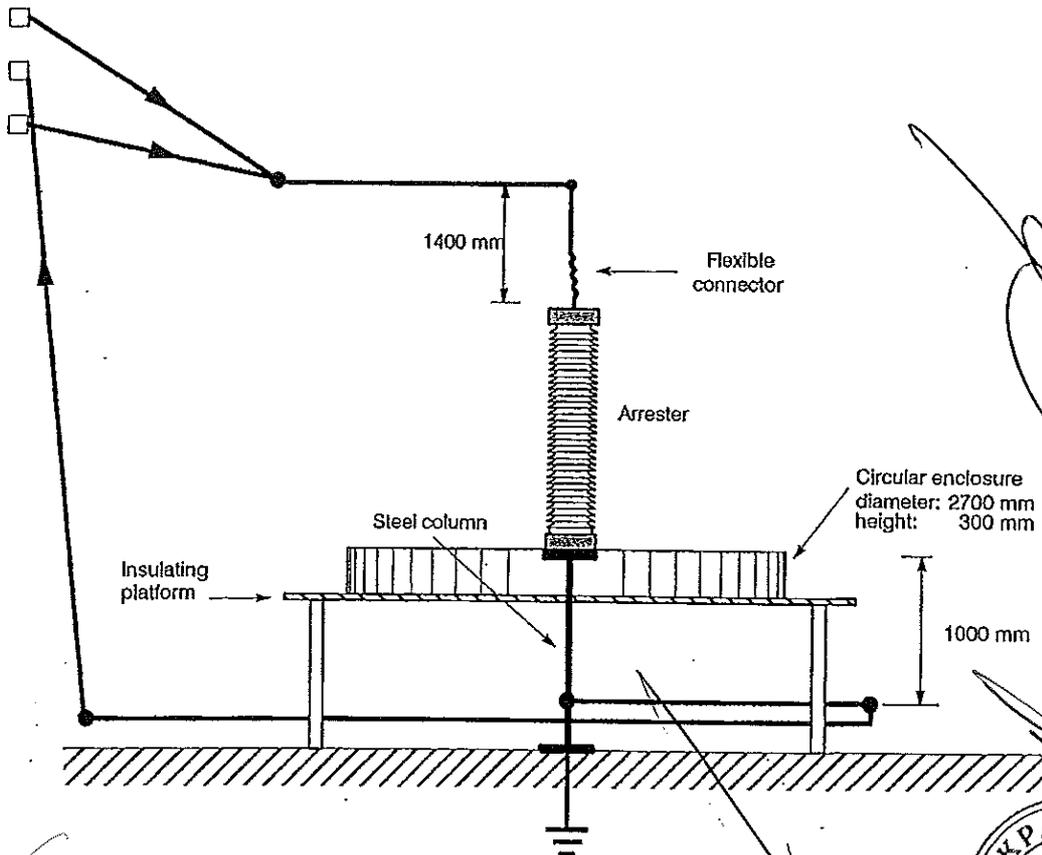
ВЕРНО С  
ОРИГИНАЛА

## TEST ARRANGEMENT

Top view:



Side view:



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ВЕРНО С  
ОРИГИНАЛА





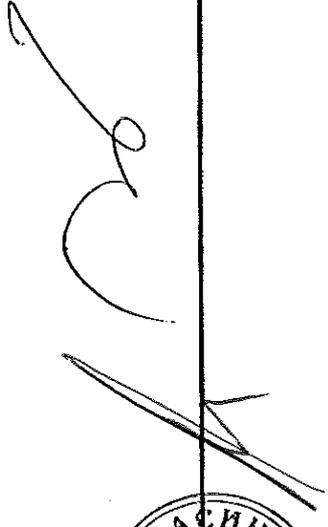
TABLE WITH TEST RESULTS

REPORT 566-01      Checking of the circuit settings for high-current pressure-relief test at rated short-circuit current (Constant voltage method)      TEST CIRCUIT S02 / S01      PAGE 4

Condition before tests: -

Date and test	Applied voltage KV	Peak value of current kA	Symmetrical current				Arc voltage peak value KV	Duration ms	Instant of venting after initiation of current ms	Leakage current $I_{pre}$ mA	Fault current $I_{ch}$ A	Remarks	Physical behaviour	
			Beginning kA	Middle kA	End kA	Average kA							Flame	Emission of Gas
011122 .4004	48.0	192	68.5	68.9	68.5	68.6	220			29.3	Checking of the prospective rated short-circuit current and the fault current.			
011122 4007	124									29.2	Checking of the overvoltage source and the fault current.			

Condition after tests: -

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ВЯНО С  
ОРИТНАЛА



KEMA

**TABLE WITH TEST RESULTS**

REPORT 566-01	High-current pressure-relief test at rated short-circuit current (Constant voltage method)	TEST CIRCUIT	S01 / S01' / S02	PAGE	5
---------------	--	--------------	------------------	------	---

Condition before tests:

Arrester new. Test sample designated P-X4 (120 kV).  
 Arrester mounted on a pedestal with a height of 30 cm and placed inside a circular enclosure with a diameter of 270 cm and a height of 30 cm.  
 This complete set-up was placed on top of an insulating platform with a vertical bottom conductor in order to simulate under service conditions.  
 Top connections made by flexible connectors. Bottom connection fixed on ground-plate.  
 Photographs 1415201, 1415201.  
 Ambient temperature: 12 °C.

Pre-failing test:

Arrester pre-failed by a constant voltage source (133 kV) initially with a leakage current of approx. 80 mA. See test 011122-4008.  
 After 4 min and 35 s when failing is complete, the arrester is subjected to a fault current of approx. 30 A for approx. 4 s. See test 011122-4009.

High-current short-circuit test:

Initially the arrester is subjected to a fault current of approx. 30 A. After 1.5 s the make-switch (MS2) closes, short-circuiting the capacitive impedance leading to the high-current to flow. See test 011122-4010.

Flame detection by means of photo-resistors on top and bottom of arrester.

Date and test	Applied voltage	Peak value of current	Symmetrical current				Test quantities				Instant of venting after initiation of current	Leakage current	Fault current	Remarks	Physical behaviour		
			Beginning	Middle	End	Average	Arc voltage peak value	Duration	I <sub>pro</sub>	I <sub>ch</sub>					Flame	Emission of	
																	ms
011122-4008	133																
011122-4009	133										77.0			Pre-fail test.	none		none
011122-4010	49.4	163		72.0						2.26		30.0		High-current test.	heavy		heavy

Condition after tests:

The arrester housing cracked open. Photographs 1415203, 145204.  
 Only small fragments of material (< 10 g) and some larger parts of the polymeric housing found outside the enclosure.

000143



TABLE WITH TEST RESULTS

REPORT 566-01      Checking of the circuit settings for high-current pressure-relief test at reduced short-circuit current (Constant voltage method)      TEST CIRCUIT S03      PAGE 6

Condition before tests: --

Date and test	Applied voltage KV	Peak value of current KA	Symmetrical current				Arc voltage peak value KV	Duration ms	Instant of vaning after initiation of current ms	Leakage current $I_{pre}$ mA	Fault current $I_{ch}$ A	Remarks	Physical behaviour		
			Beginning KA	Middle KA	End KA	Average KA							Emission of	Flame	Gas
011122 4013	49.4	71.2	27.6				130			23.5	Checking of the prospective reduced short-circuit current and the fault current.				

Condition after tests: --



**TABLE WITH TEST RESULTS**

REPORT 566-01	High-current pressure-relief test at reduced short-circuit current (Constant Voltage method)	TEST CIRCUIT	S01 / S01 / S03	PAGE	7
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**Condition before tests:**

Arrester new. Test sample designated P-X5 (120 kV).  
 Arrester mounted on a pedestal with a height of 30 cm and placed inside a circular enclosure with a diameter of 270 cm and a height of 30 cm.  
 This complete set-up was placed on top of an insulating platform with a vertical bottom conductor in order to simulate under service conditions.  
 Top connections made by flexible connectors. Bottom connection fixed on ground-plate.  
 Photograph 1415205.  
 Ambient temperature: 12 °C.

**Pre-falling test:**

Arrester pre-failed by a constant voltage source (133 kV) initially with a leakage current of approx. 80 mA. See test 011122-4014.  
 After 5 min, when falling is complete, the arrester is subjected to a fault current of approx. 30 A for approx. 3 s. See test 011122-4015.

**Reduced high-current short-circuit test:**

Initially the arrester is subjected to a fault current of approx. 30 A. After 1.5 s the make-switch (MS2) closes, short-circuiting the capacitive impedance leading to the reduced high-current to flow. See test 011122-4016.

Flame detection by means of photo-resistors on top and bottom of arrester.

Date and test	Applied voltage	Test quantities						Instant of venting after initiation of current	Leakage current	Fault current	Remarks	Physical behaviour					
		Peak value of current	Symmetrical current			Arc voltage peak value	Duration					Flame	Emission of	Gas			
			Beginning	Middle	End										Average		
011122-4014	133																
011122-4015	133							80			Pre-fail test.				none		none
011122-4016	48.3	59.0			27.6					32.4	Pre-fail test.				none		none
							2.80		218	23.0	Reduced high-current test.				heavy		heavy

Condition after tests:  
 The arrester housing cracked open. Photographs 1415206, 1415207.  
 Only small fragments of material (< 10 g) and some parts of the polymeric housing found outside the enclosure.

000145



**KEMAR**

TABLE WITH TEST RESULTS

REPORT 566-01      Checking of the circuit settings for high-current pressure-relief test at reduced short-circuit current (Constant voltage method)      TEST CIRCUIT S04      PAGE 8

Condition before tests: -

Date and test	Applied voltage kV	Peak value of current kA	Test quantities				Instant of venting after initiation of current ms	Leakage current $I_{pro}$ mA	Fault current $I_{ch}$ A	Remarks	Physical behaviour	
			Symmetrical current								Flame	Emission of Gas
			Beginning	Middle	End	Average						
011122 4019	50.4	40.8		14.0				24.5	Checking of the prospective reduced short-circuit current and the fault current.			

Condition after tests: -

*[Handwritten signatures and marks]*

000146

ОРИГИНАЛ



KEMAR



TABLE WITH TEST RESULTS

REPORT 566-01      Checking of the circuit settings for low-current pressure-relief test (Constant voltage method)      TEST CIRCUIT S05      PAGE 10

Condition before tests: -



Date and test	Applied voltage	Peak value of current	Symmetrical current				Arc voltage peak value	Duration	Instant of venting after initiation of current	Leakage current	Fault current	Remarks	Physical behaviour	
			Begin-ring	Middle	End	Average							Emission of	
													Flame	Gas
011122 40Z7	kV 123	kA 1.39	kA 0.613	kA 0.608	kA 0.613	kA 0.610	s 1.00	ms	mA	A	Checking of the prospective low short-circuit current and the fault current.			

Condition after tests: -



000148

БЪЛГАРСКО  
ОРИЕНТАЛ

TABLE WITH TEST RESULTS

REPORT 566-01 Low-current pressure-relief test (Constant voltage method) TEST CIRCUIT S01 / S01 / S05 PAGE 11

Condition before tests: Arrester new. Test sample designated P-X8 (120 kV).

Arrester mounted on a pedestal with a height of 30 cm and placed inside a circular enclosure with a diameter of 270 cm and a height of 30 cm. This complete set-up was placed on top of an insulating platform with a vertical bottom conductor in order to simulate under service conditions. Top connections made by flexible connectors. Bottom connection fixed on ground-plate. Photograph 1415114.

Ambient temperature: 12 °C.

Pre-failing test: Arrester pre-failed by a constant voltage source (133 kV) initially with a leakage current of approx. 80 mA. See test 011122-4028.

After 7 min, when failing is complete, the arrester is subjected to a fault current of approx. 30 A for approx. 3 s. See test 011122-4029.

Low high-current short-circuit test: Initially the arrester is subjected to a fault current of approx. 30 A. After 1.5 s the make-switch (MS2) closes, short-circuiting the capacitive impedance leading to the low-current test to flow. See test 011122-4030.

Flame detection by means of photo-resistors on top and bottom of arrester.

Date and test	Applied voltage kV	Test quantities						Instant of venting after initiation of current ms	Leakage current $I_{pre}$ mA	Fault current $I_{ch}$ A	Remarks	Physical behaviour	
		Peak value of current kA	Symmetrical current			Arc voltage peak value kV	Duration s					Flame	Emission of Gas
			Beginning	Middle	End								
011122 4028 7 min	131							87.0		Pre-fail test.	none	none	
011122 4029 10 min	131								32.8	Pre-fail test.	none	none	
011122 4030	122	1.36	0.602	0.605	0.604	4.10	1.04		24.1	Low-current test.	heavy	heavy	

Condition after tests: The arrester housing cracked open. Photograph 1415215. Only small fragments of material (< 10 g) and some parts of the polymeric housing found outside the enclosure.



KEMAR

000149

ВСПРОС  
ОПИШКА

TEST - CIRCUIT DIAGRAM

TEST CIRCUIT No. S01

REPORT No. 566-01

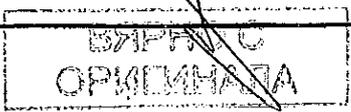
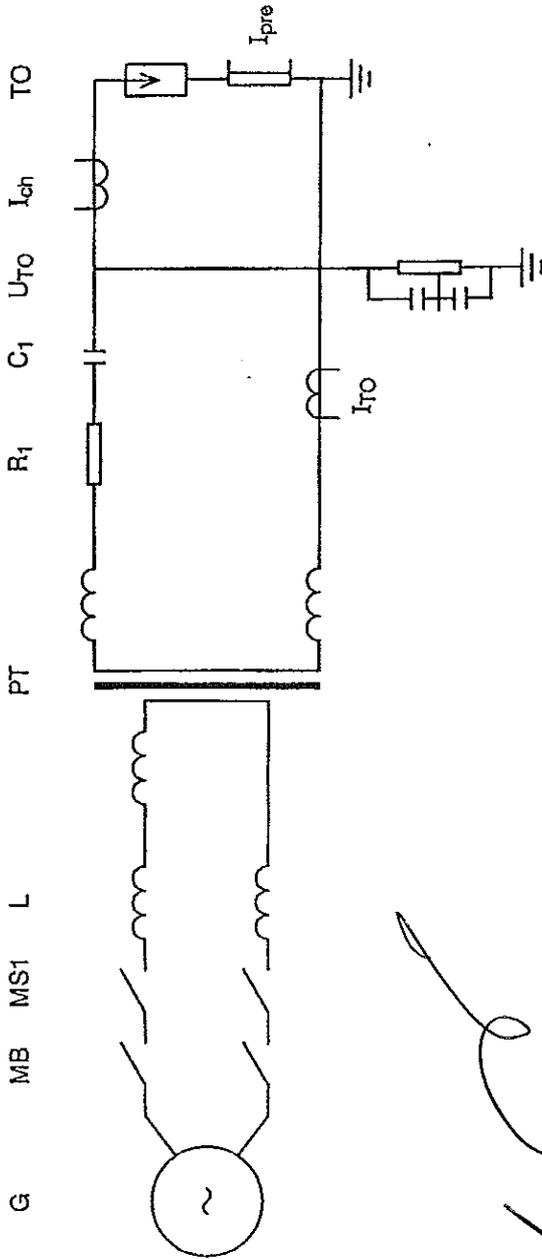
CIRCUIT COMPONENTS

- G = Generator
- MB = Master Breaker
- MS = Make Switch
- PT = Power Transformer
- R = Resistor
- C = Capacitor
- L = Inductance

TO = Test Object

MEASUREMENTS

- U = Voltage Measurement
- I = Current Measurement



000150

KEMA

TEST-CIRCUIT DIAGRAM

TEST CIRCUIT No. S02 to S05

REPORT No. 566-01

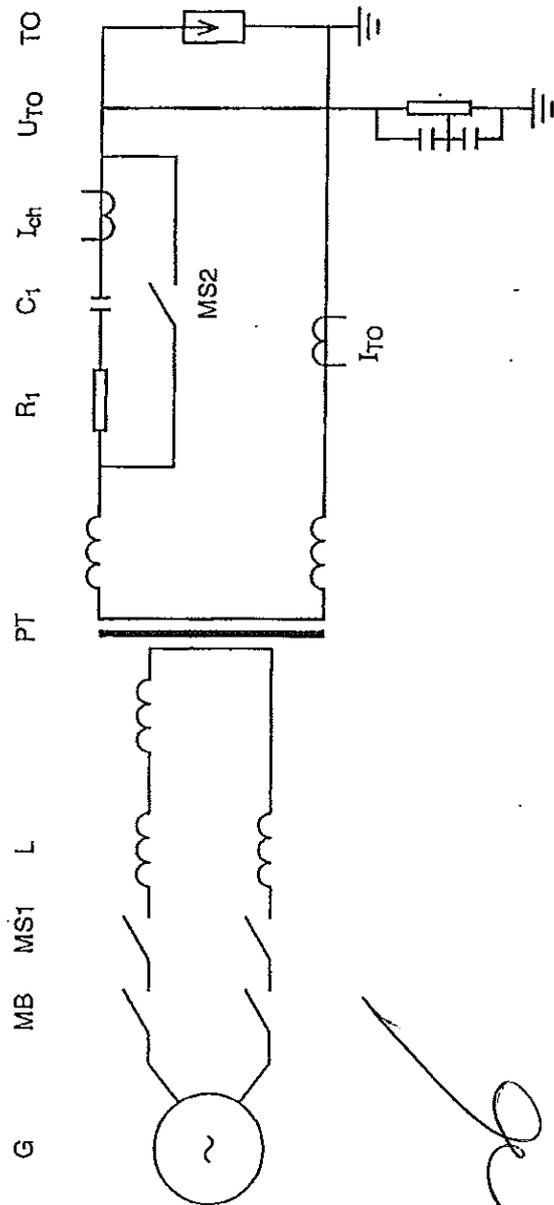
CIRCUIT COMPONENTS

- G = Generator
- MB = Master Breaker
- MS = Make Switch
- PT = Power Transformer
- R = Resistor
- C = Capacitor
- L = Inductance

TO = Test Object

MEASUREMENTS

- U = Voltage Measurement
- I = Current Measurement

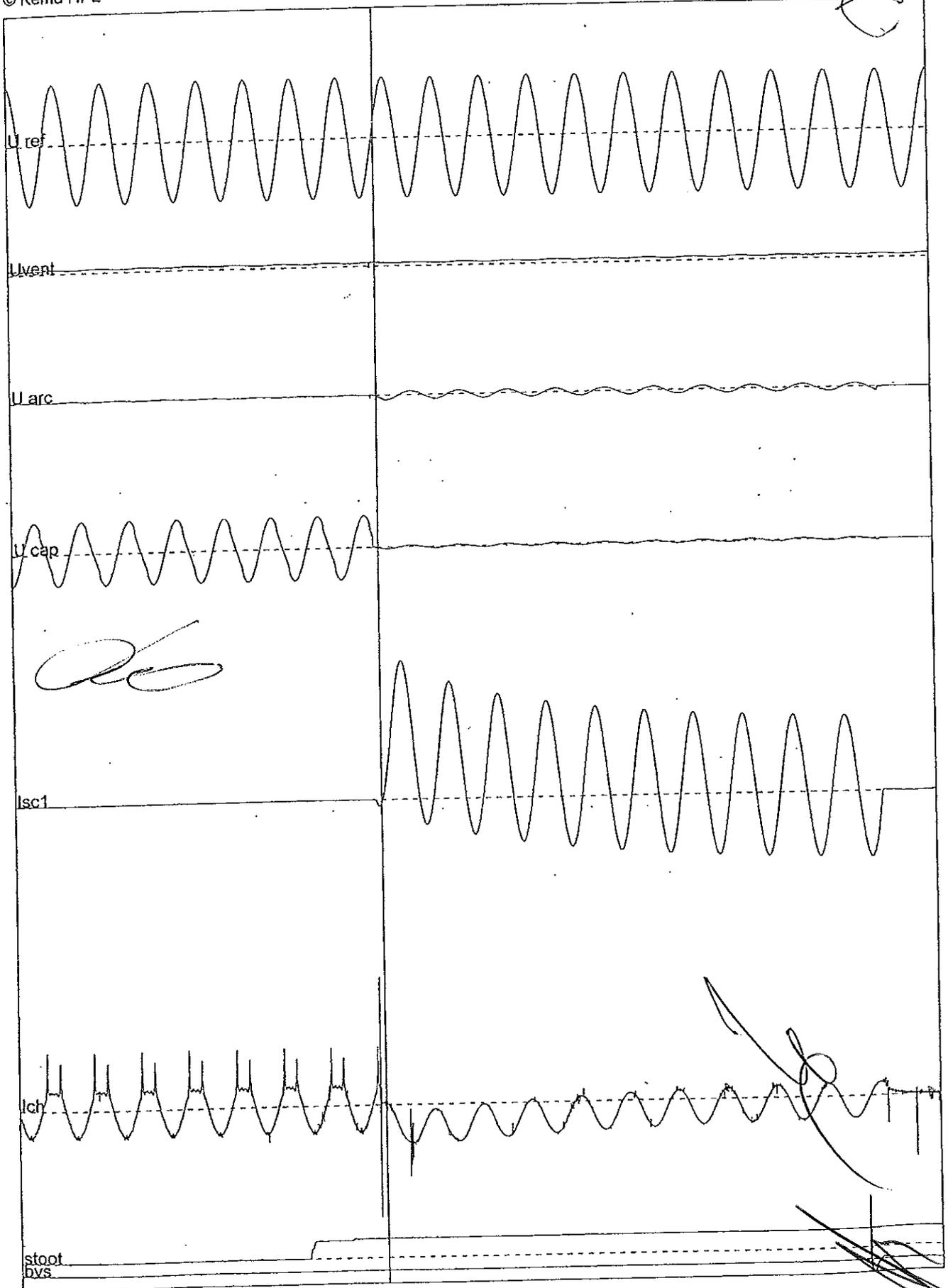



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ОРГИНАЛ



KEMAR



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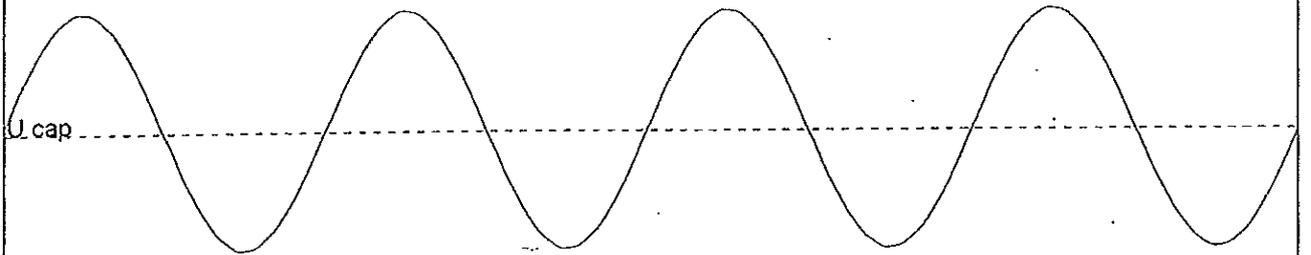
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ВЯРНО С  
ОРИГИНАЛА

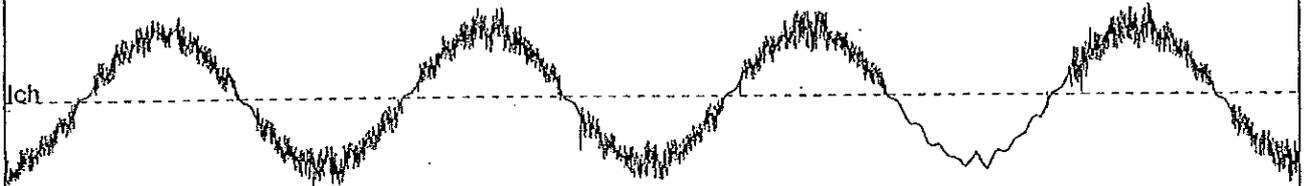


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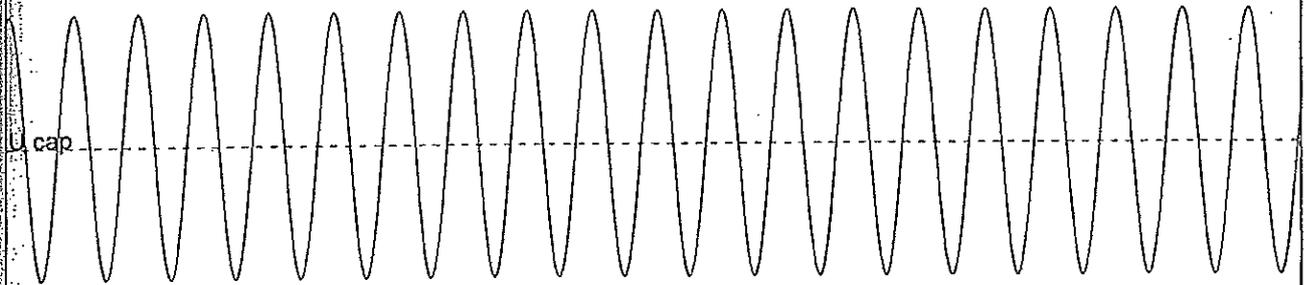
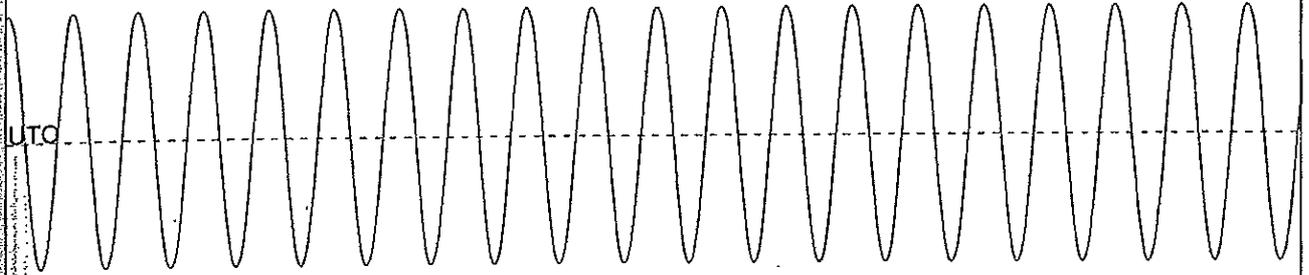
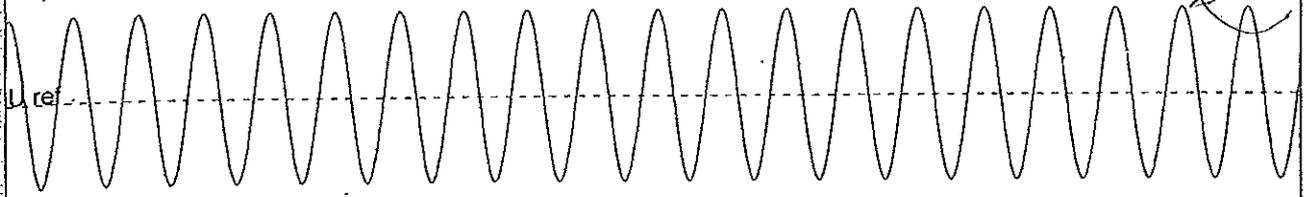
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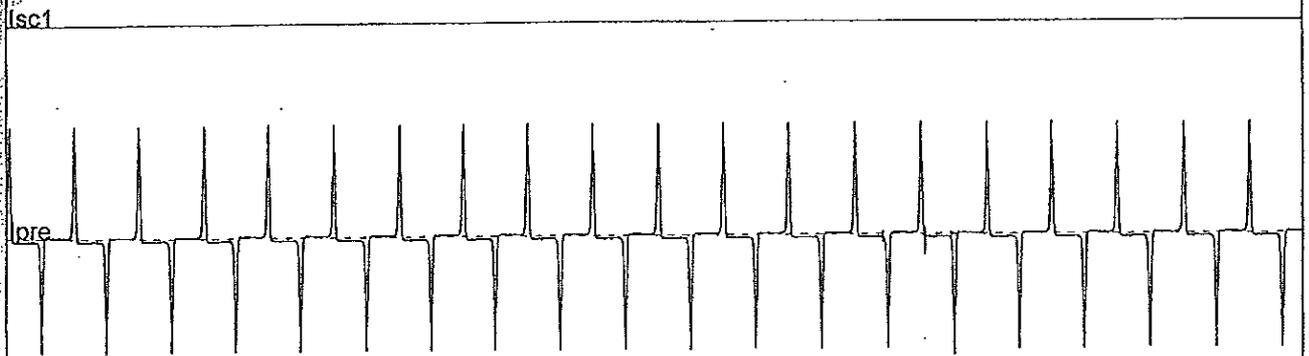
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ВЯРНО С  
ОРИГИНАЛА





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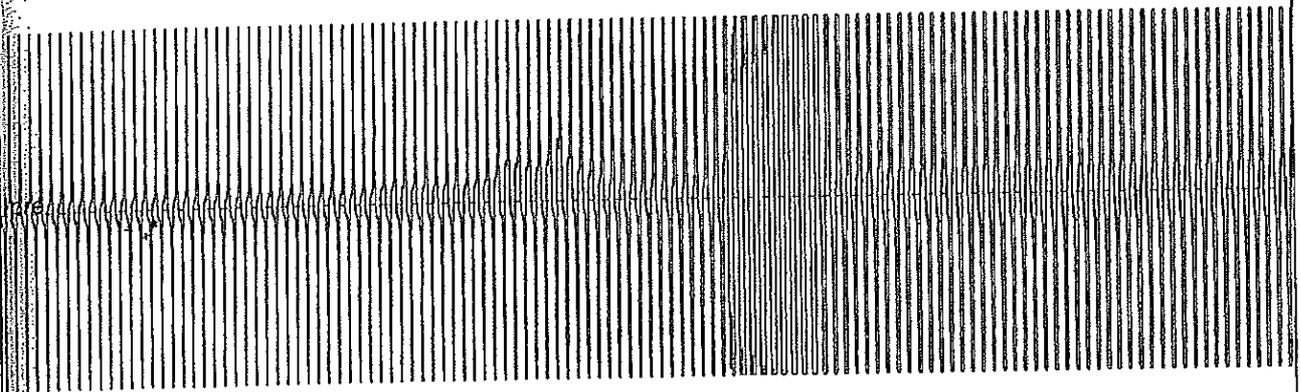
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ВЯНО С  
ОРИНАЛА



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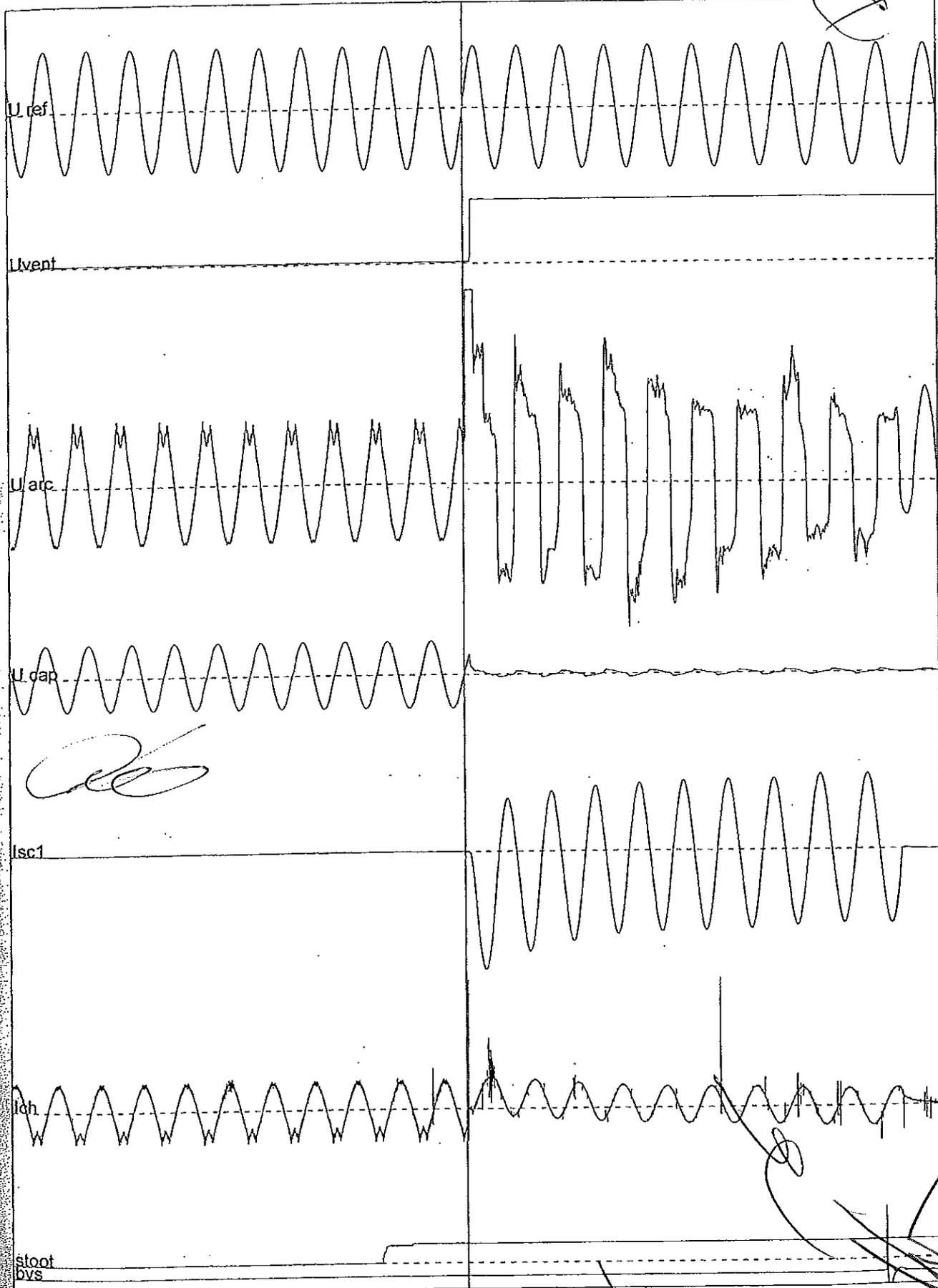
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000155

СРПС  
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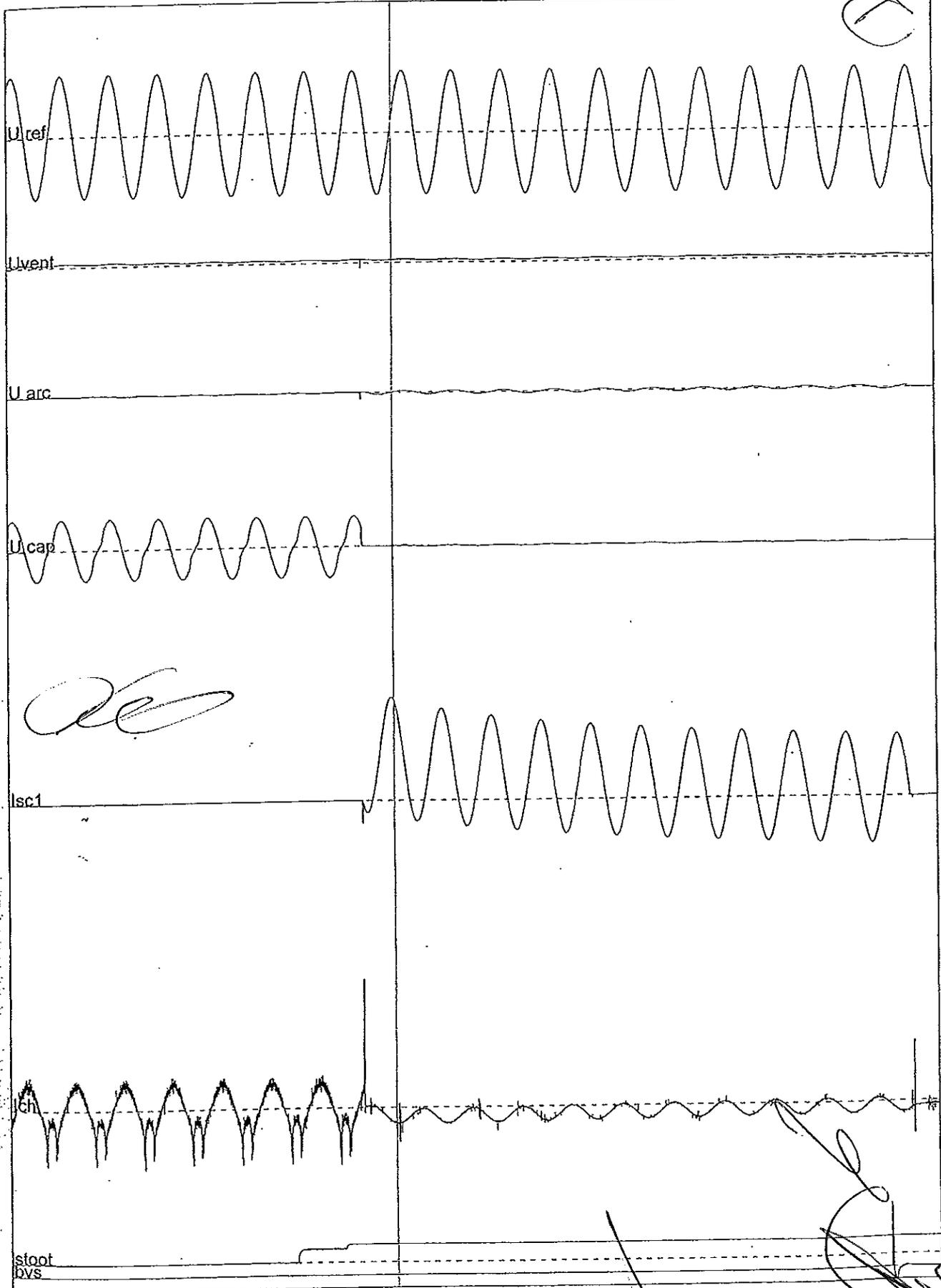
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ВЯНО С  
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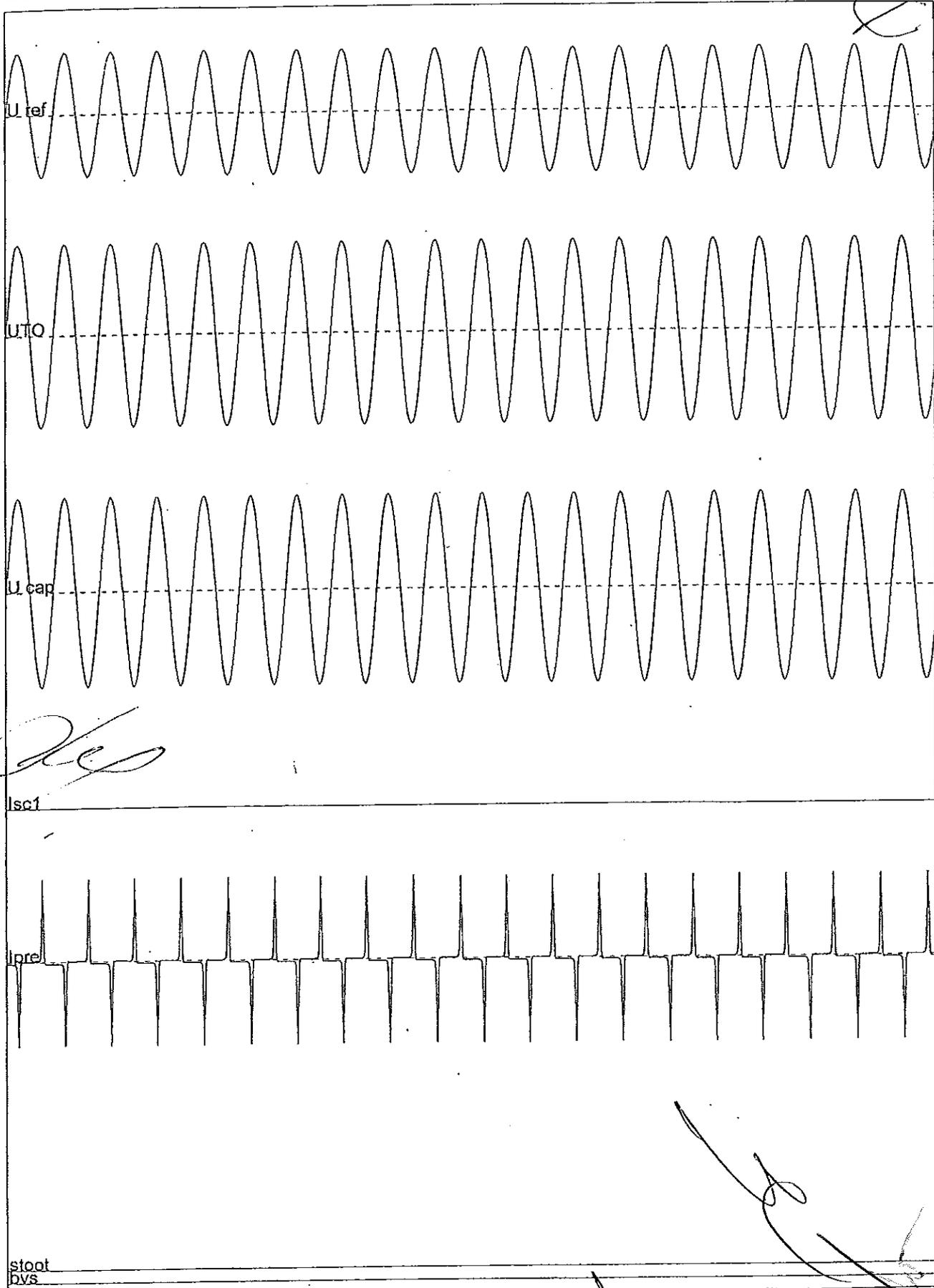
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000157

ВЯРВА С  
ОРИГИНАЛА





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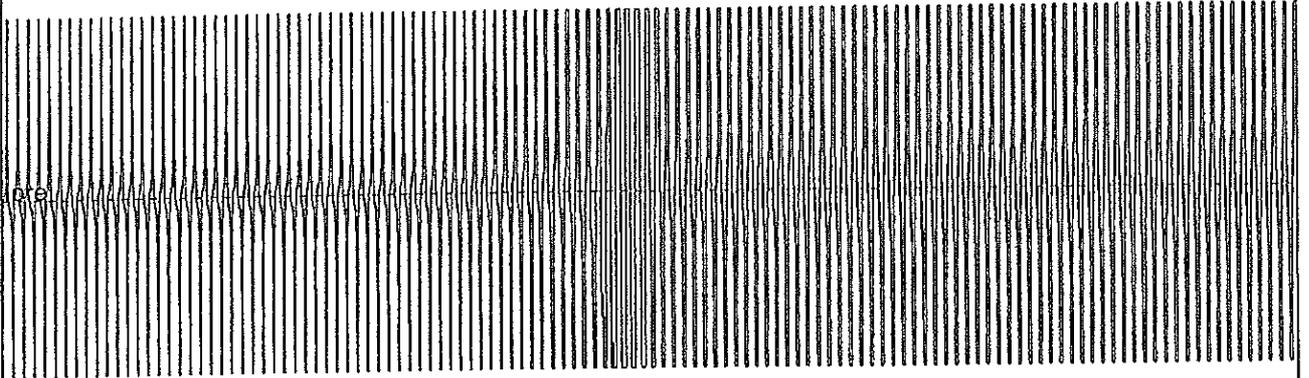
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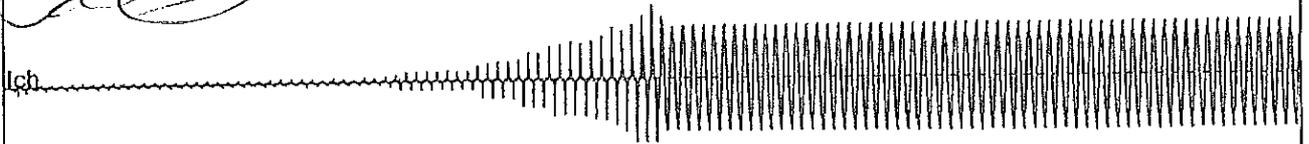
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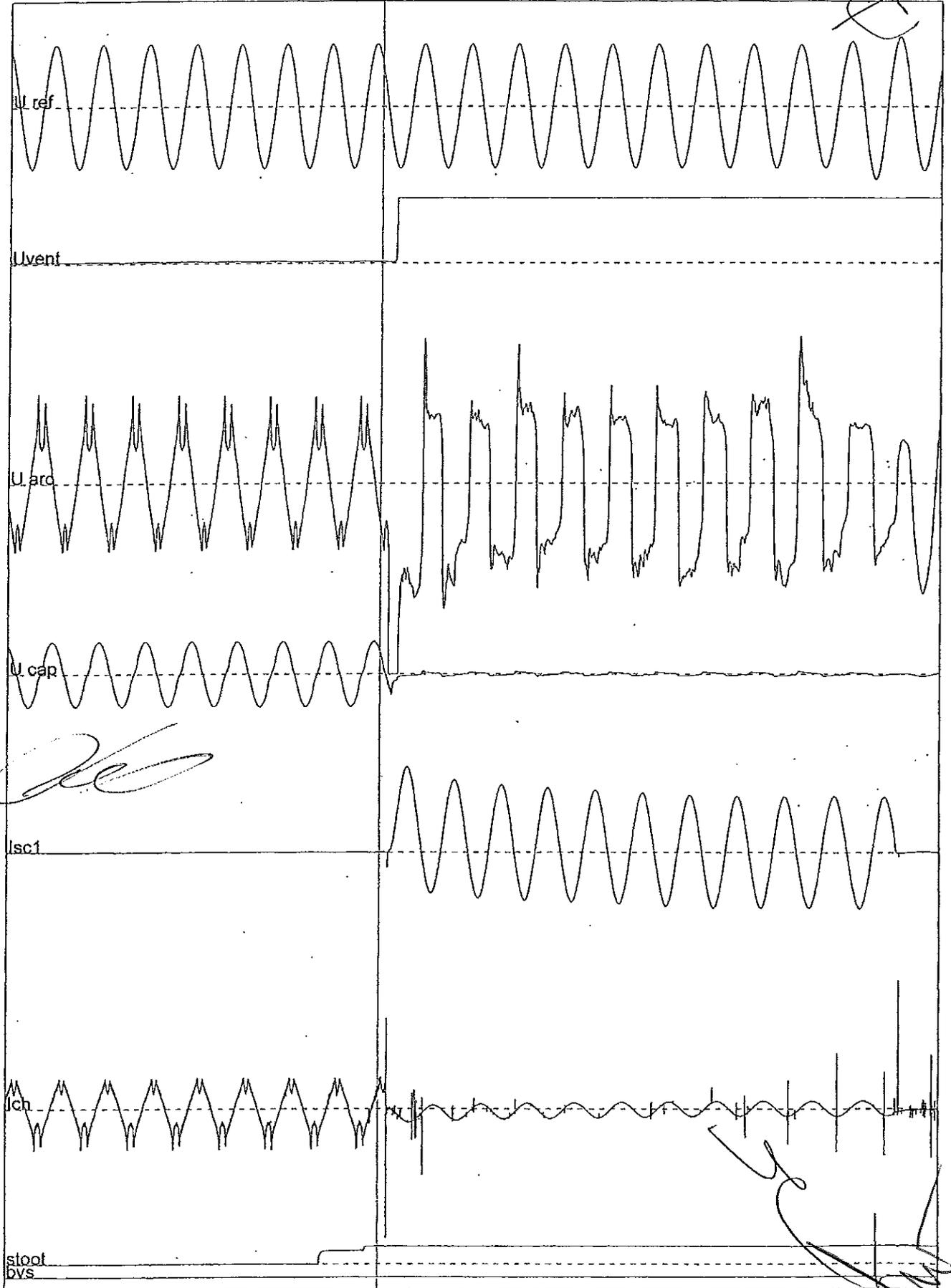
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ВЕРНО С  
ОРИГИНАЛА





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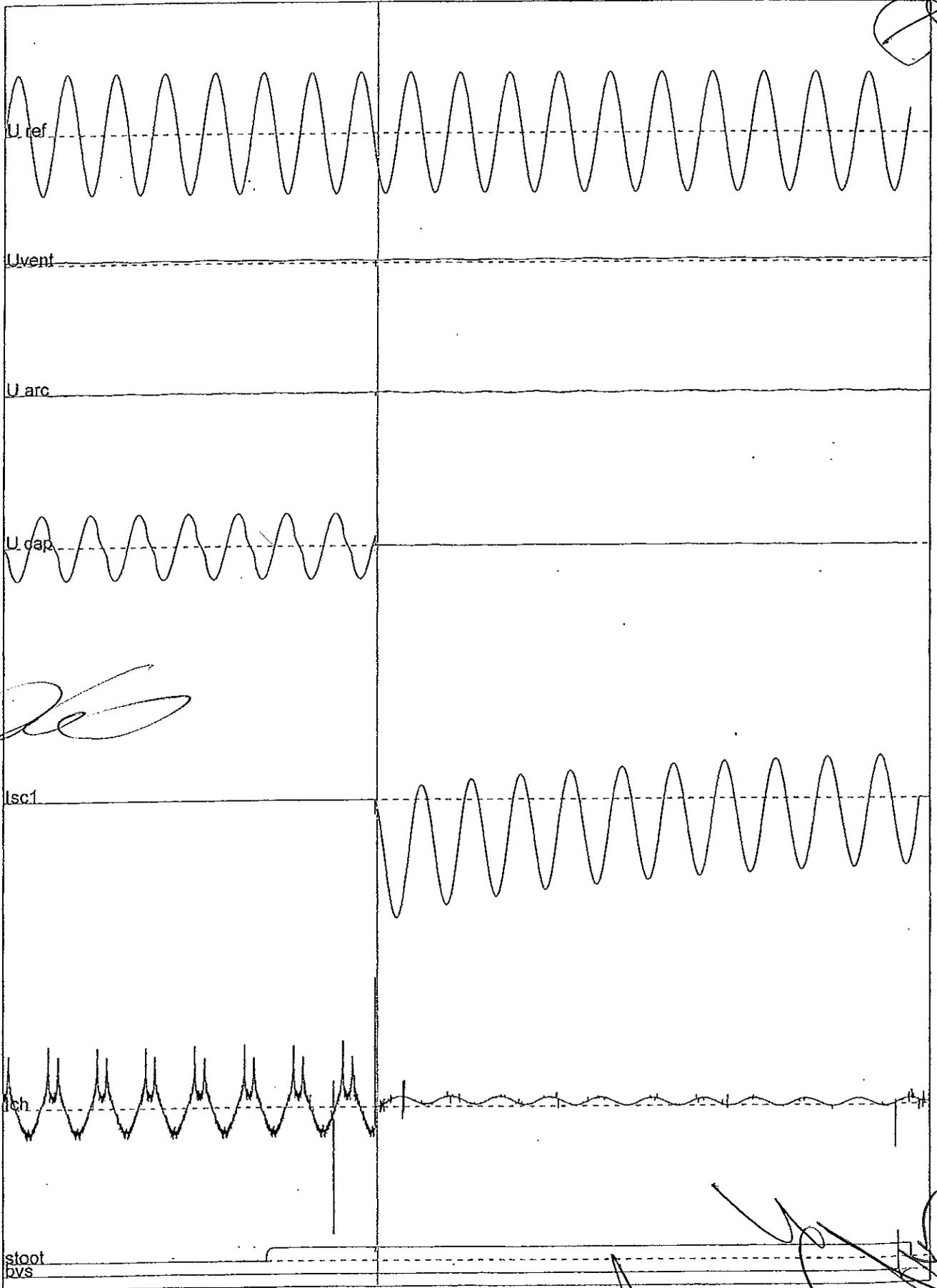
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ВЯРНО С  
ОРИГИНАЛА





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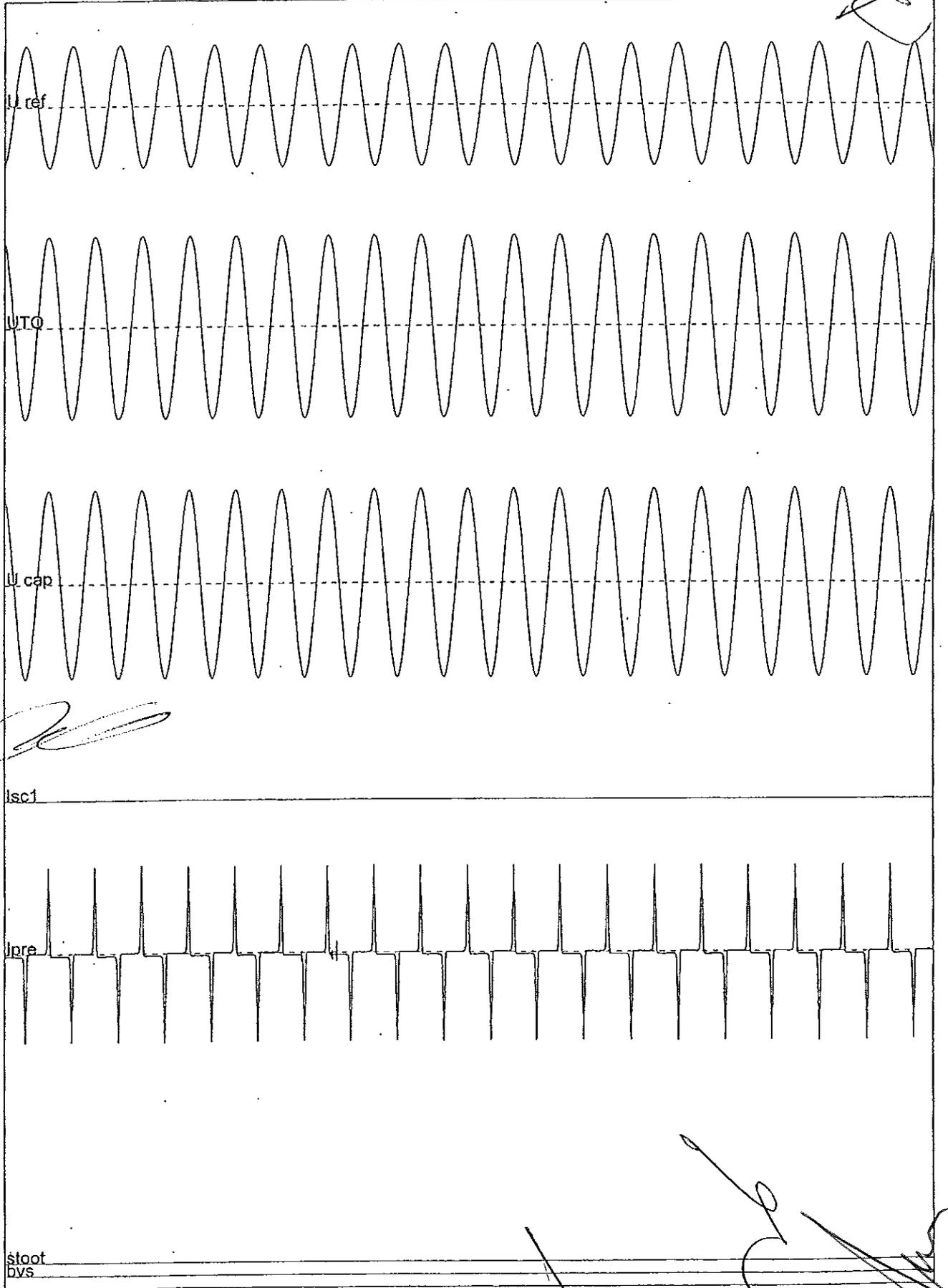
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ВЕРНО С  
ОРИГИНАЛА





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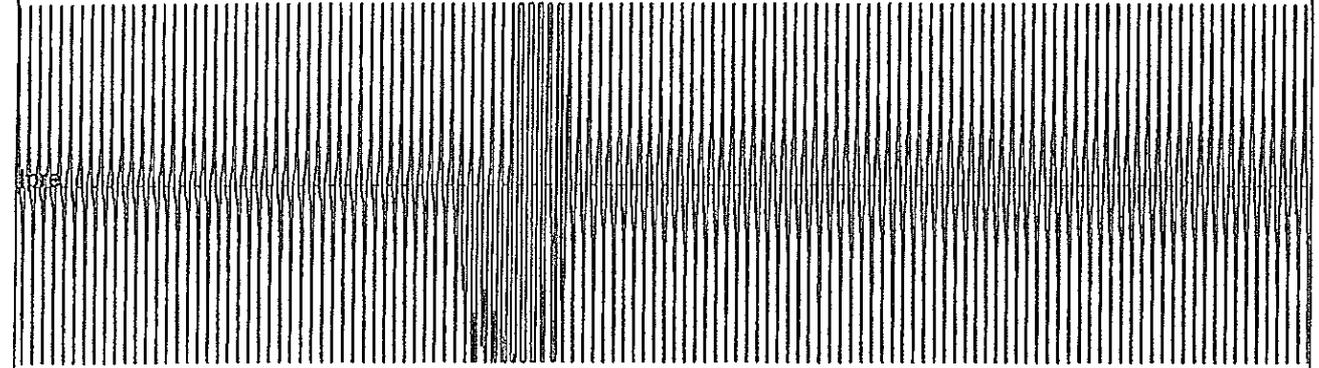
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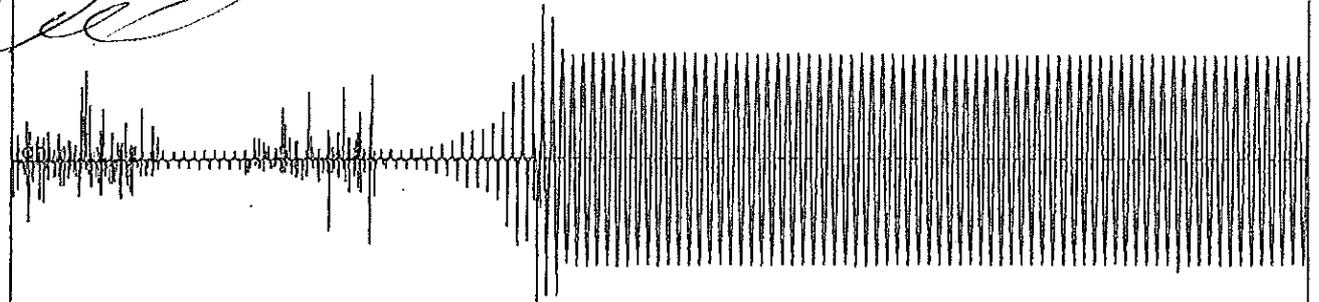
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ВЯРНО С  
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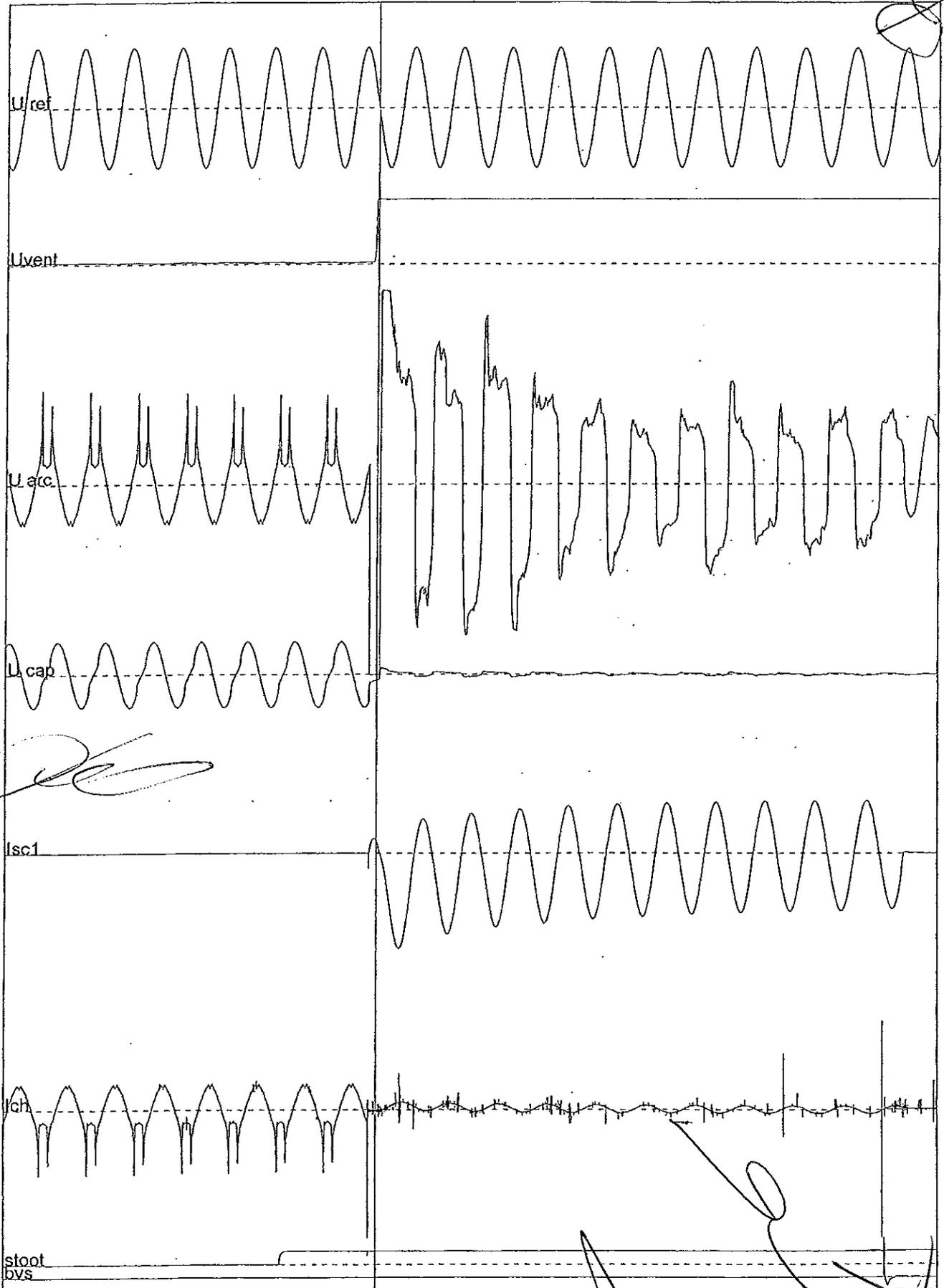
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000163

ОРИГИНАЛ  
КОПИЯ





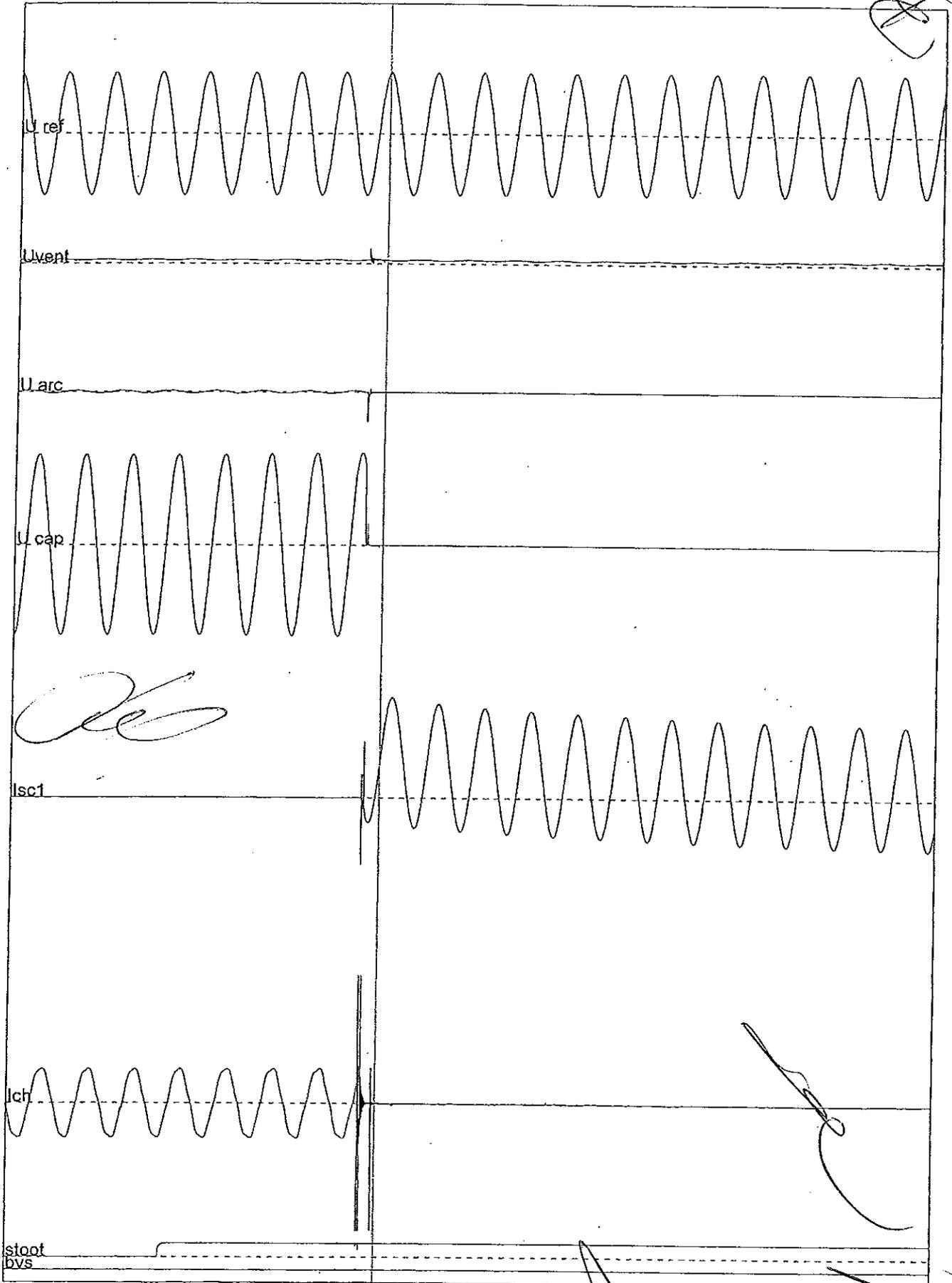
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ВЯРНО С  
ОРИГИНАЛА





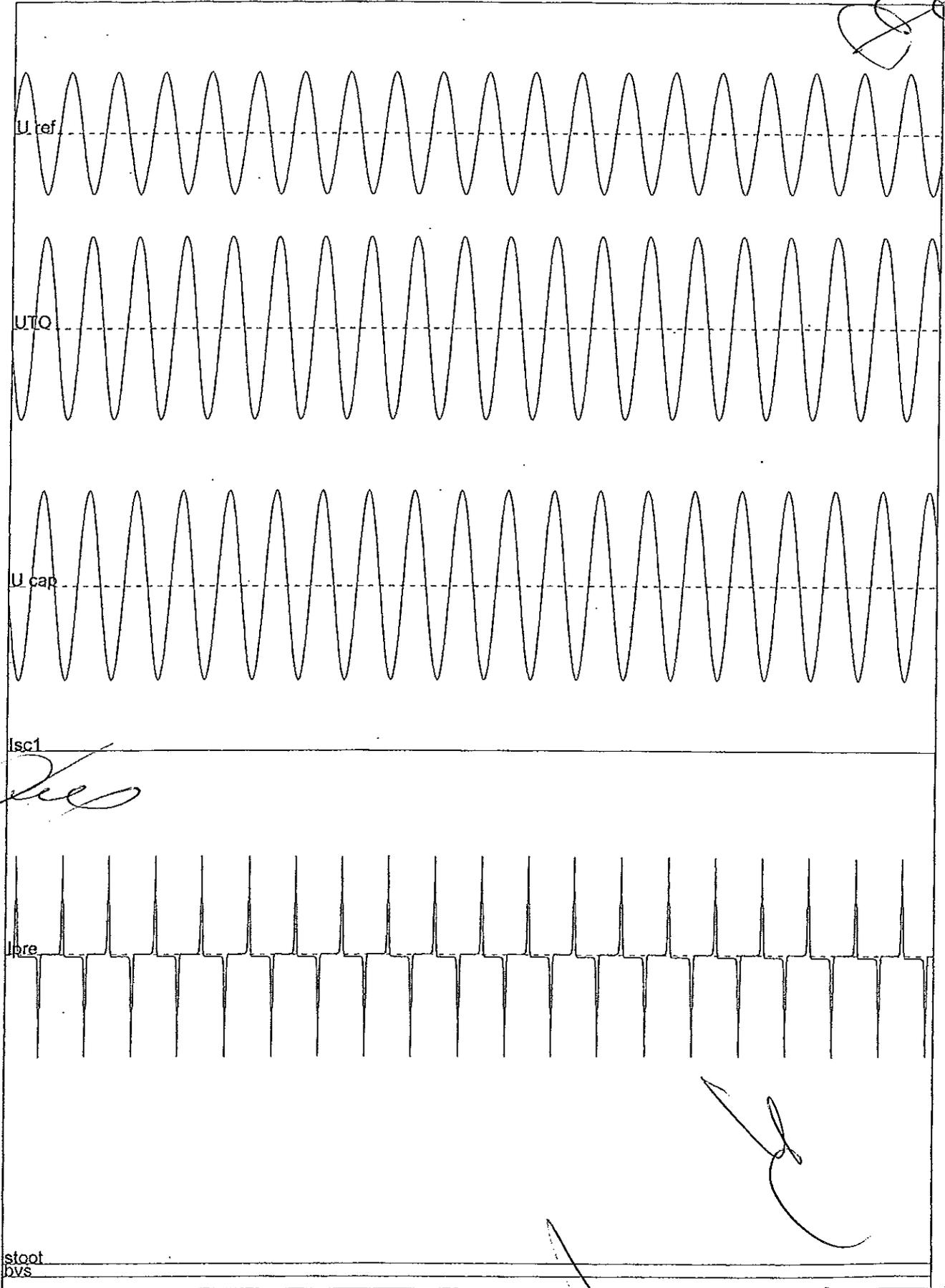
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000165

ЗАНОС  
ОРИГИНАЛА



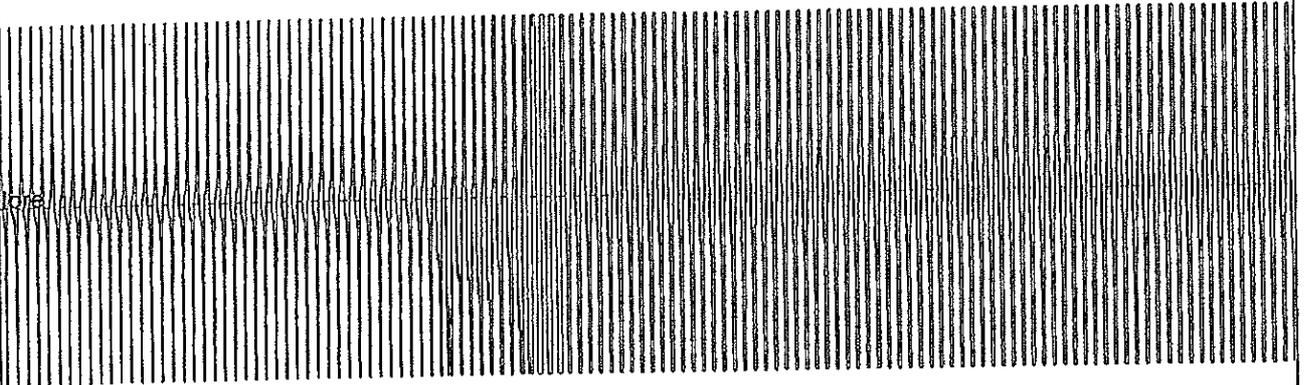
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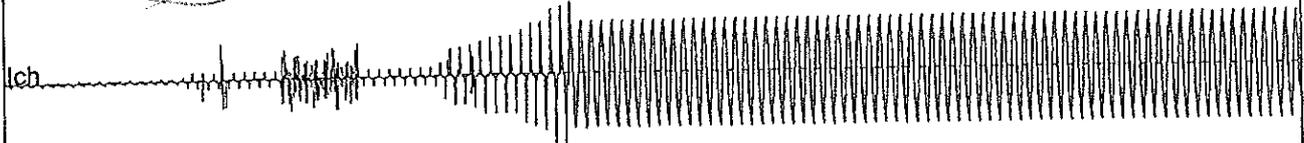
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ОРИГІНАЛ





076

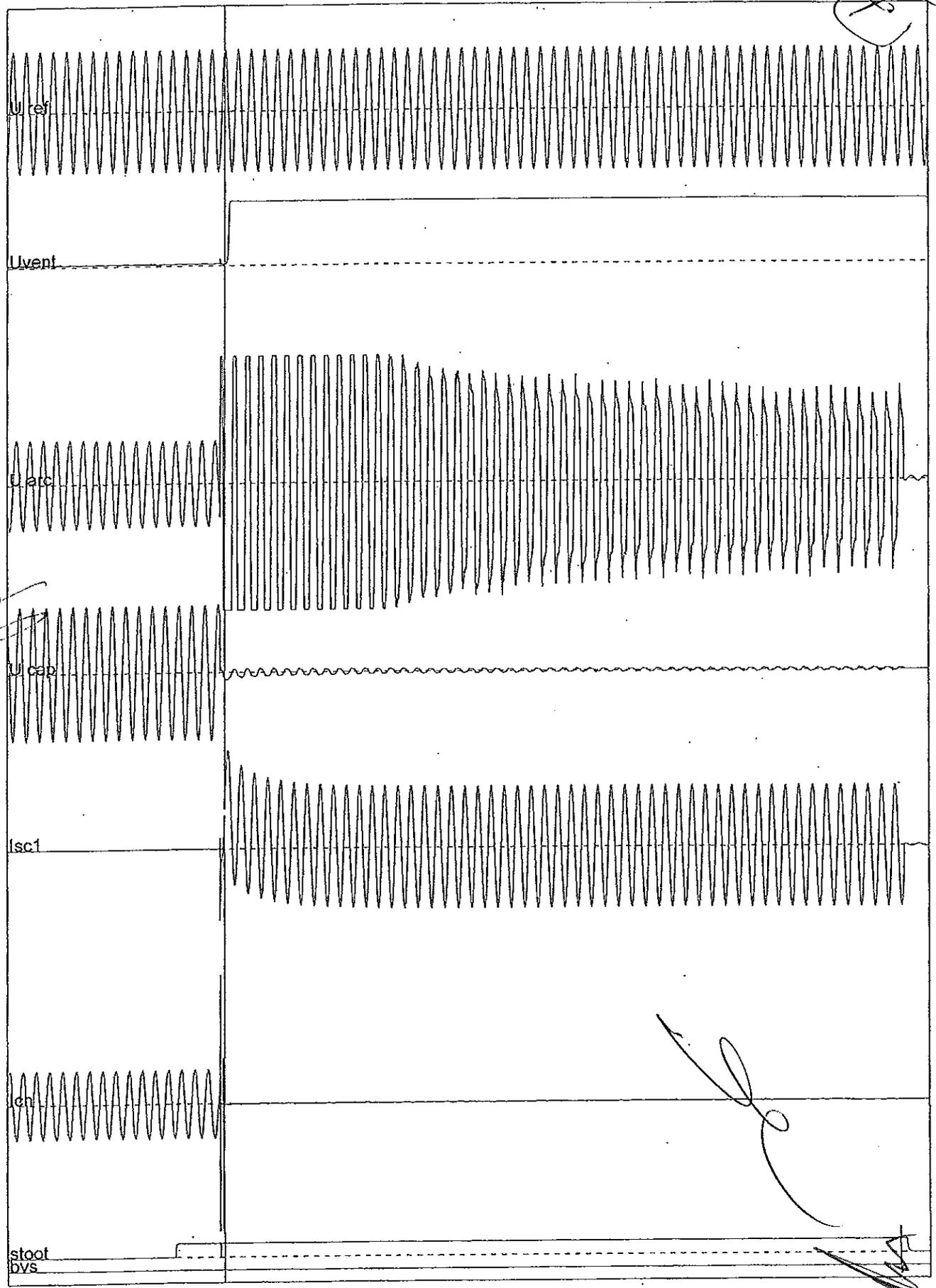
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000167

ВЕРНО  
ОРИГИНАЛ





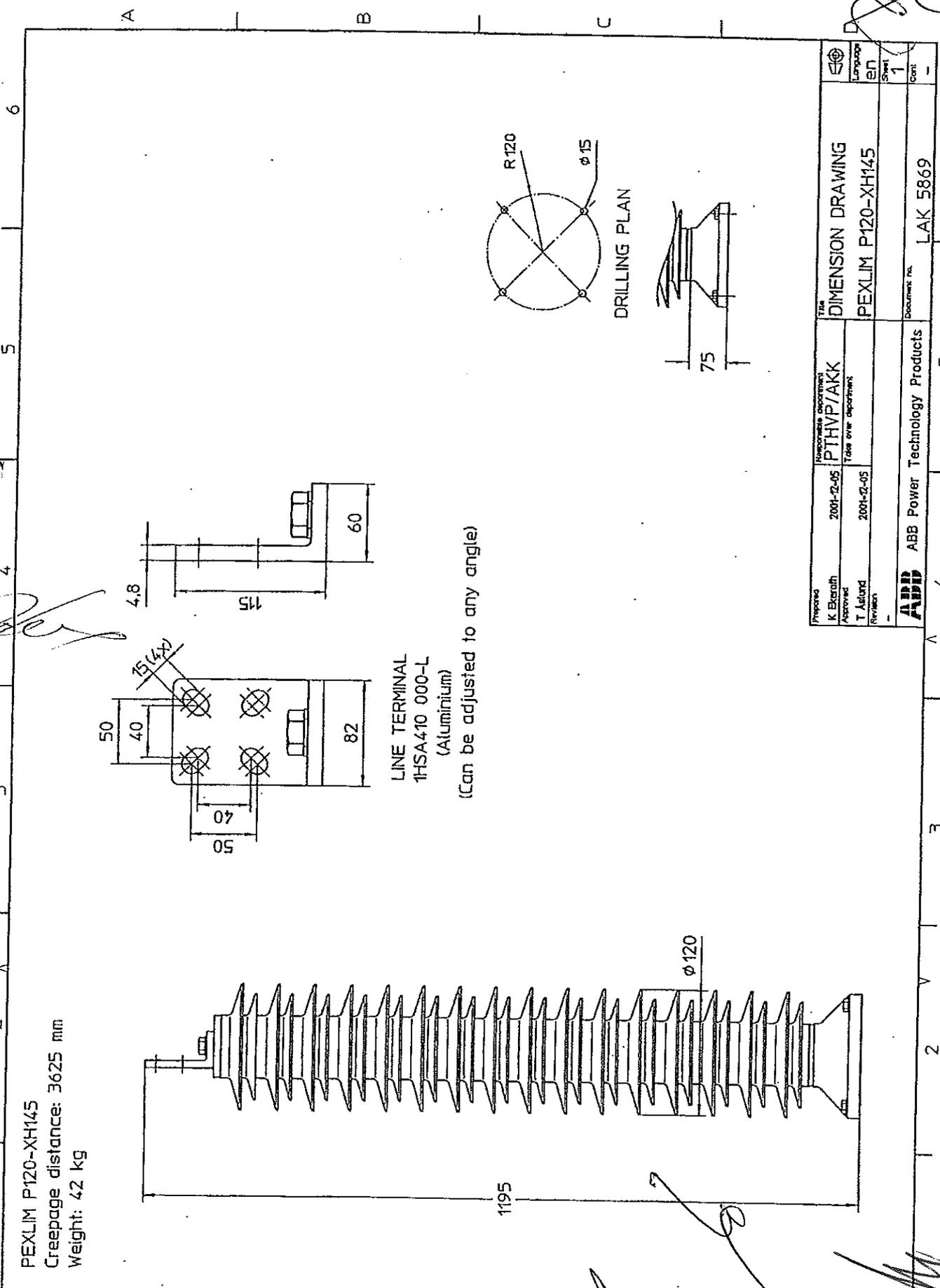
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ВЕРНО С  
ОРИГИНАЛА



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LINE TERMINAL  
1HSA410 000-L  
(Aluminium)  
(Can be adjusted to any angle)

PEXLIM P120-XH145  
Creepage distance: 3625 mm  
Weight: 42 kg

Prepared K. Blazhich	2001-12-05	Approved T. Astlund	2001-12-05	Checked -	2001-12-05
Title DIMENSION DRAWING		Language en			
Part name PTHVP/AKK		Sheet 1			
Task Take over department		Cont. -			
Author ABB		Document no. LAK 5869			
Product ABB Power Technology Products		Drawing no. LAK 5869			

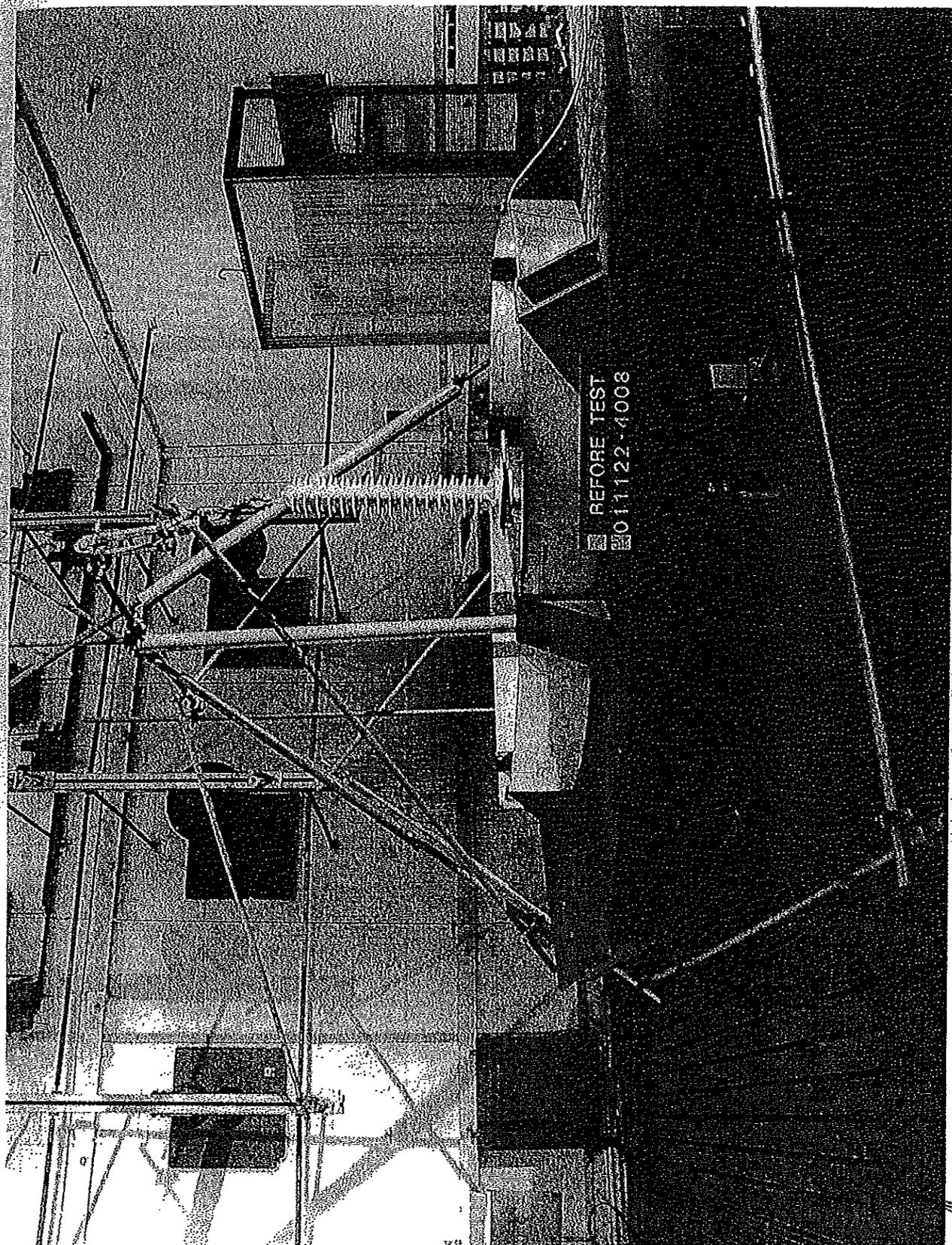
The document is issued by means of a computerized system. The digital signed copy is electronically approved. The approved document for a date entered in the 'Approved-Date' field. A manual signature is not required.

000169

ВЯРНІС  
ОРИГІНАЛ



1415201

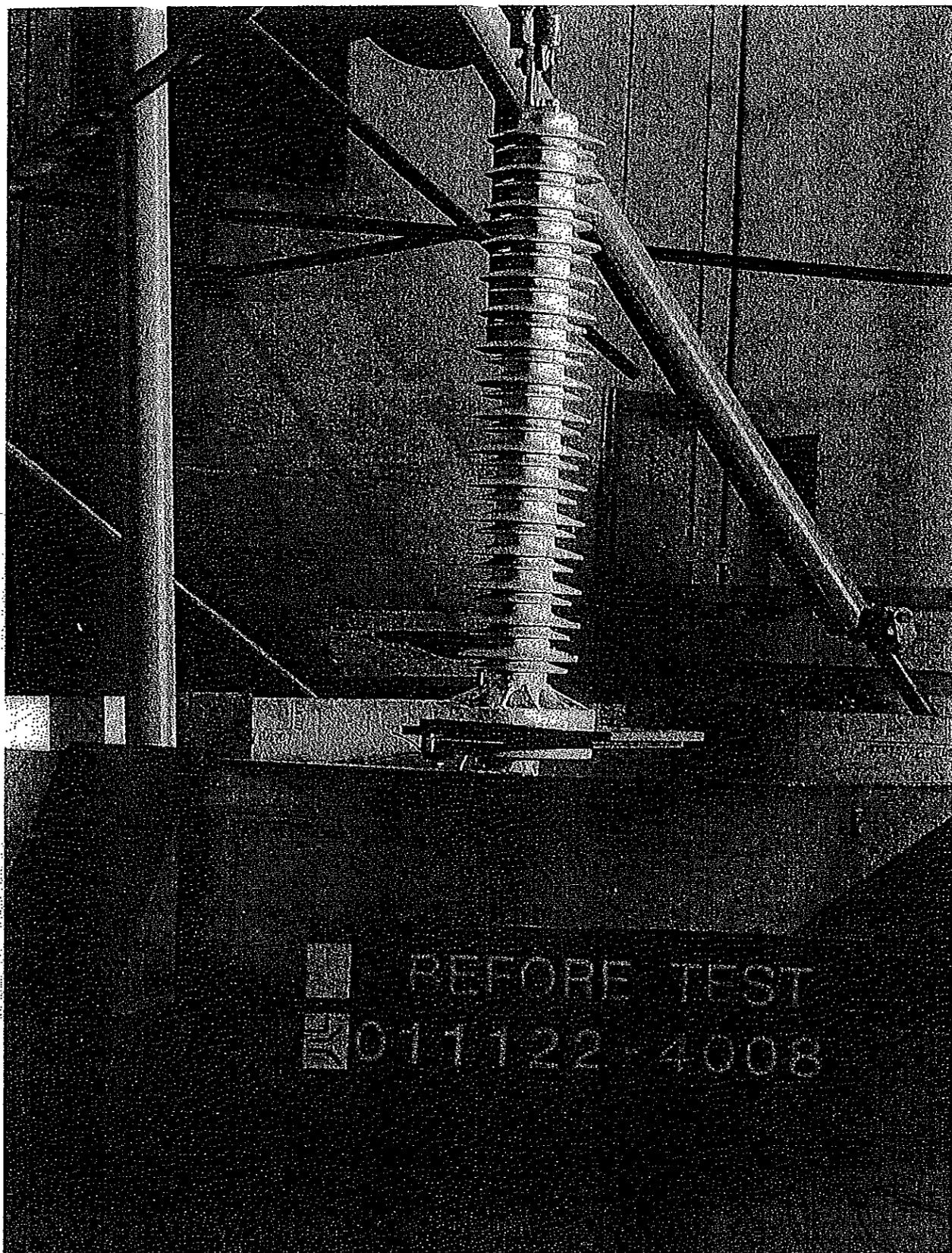


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000170

ВЯРНІС  
ОРИГІНАЛ

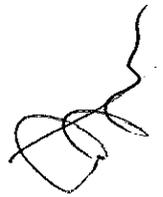




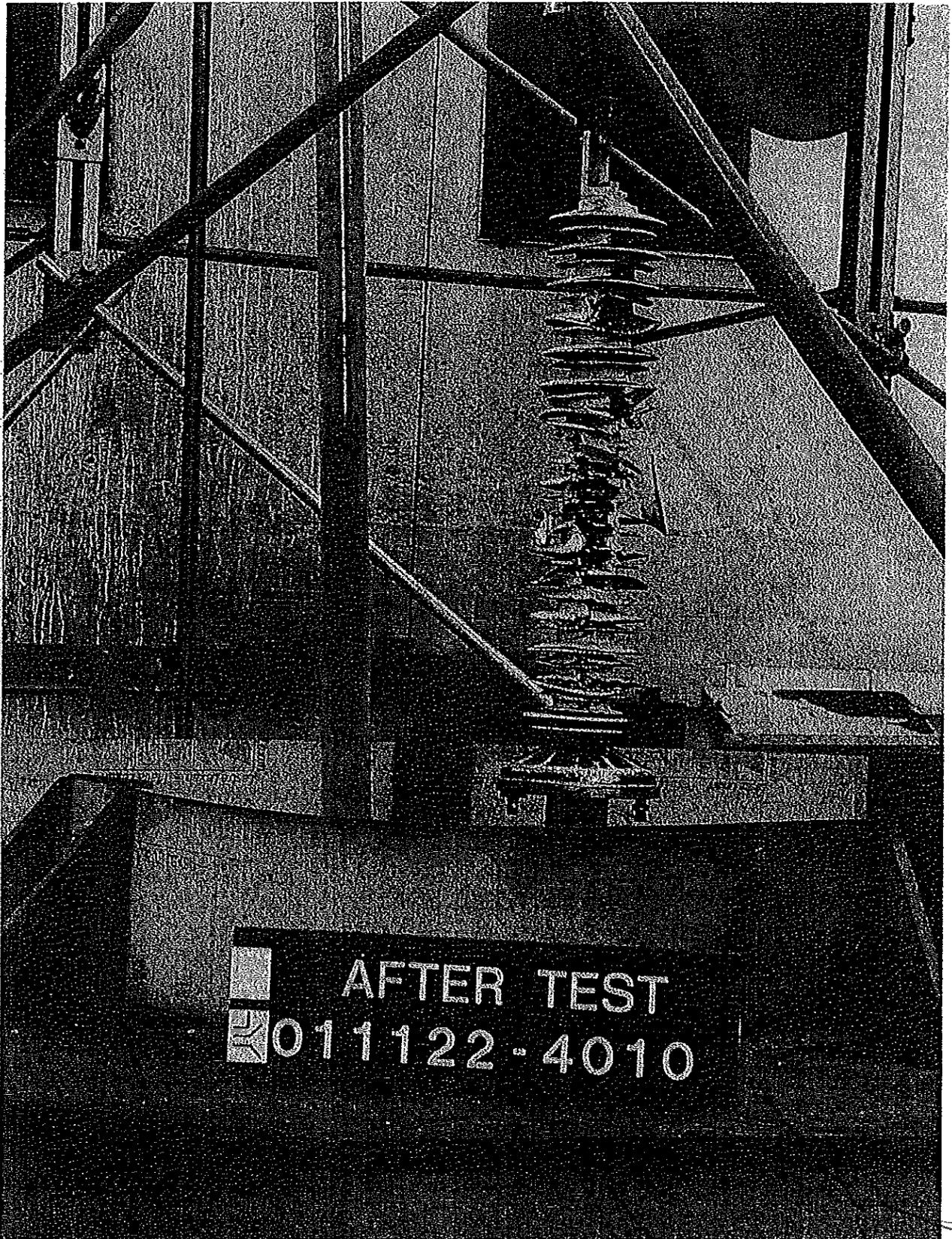
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ВЯРНО С  
ОРИГИНАЛА





1415203



AFTER TEST  
011122-4010

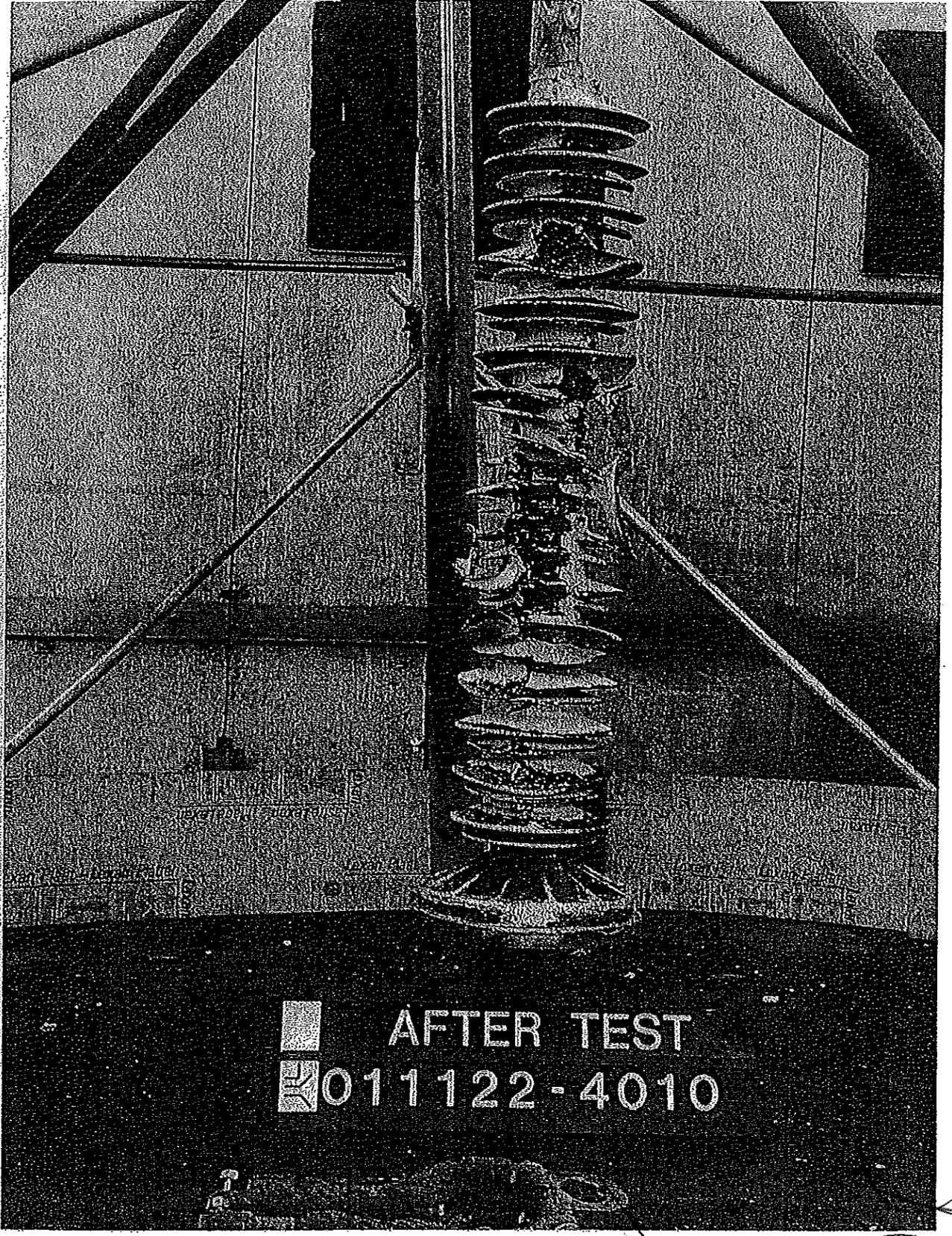
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000172

ВЯРНО С  
ОРИГИНАЛА



1415204



 AFTER TEST  
 011122-4010

 000173  
1

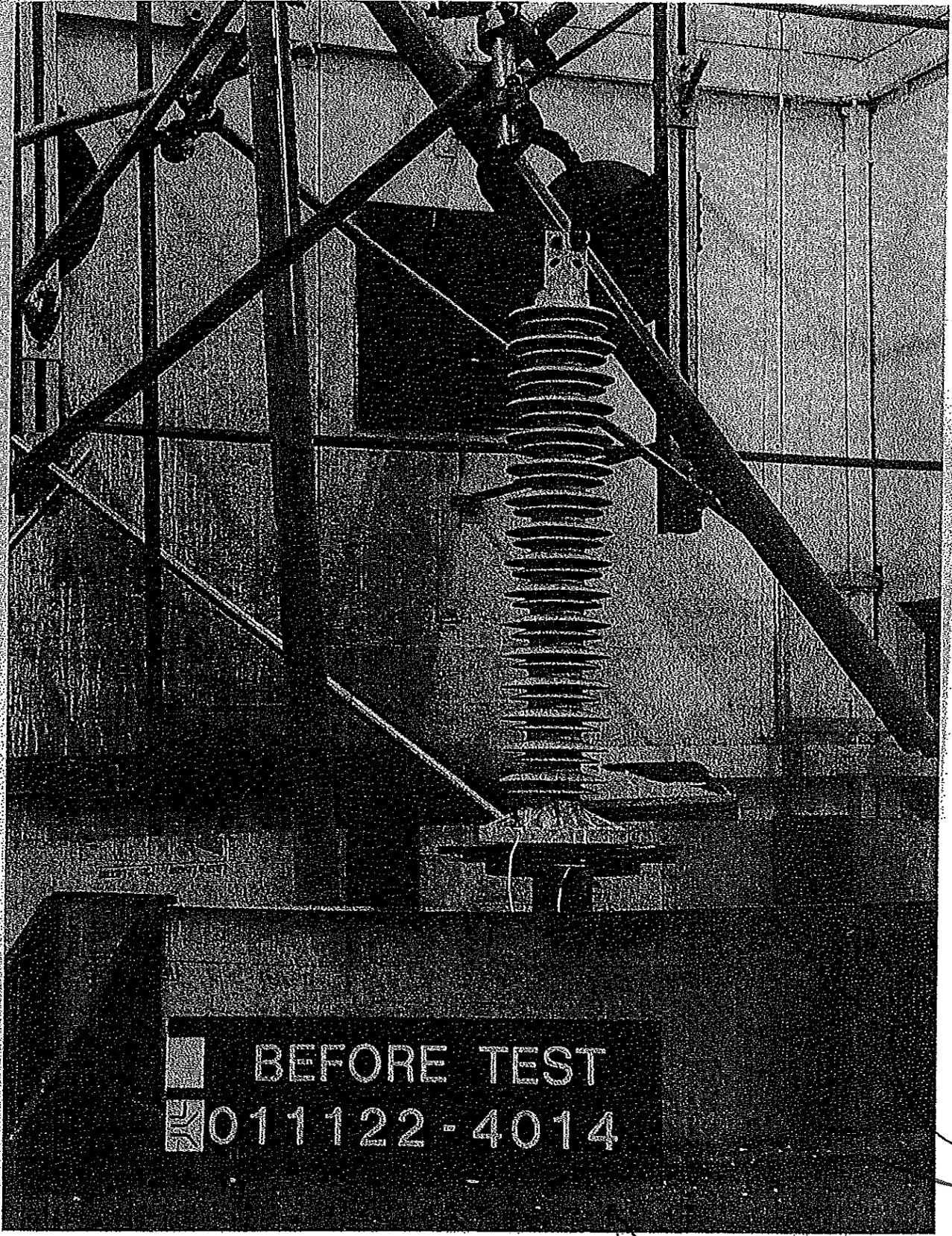
~~ВЯРНІС  
ОРИГІНАЛА~~

«КРАСИН»  
СМОЛЯН  
ООД

КЕМА

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1415205



BEFORE TEST  
011122 - 4014

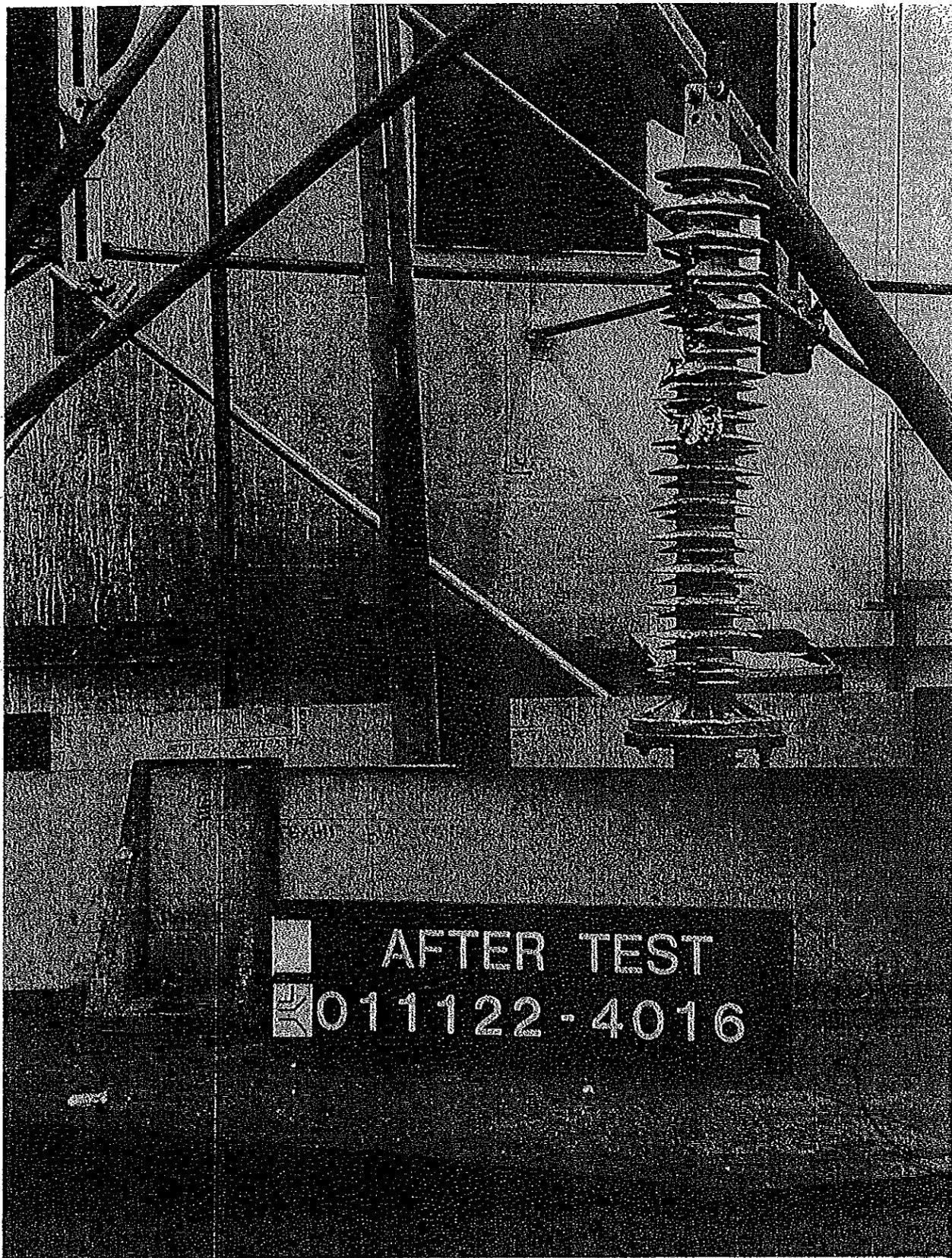
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ВЯРНО С  
ОРИГИНАЛА



1415206



AFTER TEST  
011122-4016

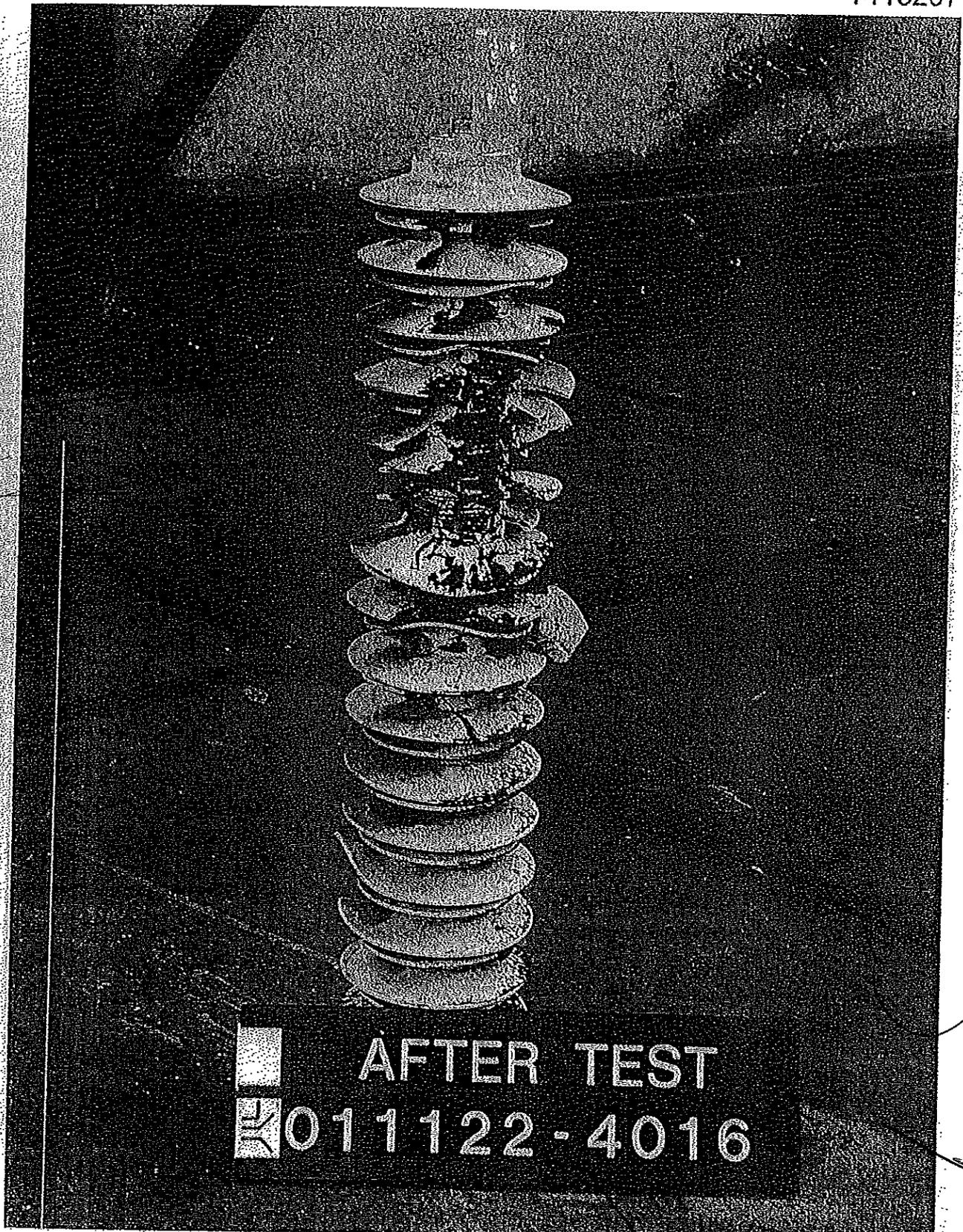
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ВЯРНО С  
ОРИГИНАЛА



KEMA

1415207



AFTER TEST  
011122-4016

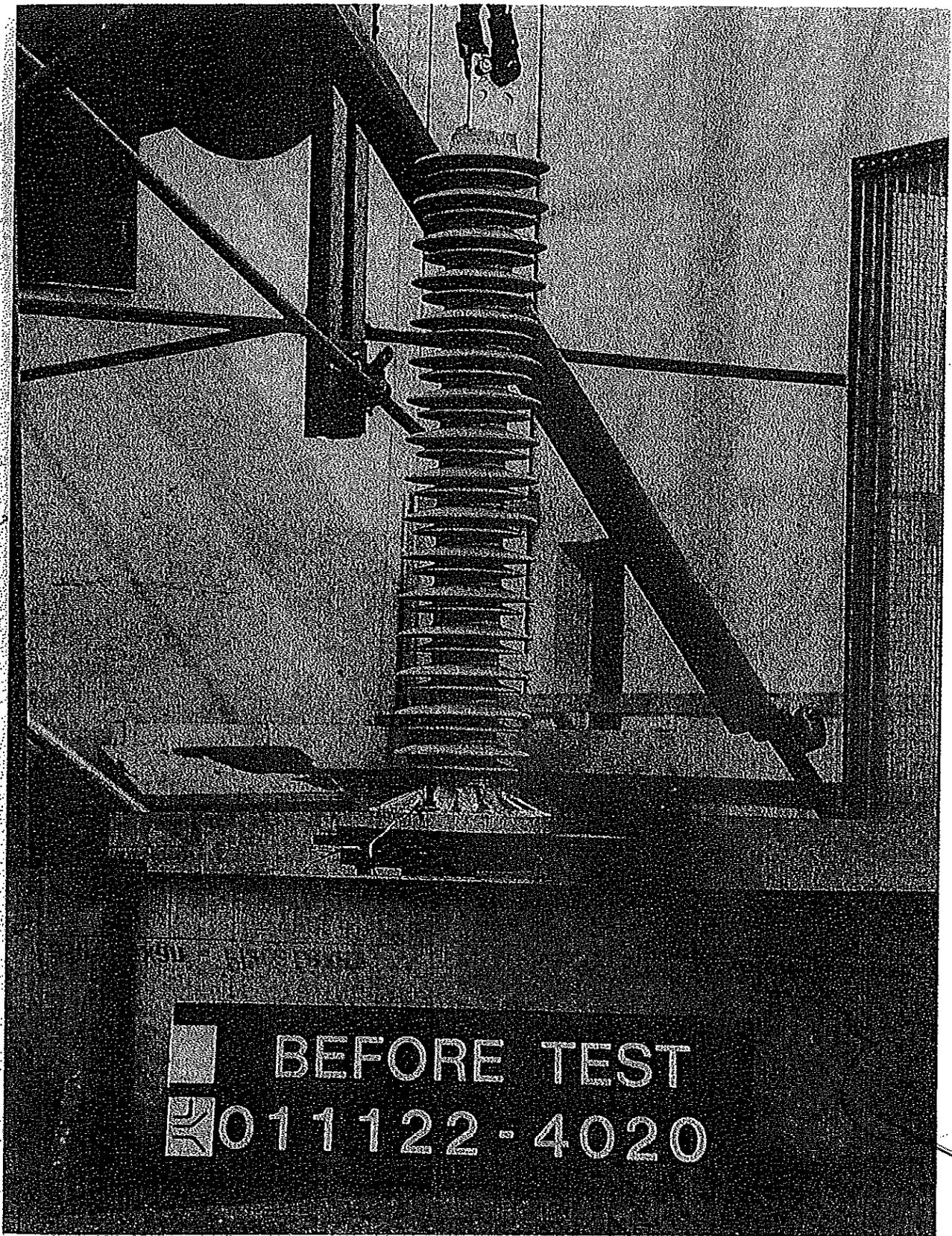
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ВЯРНОС  
ОРИГИНАЛ



КЕМА

1415210



BEFORE TEST  
011122-4020

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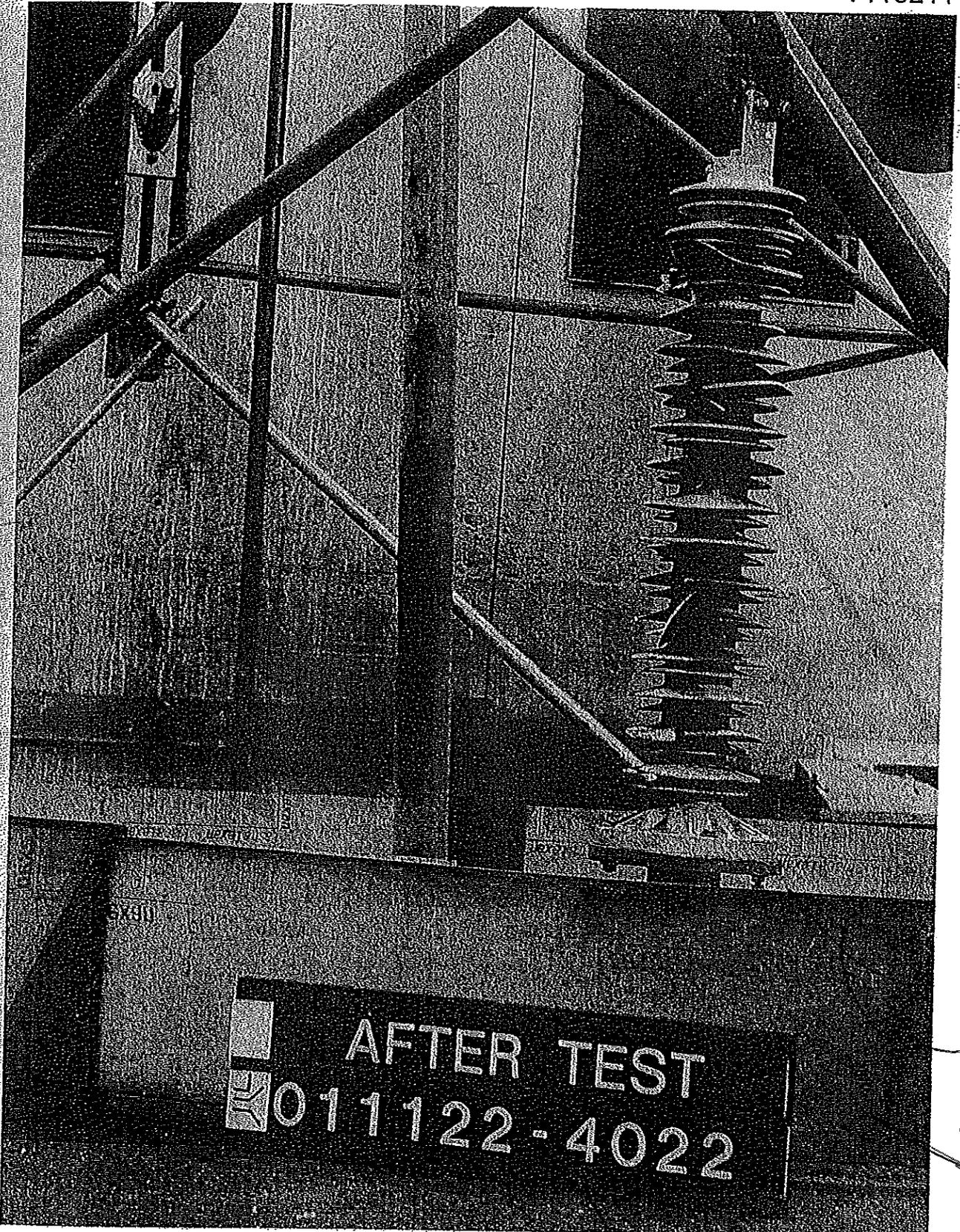
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БЯРС С  
ОРИГИНАЛ



KEMA

1415211



AFTER TEST  
 011122-4022

*Handwritten signatures and initials.*

000178

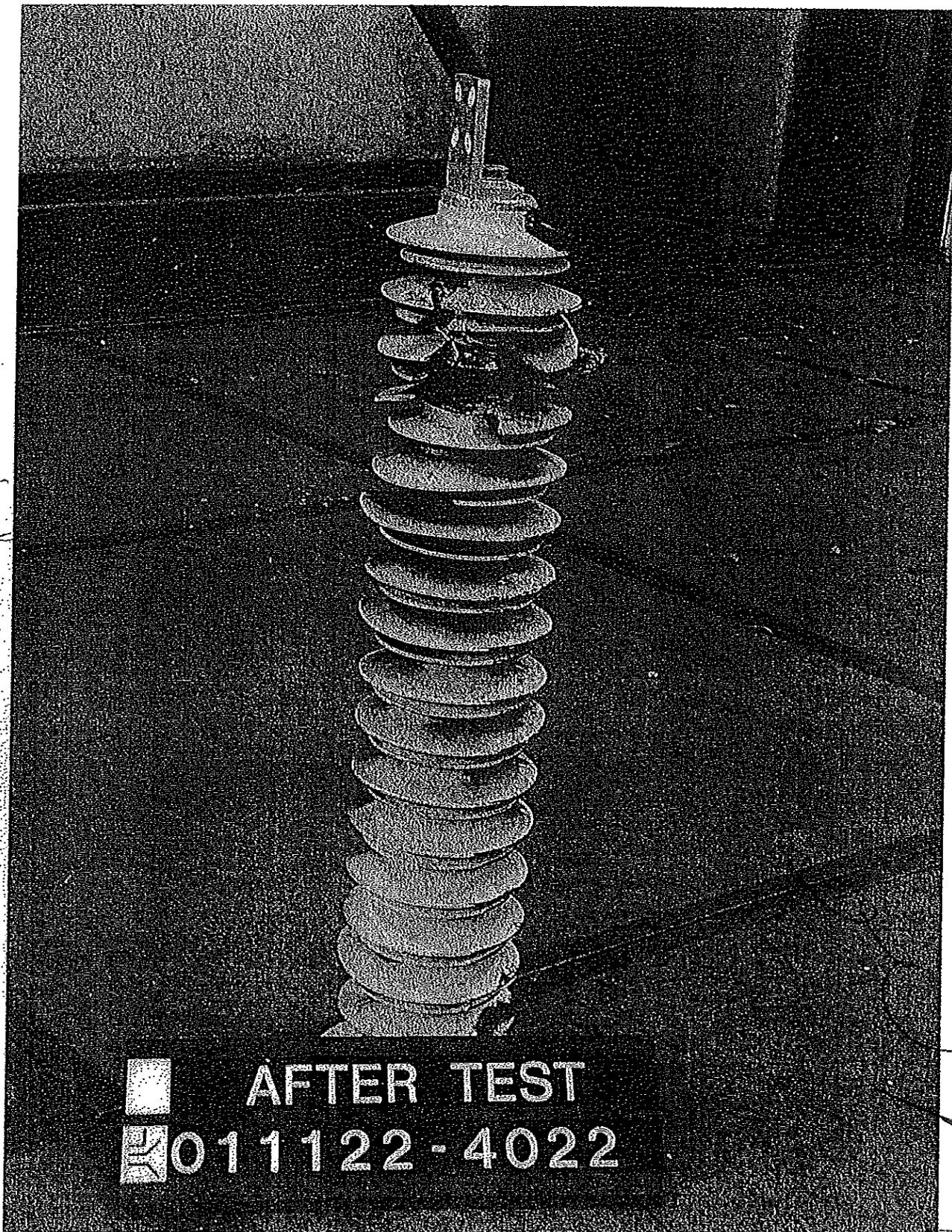
ВЯРНО С  
 ОРИГИНАЛА



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1415212



 AFTER TEST  
 011122-4022

*[Handwritten signature]*

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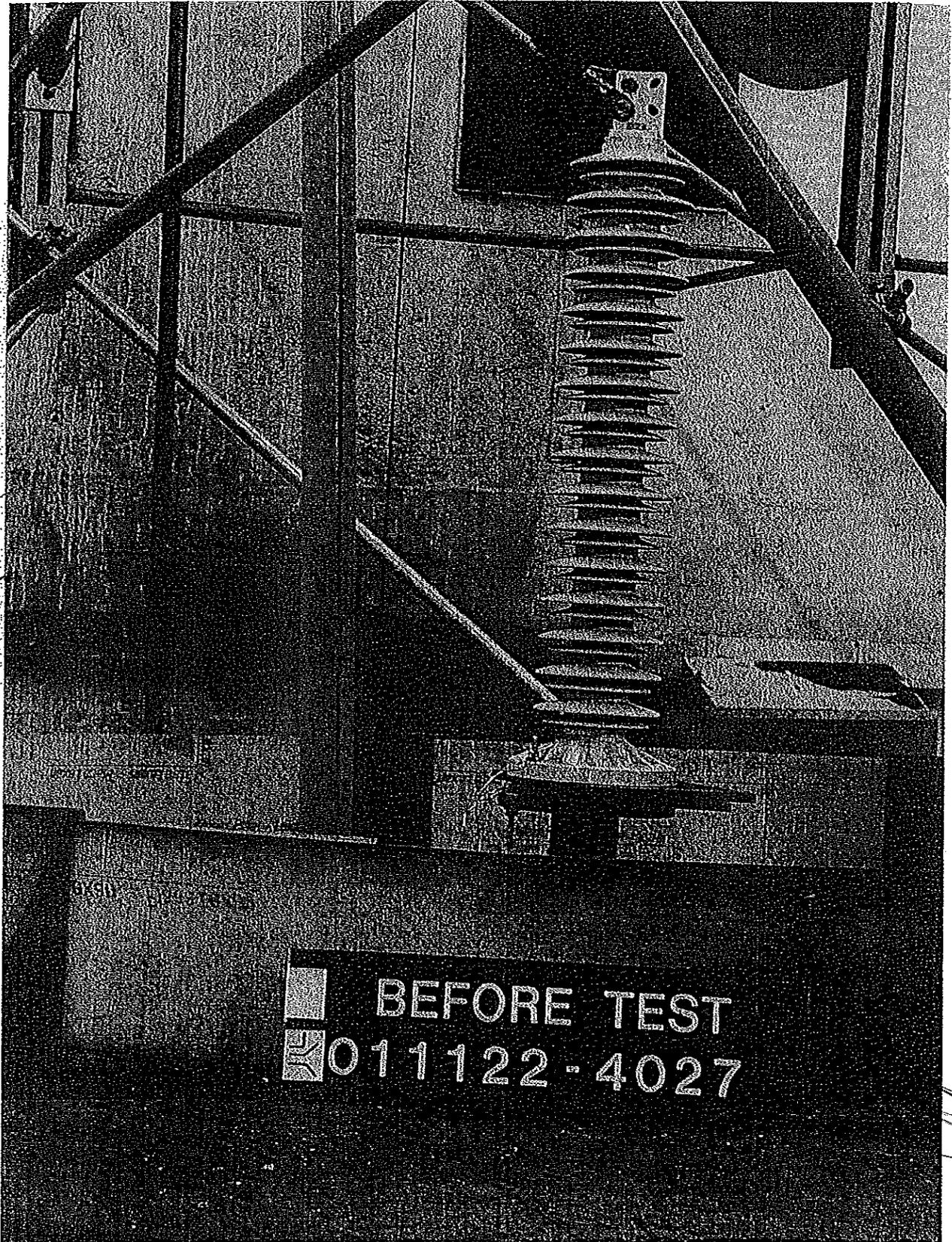
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ВЯРНО С  
 ОРИГИНАЛА



*[Handwritten signature]*

1415214



BEFORE TEST  
 011122-4027

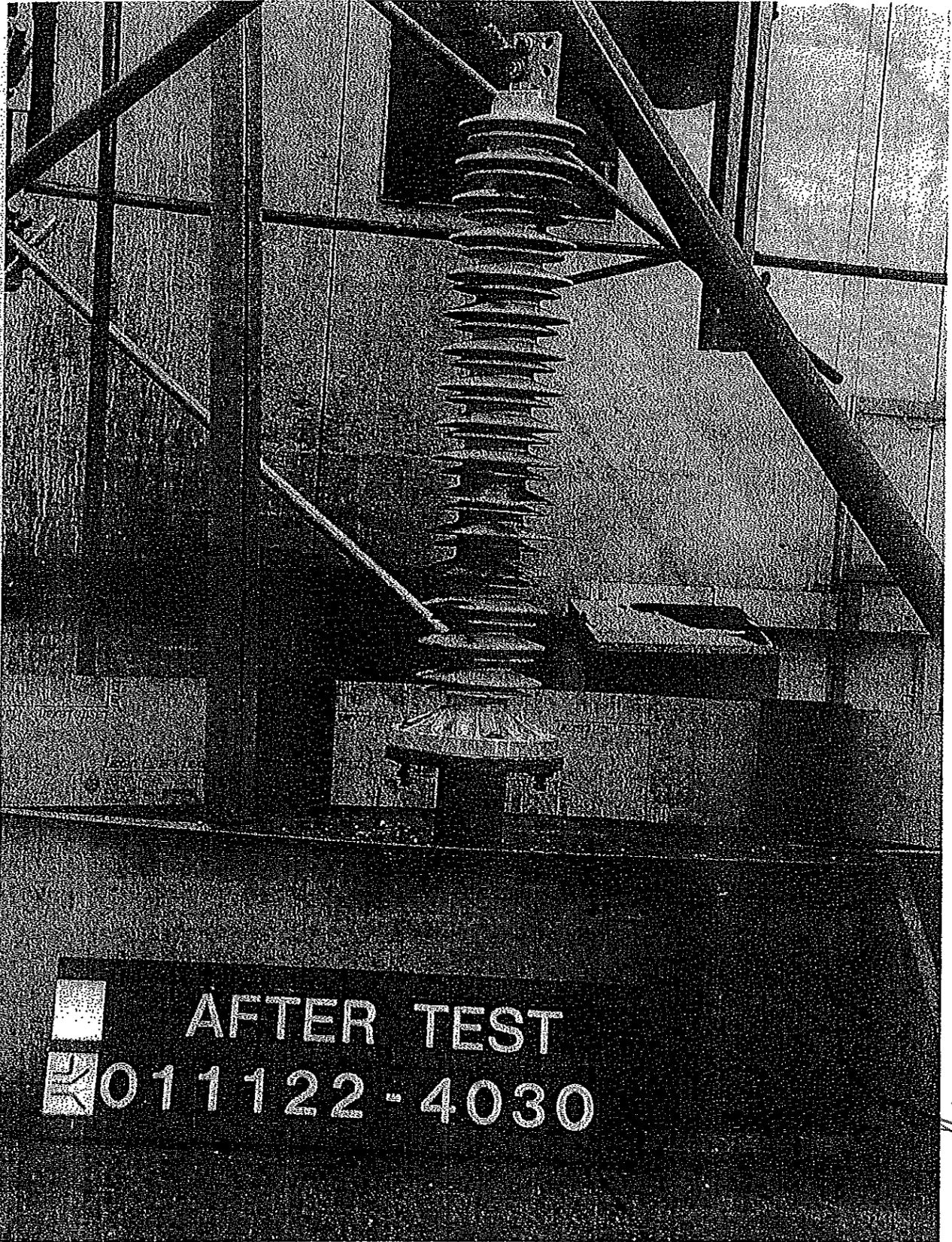
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ВЯНДС  
 ОРИГИНАЛ



1415215

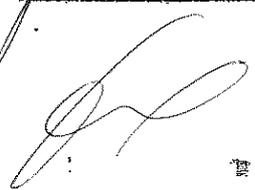


 AFTER TEST  
 011122-4030

000181

ВЯНО С  
ОРИГНАЛА







## 1 Certificate

A Certificate contains a record of a series of type tests carried out strictly in accordance with a recognized standard. The equipment tested has fulfilled the requirements of this standard and the relevant ratings assigned by the manufacturer are endorsed by KEMA. The Certificate is applicable only to the equipment tested. KEMA is responsible for the validity and the contents of the Certificate.

The responsibility for conformity of any apparatus having the same designation as the one tested rests with the manufacturer. The Certificate contains the essential drawings and a description of the equipment tested.

Detailed rules are given in KEMA's Certification procedure.

## 2 Report of Performance

A Report of Performance contains a record of one or more tests which have been carried out according to the client's instructions. These tests are not necessarily in accordance with a recognized standard. The test results do not verify ratings of the test object.

KEMA issues three types of Reports of Performance:

**2.1** *The tests have been carried out strictly in accordance with .... The apparatus has complied with the relevant requirements.*

This sentence will appear on the front page of a Report of Performance if the tests have been performed in accordance with a recognized standard, but the series of tests does not completely fulfil the requirements for a Certificate of Compliance (for example, if the number of test duties is not a complete series of type tests).

The Report contains verified drawings and a description of the equipment tested. Detailed rules are given in KEMA's Certification procedure. The condition of the test object after the tests is assessed and recorded in the Report.

**2.2** *The tests have been carried out in accordance with the client's instructions. Test procedure and test parameters were based on ....*

This sentence will appear on the front page of a Report of Performance if the number of tests, the test procedure and the test parameters are based on a recognized standard and related to the ratings assigned by the manufacturer. If the apparatus does not pass the tests such behaviour will be mentioned on the front sheet. Verification of the drawings (if submitted) and assessment of the condition after the tests is only done on the client's request.

**2.3** *The tests have been carried out according to the client's instructions.*

This sentence will appear on the front page of a Report of Performance if the tests, test procedure and/or test parameters are not in accordance with a recognized standard.

## 3 Standards

When reference is made to a standard, and the date of issue is not stated, this applies to the latest issue, including amendments which have been officially published prior to the date of the tests.

## 4 Official and uncontrolled test documents

The official test documents of KEMA High-Power Laboratory are issued in bound form. Uncontrolled copies may be provided as loose sheets for convenience of reproduction by the client. The copyright has to be respected at all times.

## 5 Accuracy of measurement

In the table of test results the measured quantities are given in three digits. This method of presentation does not indicate an accuracy. The guaranteed uncertainty in the figures mentioned, taking into account the total measuring system, is less than 5%, unless mentioned otherwise.

## 6 Qualified by STERLAB

KEMA High-Power Laboratory has been entered in the STERLAB register for laboratories under Nr. L 020 for the testing services as defined in the Field of Accreditation.

The accreditation is carried out in accordance with IESO/IEC 17025.



000182



## Type tests on PEXLIM P Surge Arresters

Test objects: Surge arrester modules rated 36, 72 and 120 kV with the ZnO blocks replaced by insulating material

Standards: IEC 60099-4, first edition 1991-11  
IEC 60060-1, second edition 1989-11  
ANSI/IEEE Std C62.11-1993  
ANSI/IEEE Std 4-1978

Tests performed: Insulation withstand tests

Test report: Q 99-281

Validation: The test objects initially represented arrester modules used for arrester type PEXLIM Q. However, the physical dimensions for the modules used for arrester type PEXLIM P-X are identical. The test results, therefore, also are valid for arresters of type PEXLIM P-X.

Tests completed: 1999-10-21

Tests performed at: ABB Transformers AB/High Voltage Laboratory

Report consists of: 37 pages (Report Q 99-281, 36 pages)

We hereby certify that the objects specified above have successfully passed the test herein reported, thereby verifying guaranteed data.

Ludvika 2002-01-08

ABB Power Technology Products AB  
High Voltage Products/Surge Arresters  
Quality Department

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на основание чл. 2 от ЗЗЛД



Kurt Jansson

ABB Power Technology Products AB

000183



# ABB TRANSFORMERS AB

на основании чл. 2 от 33ЛД

Report

R Q 99-281

Författare-Author  
Mikael Gärdskog

Datum-Date Reg.  
99-10-29

Reg.  
5680

Sida-Page  
1

Godkännare-Approved  
Bengt Jönsson  
Uppdrags- SWG/AK

на основании чл. 2 от 33ЛД

teoretisk  
Ökning-Analys  
ical Investigation  
ig, experim. under-  
-Test, experi-  
Investigation  
ort-Interim Report

Ordnummer-Ref.No.  
6771.24407 UP6, project 970002  
Debiteras ordnummer  
#

PKI/AKI

Titel-Title  
Dielectric  
surge ar

Antal textsidor-No. of pages  
33

Antal bilagesidor-No. of supplm. pages  
3

## TYPE TESTS

Slutrapport-Final report

Proving/undersökning avslutad  
Test investigation finished  
99-10-21

## Sammanfattning-Summary

### TEST OBJECT

Three empty surge arrester modules

1. PEXLIM Q36/R36, Document no. LAK 5476      Supplem. Page 1.
2. PEXLIM Q72/R72, Document no. LAK 5477      Supplem. Page 2.
3. PEXLIM Q120/R120, Document no. LAK 5478      Supplem. Page 3.

### PERFORMED TESTS

- Full lightning impulse withstand voltage test, dry
- Switching impulse withstand voltage test, wet
- Power frequency withstand voltage test, dry and wet

### APPLIED STANDARDS

IEC 99-4, first edition 1991-11, IEC 60-1, second edition 1989-11  
ANSI/IEEE Std C62.11-1993, ANSI/IEEE Std 4-1978

### RESULTS

The following withstand voltage levels were achieved (corrected for atmospheric conditions).

	PEXLIM Q36/R36 Withstand voltage level (kV)	PEXLIM Q72/R72 Withstand voltage level (kV)	PEXLIM Q120/R120 Withstand voltage level (kV)
1,2/50 $\mu$ s, dry, ANSI / IEC	283	400	578
250/2500 $\mu$ s, wet, IEC	242	330	462
50 Hz, wet, IEC	126	187	293
60 Hz, wet, ANSI	126	187	293
60 Hz, dry, ANSI	136	200	316

Distribution  
SETFO/T-arkiv SWG/AKB

Enbart sida 1-Page 1 only  
SETFO/Q-arkiv

Nyckelord /Ämnesord-Key words

Övriga nyckelord

Arkiveringsstid Q

- 1 år  
 2 år  
 mer än 3 år

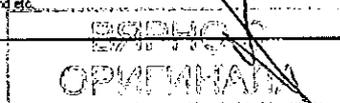
Anm. Nyckelord/Ämnesord används när rapporten skrivs på svenska.

"Keywords" används när rapporten skrivs på engelska

Övriga nyckelord används endast i undantagsfall och avser t. ex. materialbeteckning, produktutveckling, leverantör, kund etc.

Se för övrigt ZQ:TA 990-101

000184



1  
TEST OBJECT

Three empty surge arrester modules

- 1. PEXLIM Q36/R36, Document no. LAK 5476      Supplem. Page 1.
- 2. PEXLIM Q72/R72, Document no. LAK 5477      Supplem. Page 2.
- 3. PEXLIM Q120/R120, Document no. LAK 5478      Supplem. Page 3.

During the test the arrester housings were placed on a platform 1 m above the floor (ground level)

2  
ATMOSPHERIC CONDITIONS

Date 99-09-14	Date 99-09-29	Date 99-08-26
t= 19 °C	t= 20 °C	t= 23 °C
h= 38 %	h= 50 %	h= 33 %
b= 752 mmHg	b= 728 mmHg	b= 749 mmHg

Date 99-09-15	Date 99-10-20	Date 99-10-21
t= 23 °C	t= 21 °C	t= 21 °C
h= 39 %	h= 27 %	h= 27 %
b= 749 mmHg	b= 756 mmHg	b= 755 mmHg

3  
TESTS

3.1 Full lightning impulse withstand voltage test, 1,2/50 µs, dry      According to IEC Standard

The test was carried out by the up and down method for determination of the U<sub>50%</sub> disruptive discharge voltage, positive polarity.

Number of applied impulses, 30.      dU= 3%.

The withstand voltage was determined by application of 15 impulses of both positive and negative polarity at a voltage 3% lower than the achieved U<sub>50%</sub> voltage level.

The table below shows the obtained results (corrected for atmospheric conditions).

K= 1.00, applied at the test.

	Date 99-09-14	Date 99-09-29	Date 99-08-26
1,2/50 µs, dry, ANSI / IEC	PEXLIM Q36/R36	PEXLIM Q72/R72	PEXLIM Q120/R120
	U <sub>50%</sub> disruptive discharge	U <sub>50%</sub> disruptive discharge	U <sub>50%</sub> disruptive discharge
Corrected (kV)	Kt=0.969 291.5	Kt=0.940 412	Kt=0.940 595
	Withstand voltage level	Withstand voltage level	Withstand voltage level
Corrected (kV)	Kt=0.969 283	Kt=0.940 400	Kt=0.940 578

000185

ВЕРИФИКАЦИЯ  
ОРИГИНАЛА



**3.2**

Switching impulse withstand voltage test, wet, 250/2500  $\mu$ s According to IEC Standard

The test was carried out by the up and down method for determination of the  $U_{50\%}$  disruptive discharge voltage, positive polarity.

Number of applied impulses, 30,  $dU = 3\%$ .

The withstand voltage was determined by application of 15 impulses of both positive and negative polarity at a voltage 3-6% lower than the achieved  $U_{50\%}$  voltage level.

The table below shows the obtained results (corrected for atmospheric conditions).  
 $K = 1.00$ , applied at the test.

	Test date 99-09-15	Test date 99-10-20	Test date 99-10-20
<b>250/2500 <math>\mu</math>s, wet, IEC</b>	<b>PEXLIM Q36/R36</b>	<b>PEXLIM Q72/R72</b>	<b>PEXLIM Q120/R120</b>
	U50% disruptive discharge	U50% disruptive discharge	U50% disruptive discharge
Corrected (kV)	K1=0.976 249	K1=0.991 341	K1=0.991 491
	Withstand voltage level	Withstand voltage level	Withstand voltage level
Corrected (kV)	K1=0.976 242	K1=0.940 330	K1=0.991 462
Precipitation rate: (horizontal/vertical)	1,8/1,6 mm/min,	1,0/1,6 mm/min,	1,3/1,3 mm/min,
Resistivity of water:	100 $\Omega$ m	95 $\Omega$ m	95 $\Omega$ m

**3.3**

Power frequency withstand voltage test, 50 Hz, 60s, wet. According to IEC Standards

Power frequency withstand voltage test, 60 Hz, 10s, wet. According to ANSI/IEEE Standards

Power frequency withstand voltage test, 60 Hz, 60s, dry. According to ANSI/IEEE Standards

The table below shows the obtained results (corrected for atmospheric conditions).

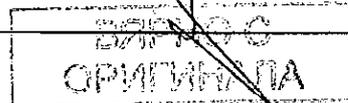
$K = 1.00$ , applied at the test.

	Test date 99-10-20	Test date 99-10-20	Test date 99-10-20
<b>50 Hz, wet, IEC</b>	<b>PEXLIM Q36/R36</b>	<b>PEXLIM Q72/R72</b>	<b>PEXLIM Q120/R120</b>
	Withstand voltage level	Withstand voltage level	Withstand voltage level
Corrected (kV)	K1=0.991 126	K1=0.992 187	K1=0.991 293
Precipitation rate: (horizontal/vertical)	1,2/1,4 mm/min,	1,3/1,3 mm/min,	1,3/1,3 mm/min,
Resistivity of water:	95 $\Omega$ m	95 $\Omega$ m	95 $\Omega$ m

	Test date 99-10-21	Test date 99-10-21	Test date 99-10-21
<b>60 Hz, wet, ANSI/IEEE</b> Std 4-1978, 1.3.3.2, table 1.2, Practice in USA	<b>PEXLIM Q36/R36</b>	<b>PEXLIM Q72/R72</b>	<b>PEXLIM Q120/R120</b>
	Withstand voltage level	Withstand voltage level	Withstand voltage level
Corrected (kV)	K1=0.990 126	K1=0.991 187	K1=0.990 293
Precipitation rate:	5.0 mm/min,	4.7 mm/min,	4.5 mm/min,
Resistivity of water:	180 $\Omega$ m	180 $\Omega$ m	180 $\Omega$ m

	Test date 99-10-21	Test date 99-10-21	Test date 99-10-21
<b>60 Hz, dry, ANSI/IEEE</b>	<b>PEXLIM Q36/R36</b>	<b>PEXLIM Q72/R72</b>	<b>PEXLIM Q120/R120</b>
	Withstand voltage level	Withstand voltage level	Withstand voltage level
Corrected (kV)	K1=0.919 136	K1=0.923 200	K1=0.919 316

000186



Test Record

Test date 15 Sep 1999

Serial nbr. R27

IMPULSE VOLTAGE TEST

MEASUREMENTS

LIGHTNING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage 300kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	275	1.20/52	1
100	274	1.20/52	2
100	274	1.20/12	3
100	274	1.21/52	4
100	274	1.20/52	5
100	274	1.20/52	6
100	274	1.20/52	7
100	273	1.21/52	8
100	274	1.20/52	9
100	274	1.20/52	10
100	274	1.19/52	11
100	273	1.19/52	12
100	275	1.21/52	13
100	274	1.21/52	14
100	274	1.20/52	15

LIGHTNING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage -300kV.

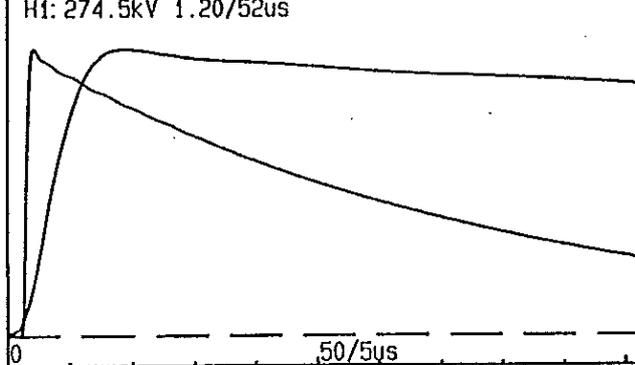
Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	-274	1.21/52	16
100	-274	1.21/52	17
100	-274	1.21/52	18
100	-274	1.21/52	19
100	-274	1.20/52	20
100	-274	1.21/52	21
100	-274	1.20/52	22
100	-274	1.20/52	23
100	-274	1.21/52	24
100	-274	1.20/52	25
100	-274	1.20/52	26
100	-274	1.20/52	27
100	-274	1.20/52	28
100	-274	1.21/52	29
100	-274	1.21/52	30

000187

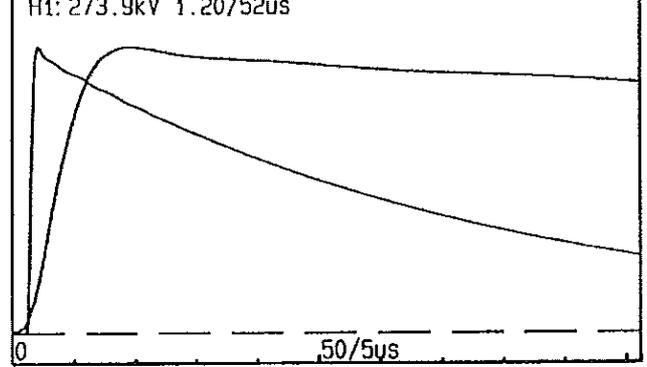
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ОРИГІНАЛ



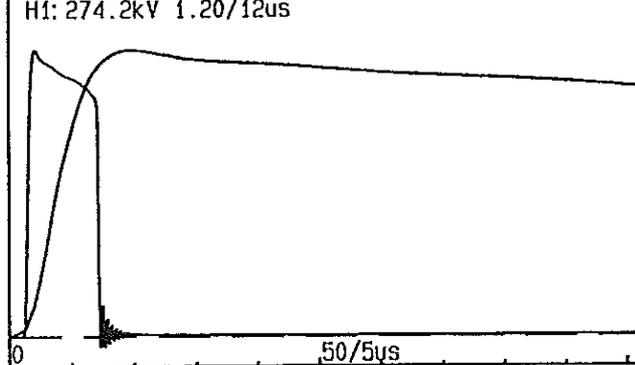
No: 1 Lightning impulse 100%



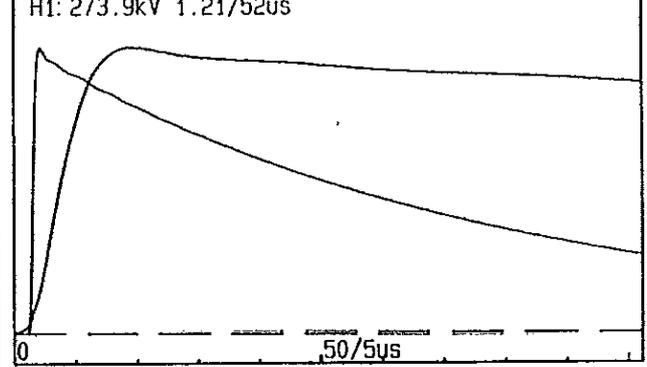
No: 2 Lightning impulse 100%



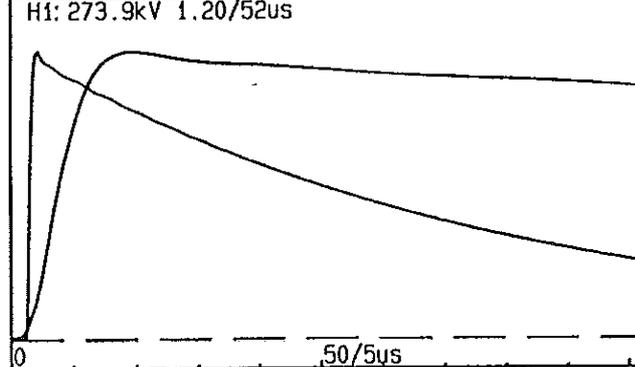
No: 3 Lightning impulse 100%



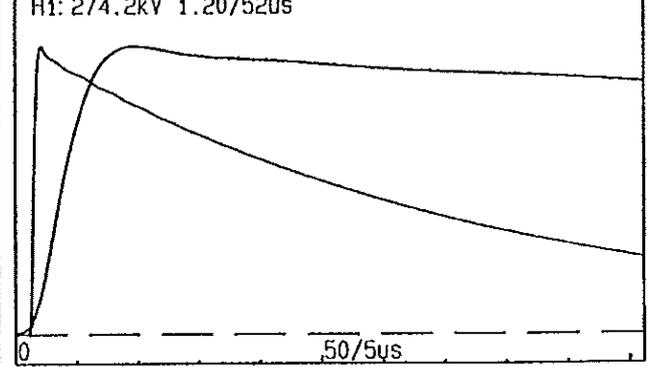
No: 4 Lightning impulse 100%



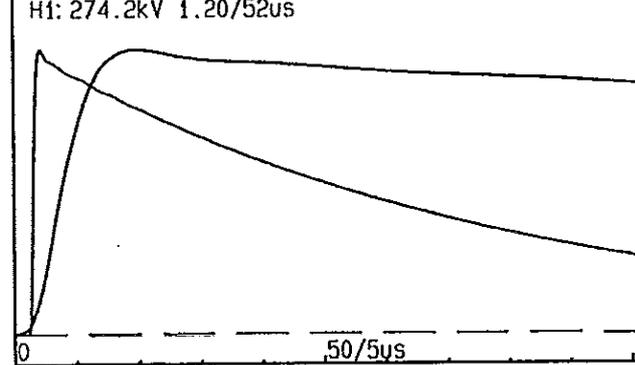
No: 5 Lightning impulse 100%



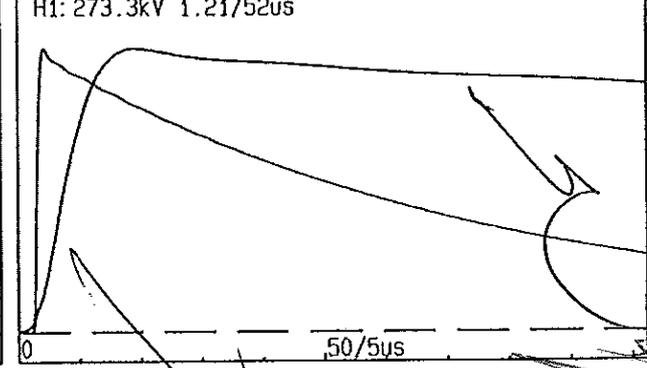
No: 6 Lightning impulse 100%



No: 7 Lightning impulse 100%



No: 8 Lightning impulse 100%



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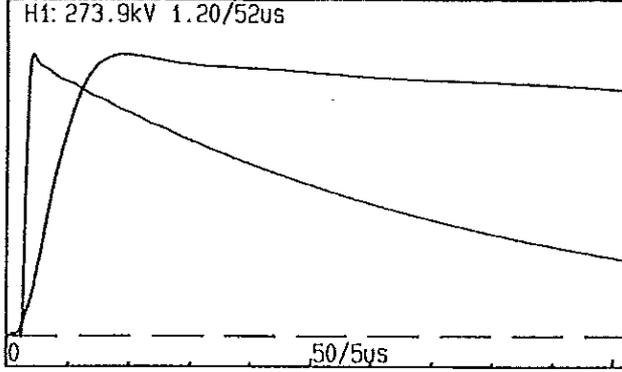
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ОРИГИНАЛ

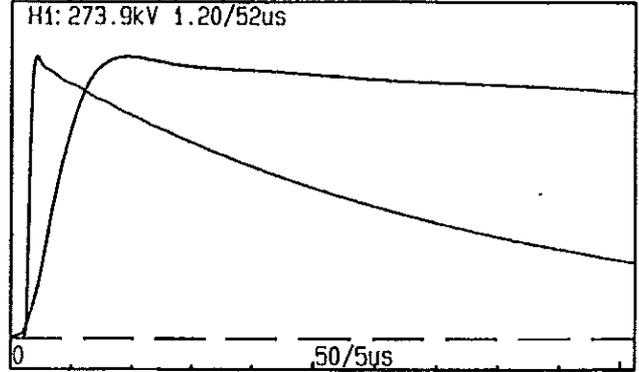


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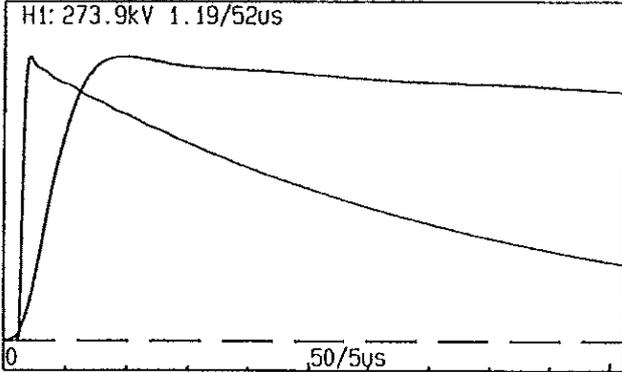
No: 9 Lightning impulse 100%



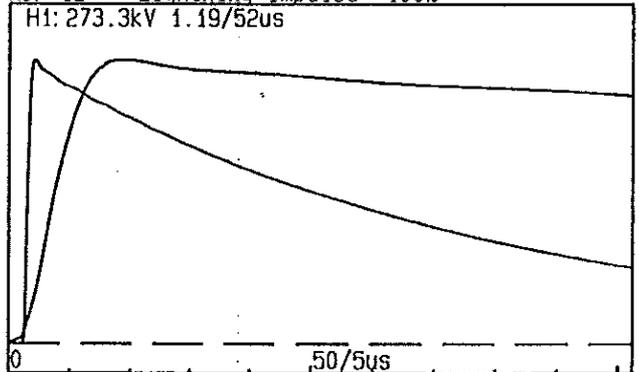
No: 10 Lightning impulse 100%



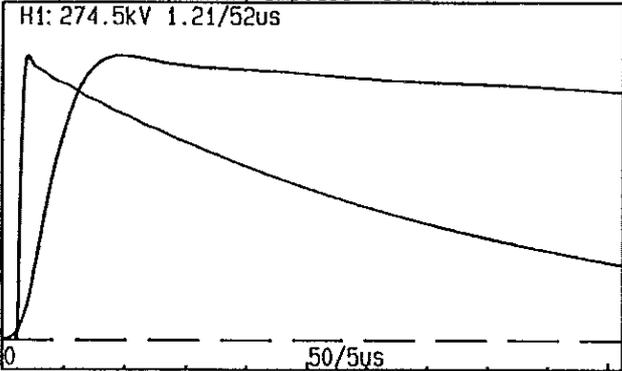
No: 11 Lightning impulse 100%



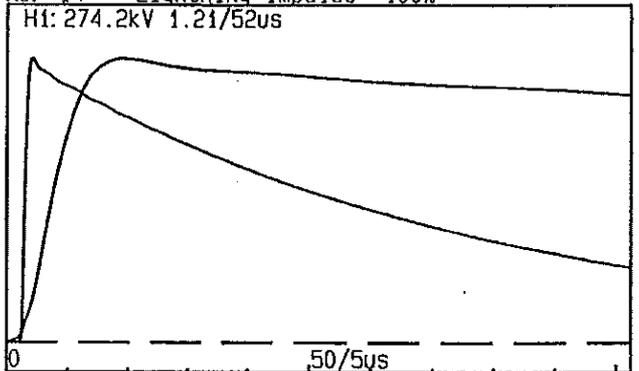
No: 12 Lightning impulse 100%



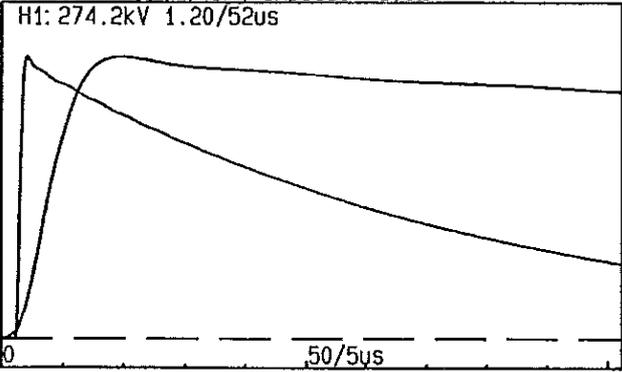
No: 13 Lightning impulse 100%



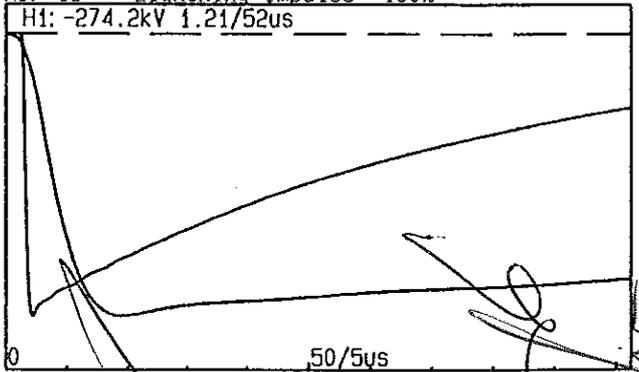
No: 14 Lightning impulse 100%



No: 15 Lightning impulse 100%



No: 16 Lightning impulse 100%



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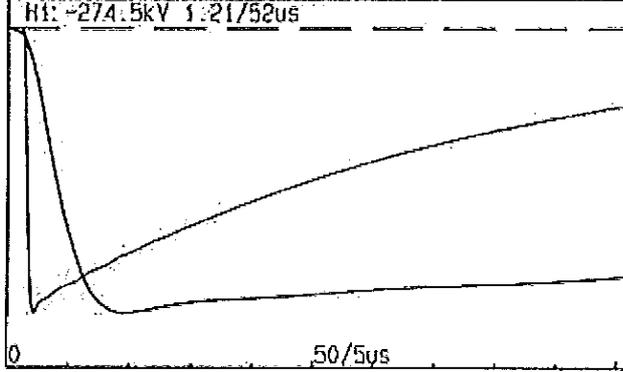
000189

ВЯРНО С  
ОРИГИНАЛА

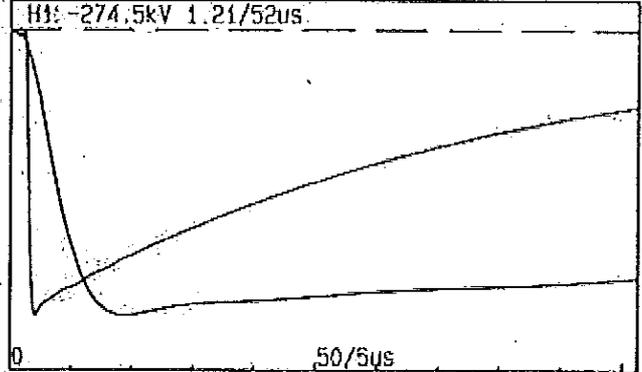


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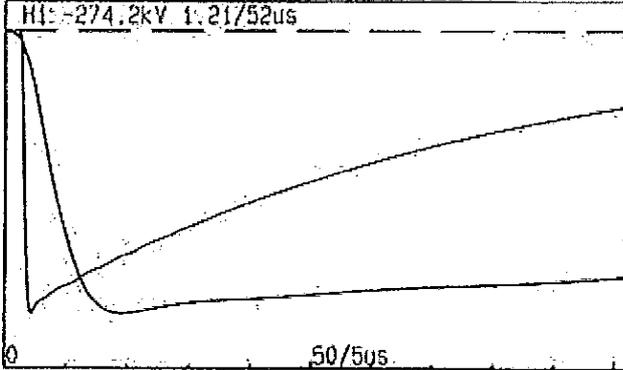
No: 17 Lightning impulse 100%



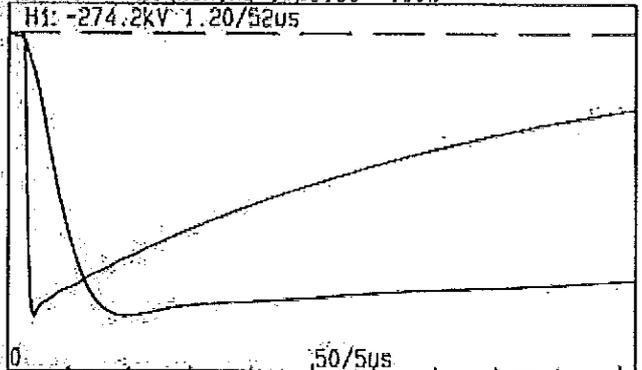
No: 18 Lightning impulse 100%



No: 19 Lightning impulse 100%

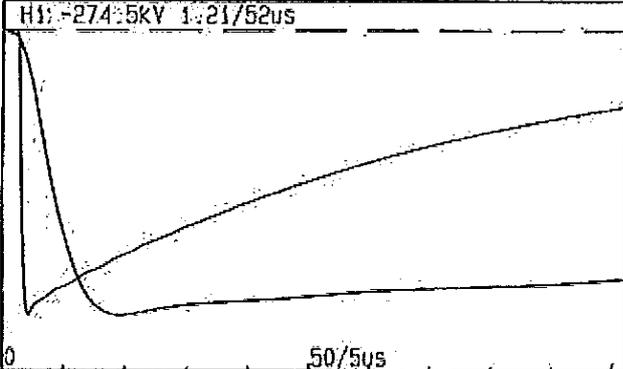


No: 20 Lightning impulse 100%

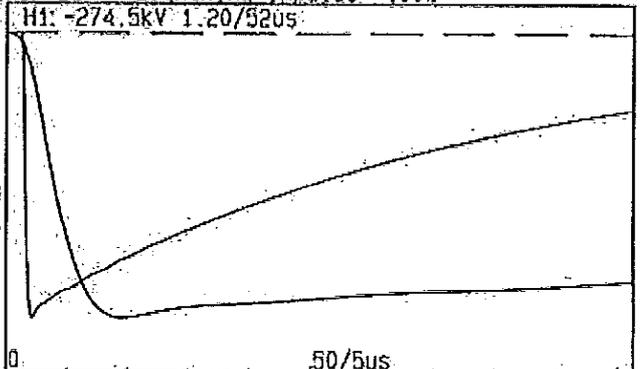


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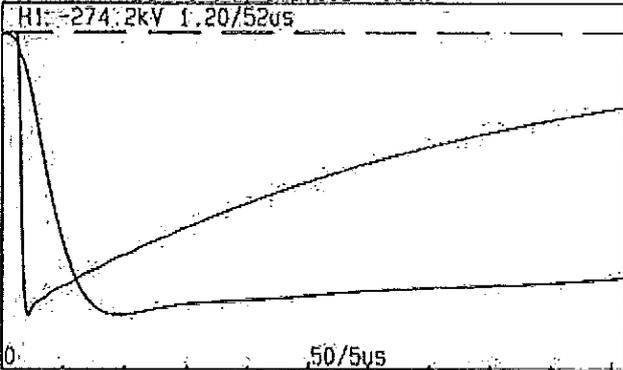
No: 21 Lightning impulse 100%



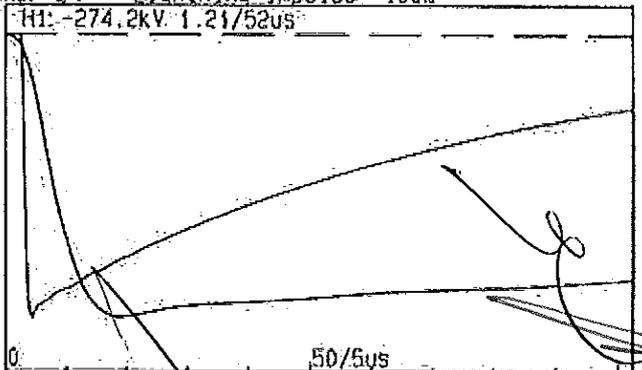
No: 22 Lightning impulse 100%



No: 23 Lightning impulse 100%



No: 24 Lightning impulse 100%

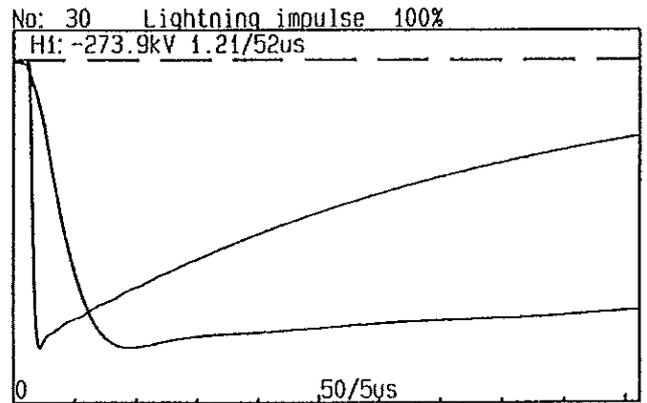
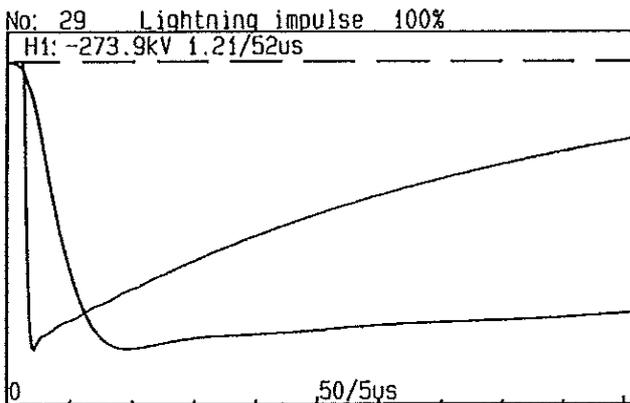
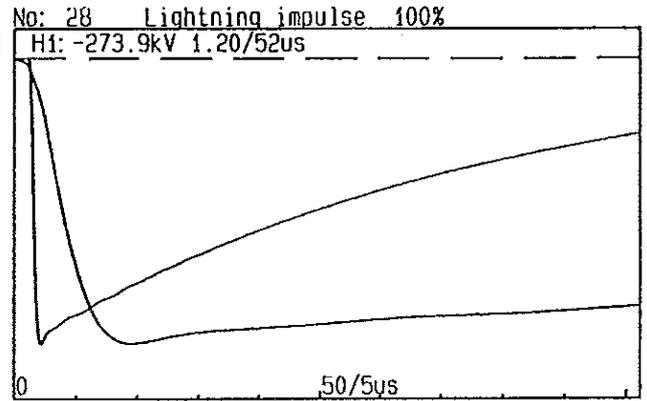
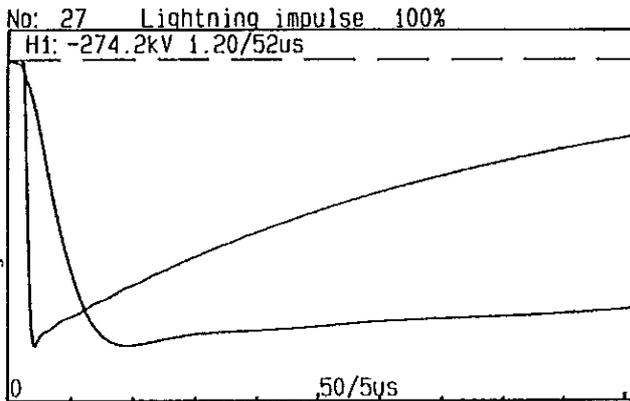
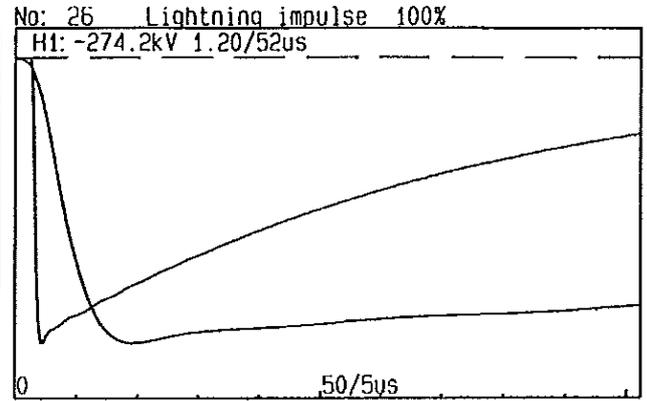
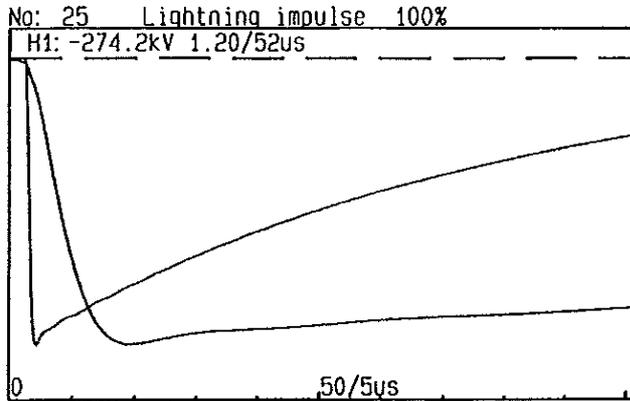


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000190

ВЯРНО С  
ОРИГИНАЛА





000191

ВРАНО С  
ОРИГИНАЛА



**Test Record**

Test date : 15 Sep 1999

Serial nbr. : R27

**IMPULSE VOLTAGE TEST**

**MEASUREMENTS**

SWITCHING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage 250kV.

Amplitude %	kV	Impulse shape µs	Oscillogram number
100	238	248/1544	31
100	237	247/1551	32
100	237	256/1548	33
100	237	252/1548	34
100	237	259/1549	35
100	237	259/1549	36
100	236	245/1549	37
100	236	247/1549	38
100	236	250/1548	39
100	236	250/1549	40
100	236	253/299	41
100	236	259/1550	42
100	236	251/1552	43
100	236	252/384	44
100	236	248/1549	45

SWITCHING IMPULSE VOLTAGE TEST on terminal H1.  
Nominal test voltage -250kV.

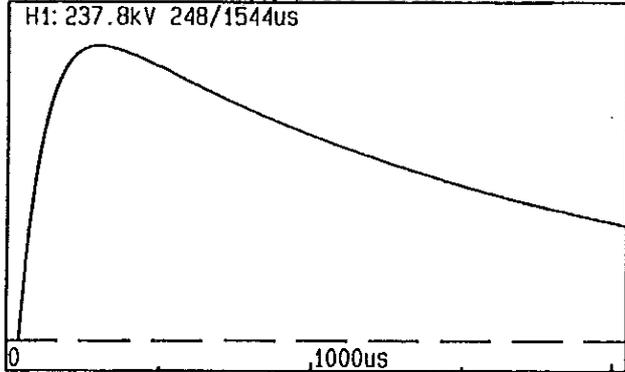
Amplitude %	kV	Impulse shape µs	Oscillogram number
100	-236	261/1546	46
100	-235	243/1548	47
100	-236	250/1546	48
100	-236	248/1547	49
100	-236	252/1546	50
100	-236	251/1548	51
100	-236	249/1546	52
100	-236	255/1546	53
100	-236	239/1549	54
100	-236	256/1546	55
100	-236	244/1548	56
100	-236	257/1545	57
100	-236	244/1545	58
100	-236	243/1543	59
100	-236	259/1547	60

000192

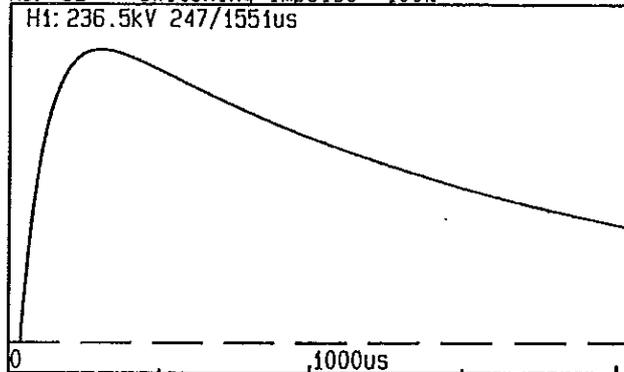
ВЕРНО С  
ОРИГИНАЛА



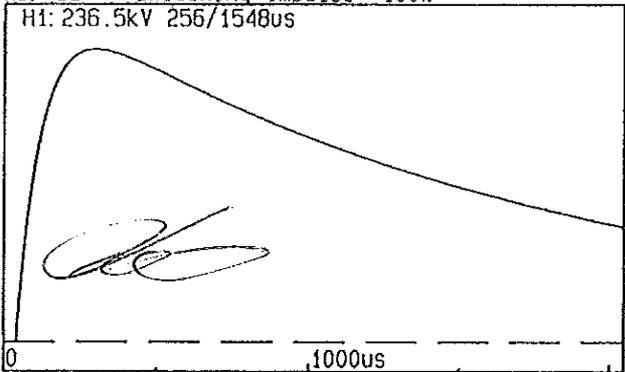
No: 31 Switching impulse 100%



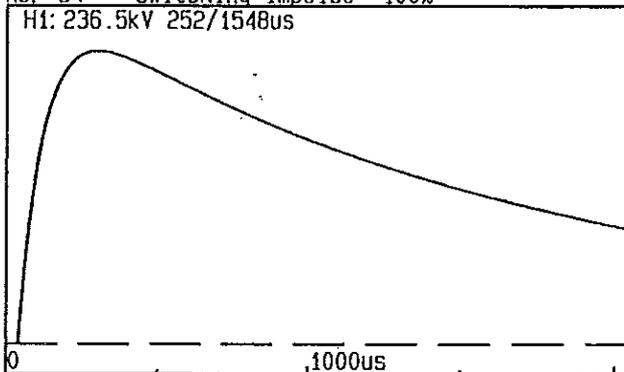
No: 32 Switching impulse 100%



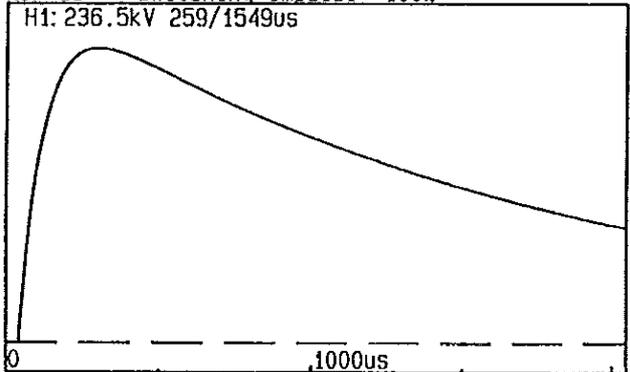
No: 33 Switching impulse 100%



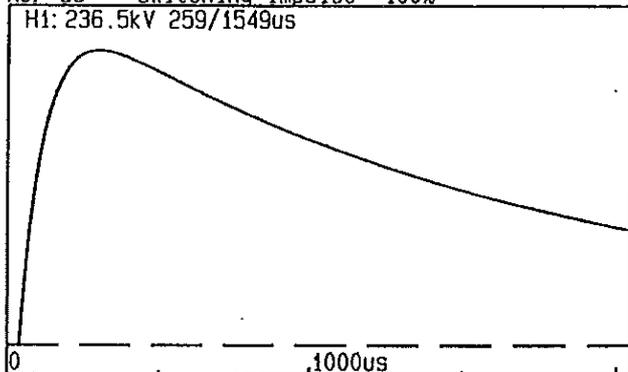
No: 34 Switching impulse 100%



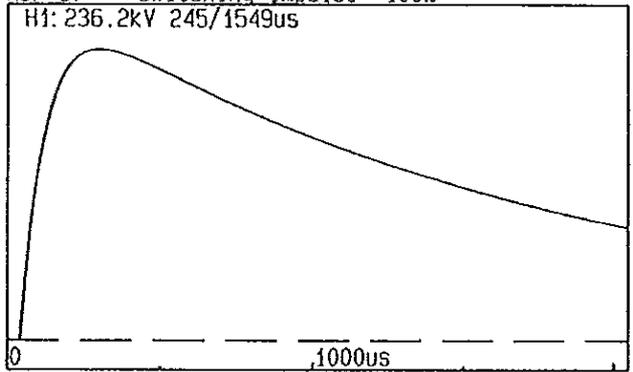
No: 35 Switching impulse 100%



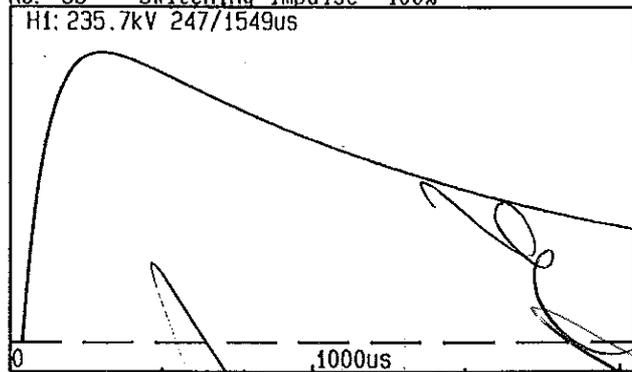
No: 36 Switching impulse 100%



No: 37 Switching impulse 100%



No: 38 Switching impulse 100%

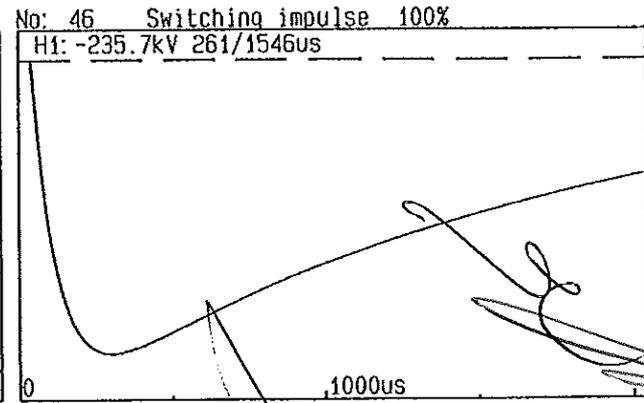
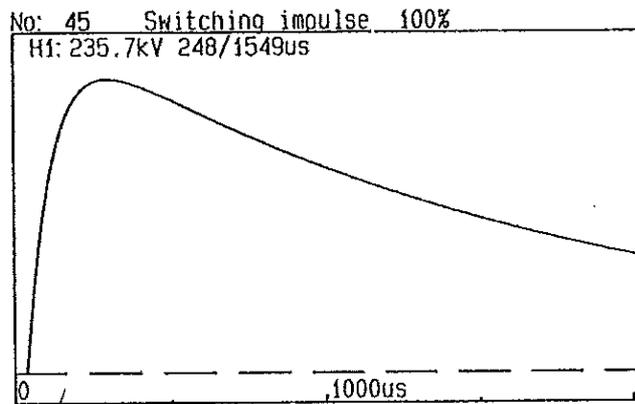
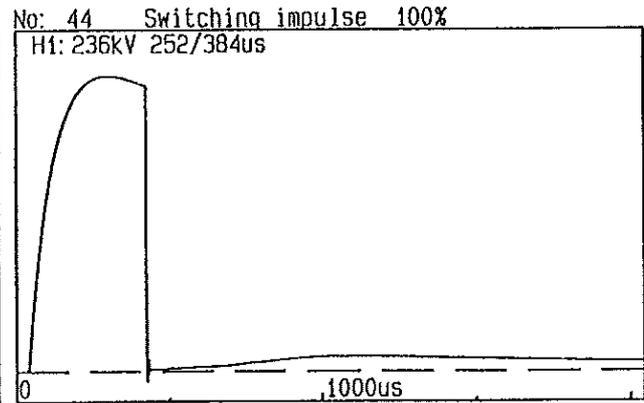
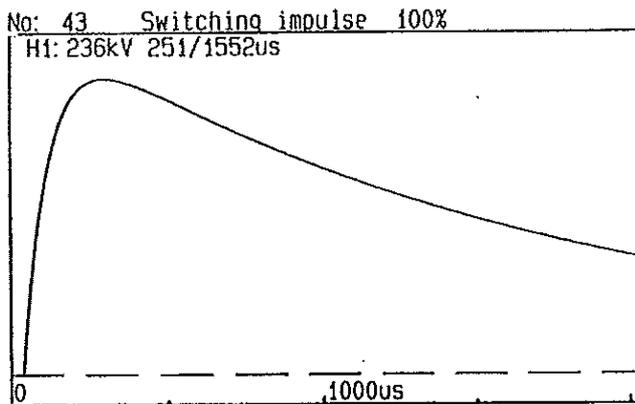
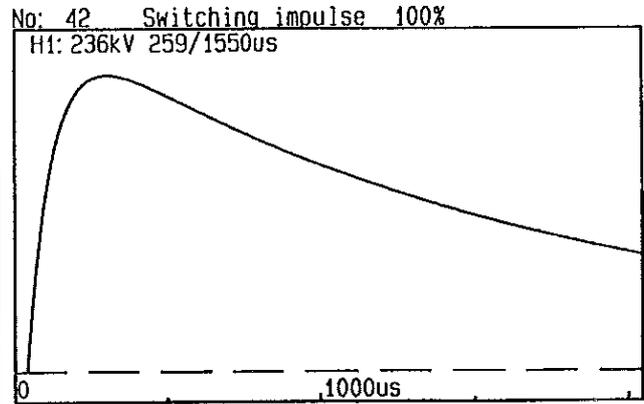
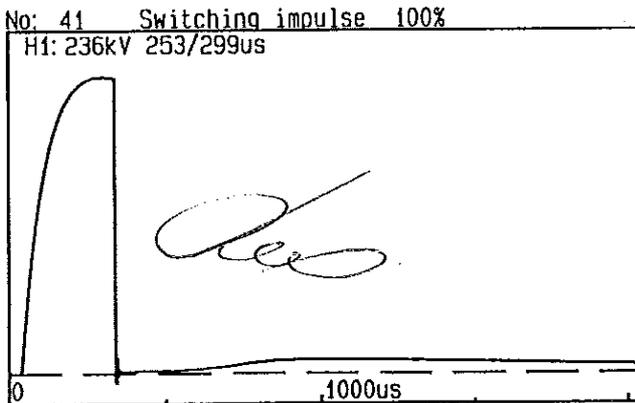
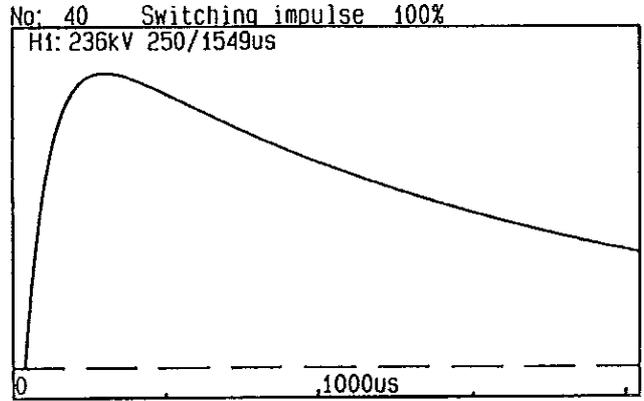
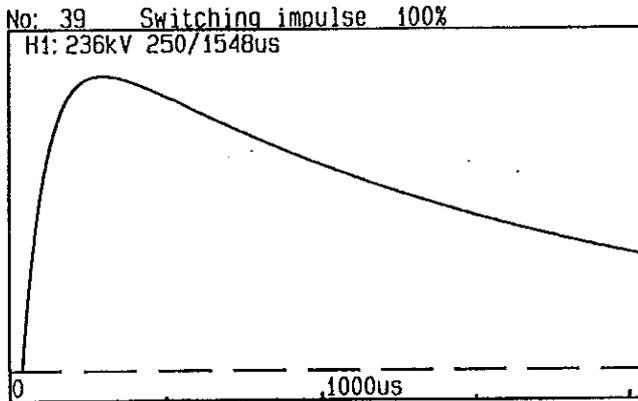


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ОРИГИНАЛ



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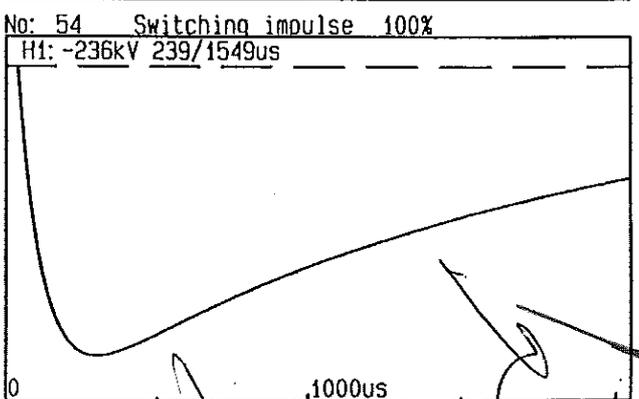
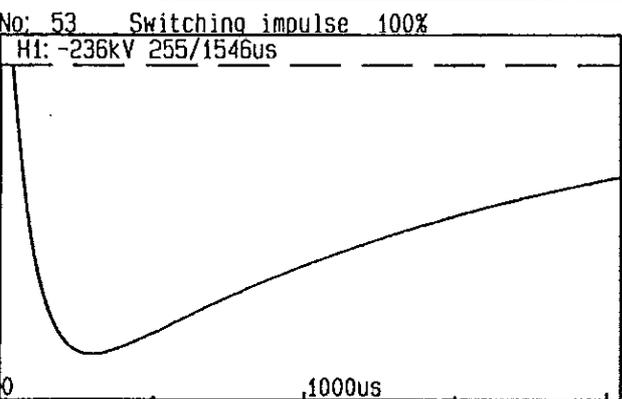
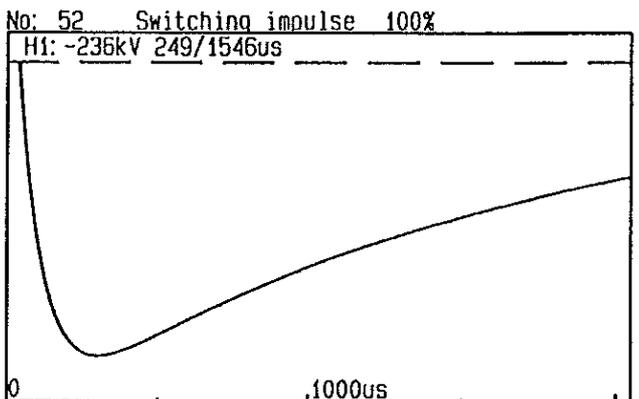
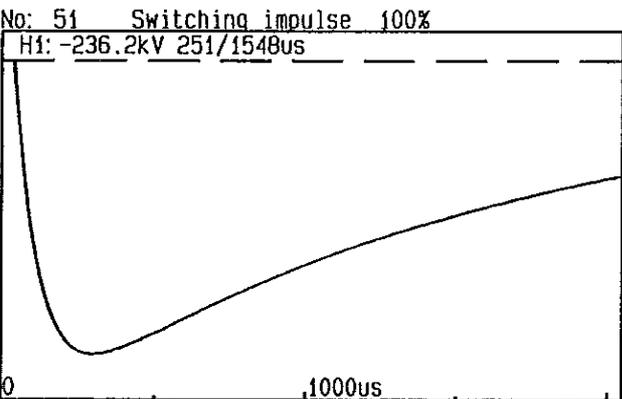
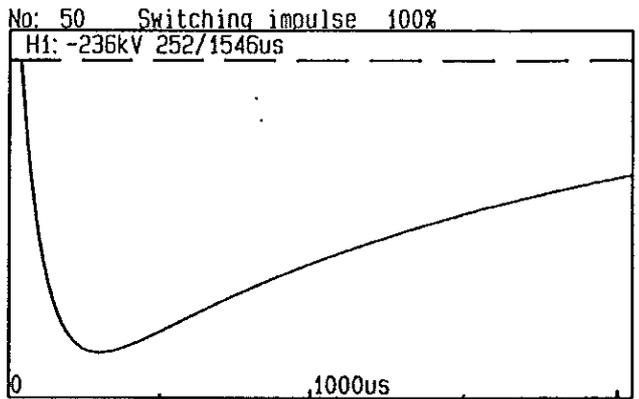
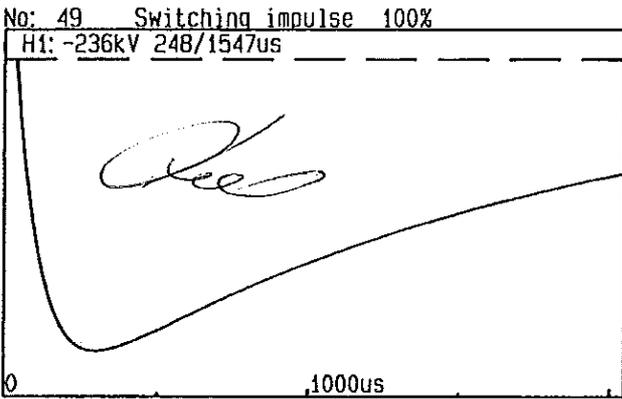
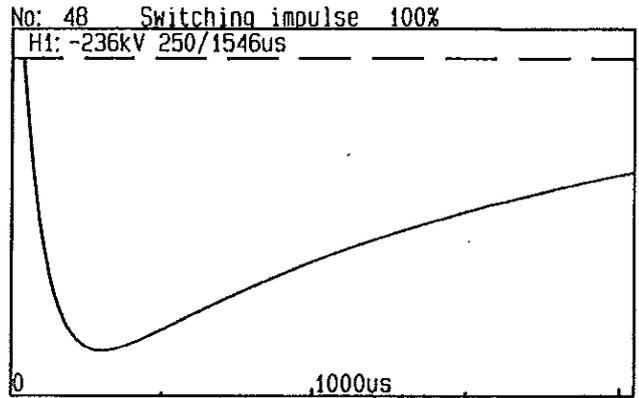
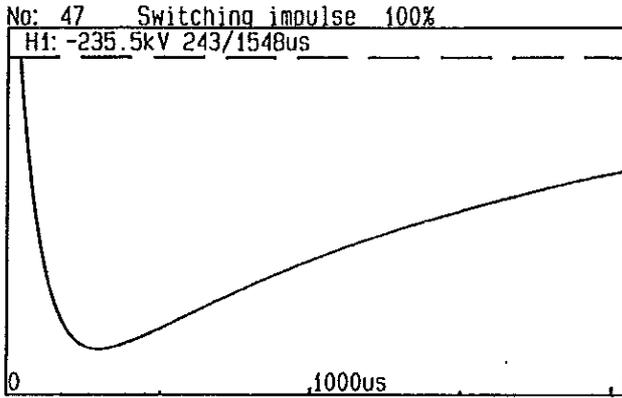


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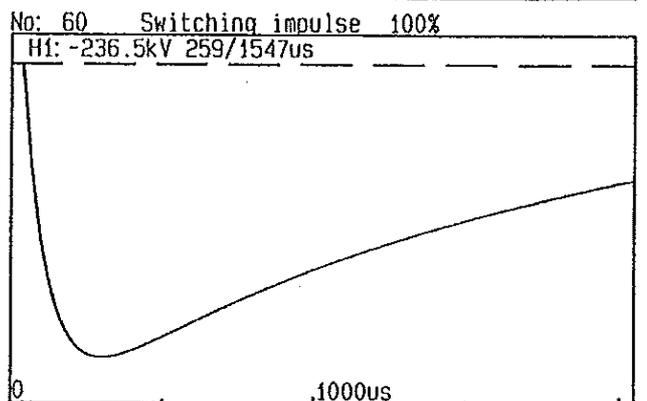
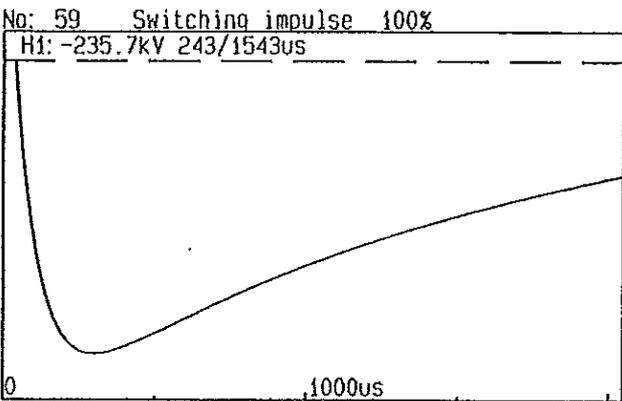
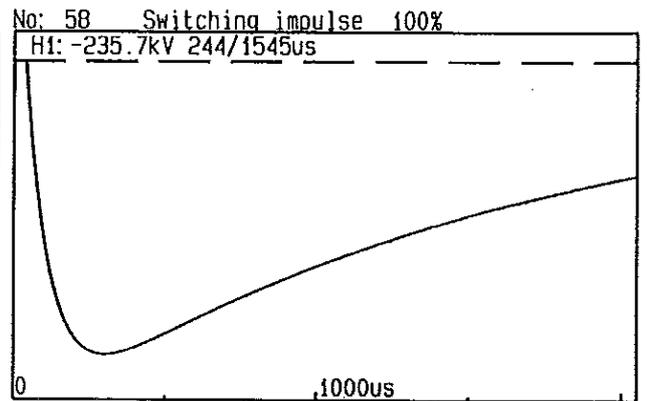
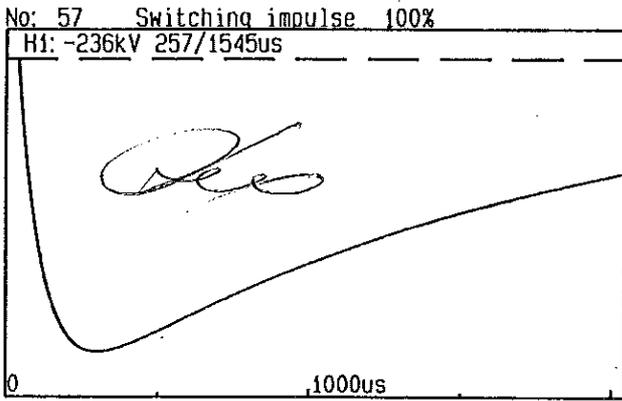
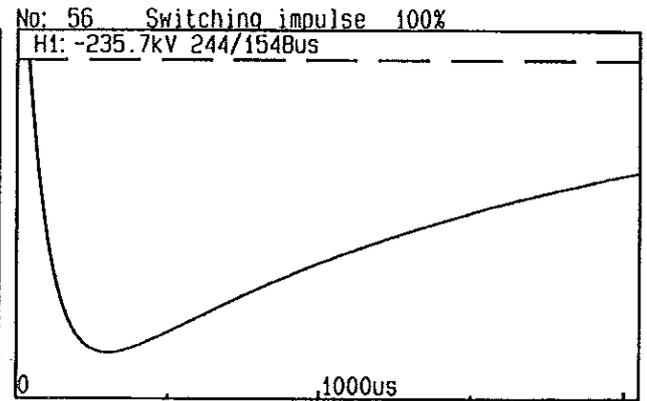
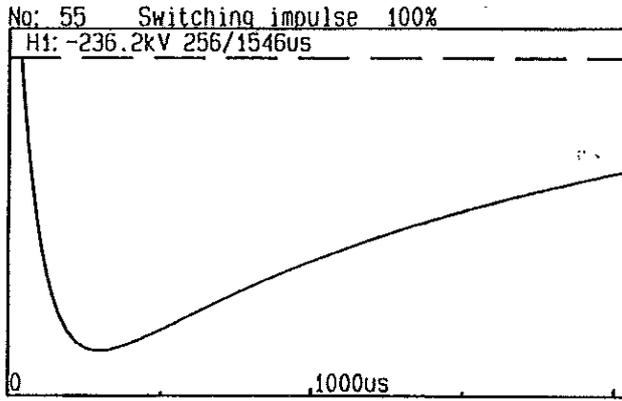


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Test Record

Test date : 29 Sep 1999

Serial nbr. : Q72

IMPULSE VOLTAGE TEST

MEASUREMENTS

LIGHTNING IMPULSE VOLTAGE TEST on terminal H1.  
Nominal test voltage 376kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	375	1.30/53	1
100	375	1.30/53	2
100	375	1.31/54	3
100	376	1.30/54	4
100	376	1.31/53	5
100	376	1.31/53	6
100	376	1.31/53	7
100	376	1.31/53	8
100	376	1.31/53	9
100	375	1.30/54	10
100	375	1.30/54	11
100	376	1.31/54	12
100	375	1.30/53	13
100	375	1.31/54	14
100	375	1.30/54	15

*Free*

LIGHTNING IMPULSE VOLTAGE TEST on terminal H1.  
Nominal test voltage -376kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	-375	1.30/53	16
100	-375	1.29/53	17
100	-376	1.30/53	18
100	-376	1.29/53	19
100	-376	1.29/53	20
100	-376	1.29/53	21
100	-375	1.29/53	22
100	-375	1.29/53	23
100	-376	1.30/53	24
100	-375	1.29/53	25
100	-375	1.29/53	26
100	-375	1.29/53	27
100	-375	1.29/53	28
100	-375	1.29/53	29
100	-375	1.30/53	30

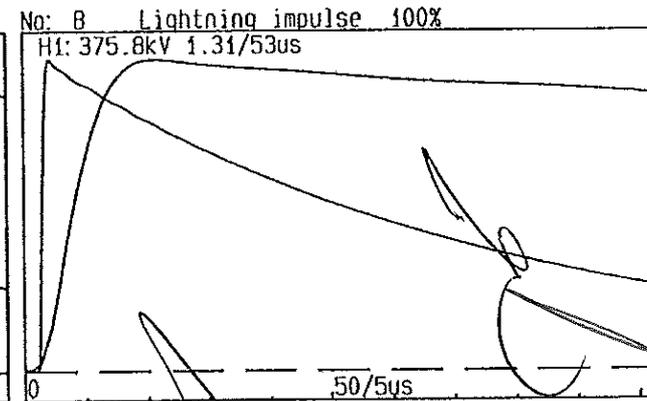
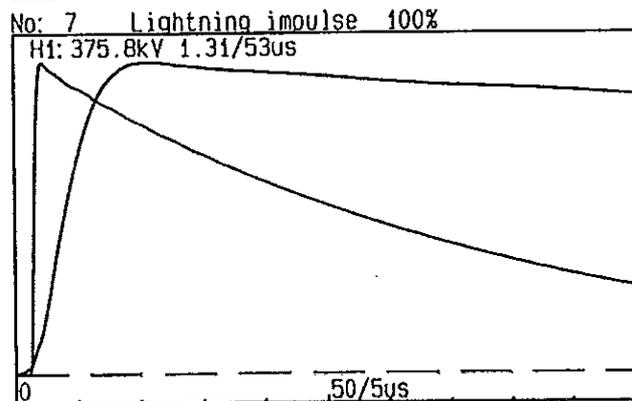
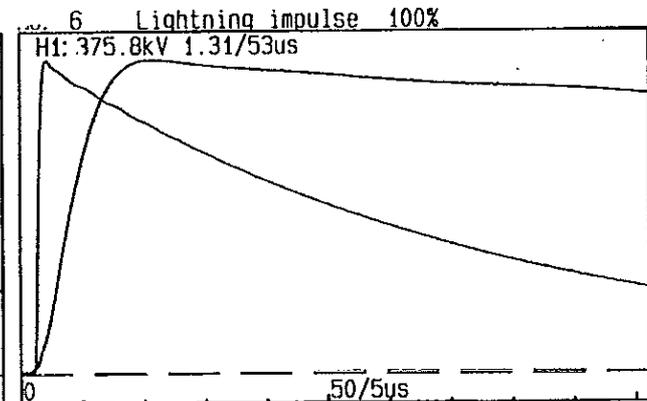
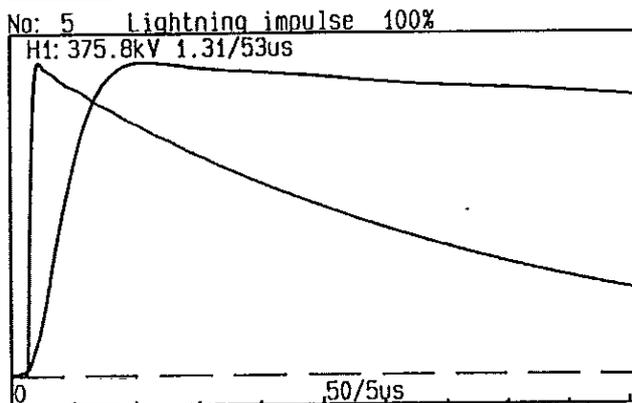
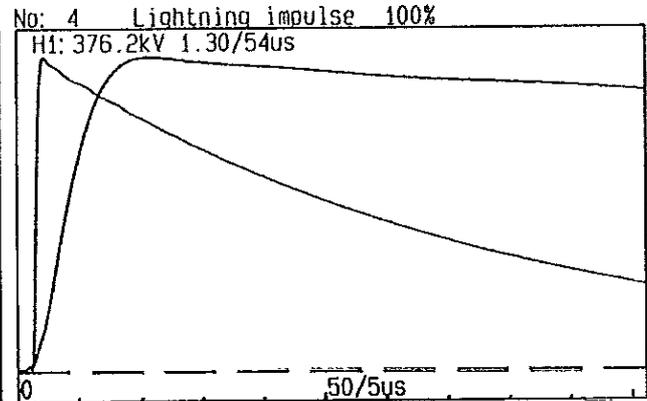
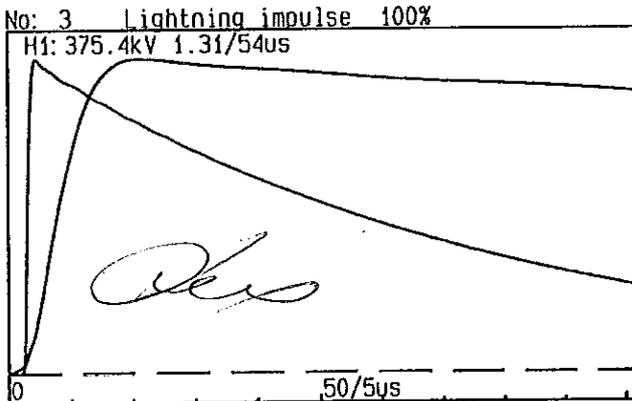
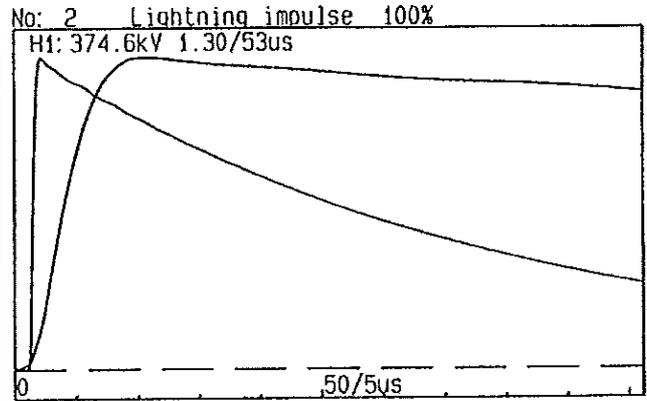
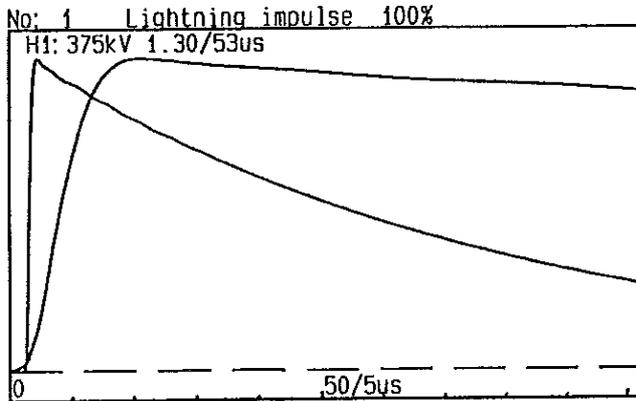
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ВАРНІС  
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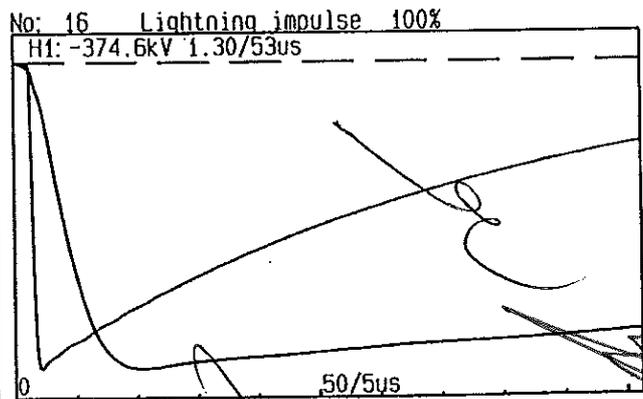
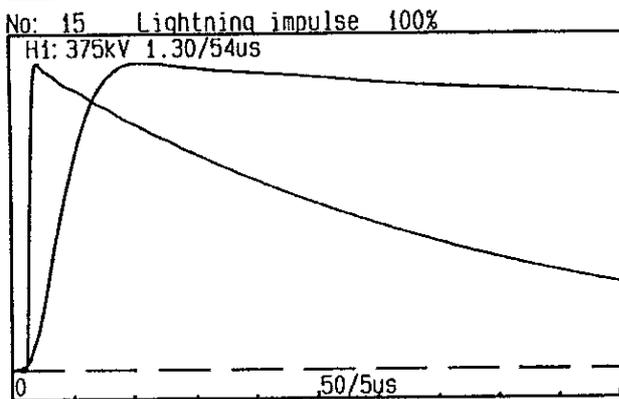
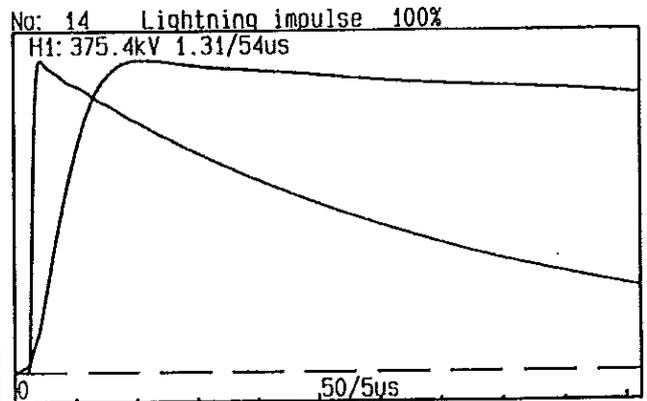
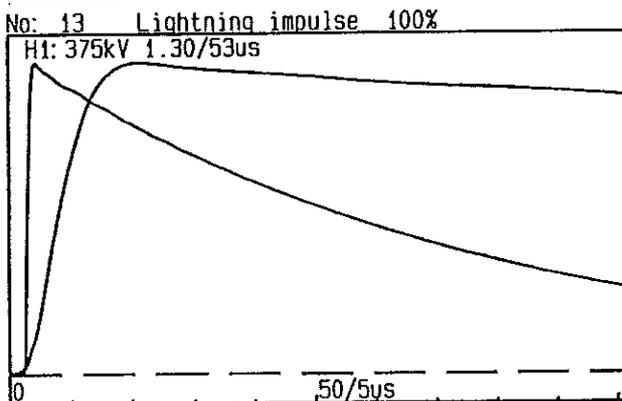
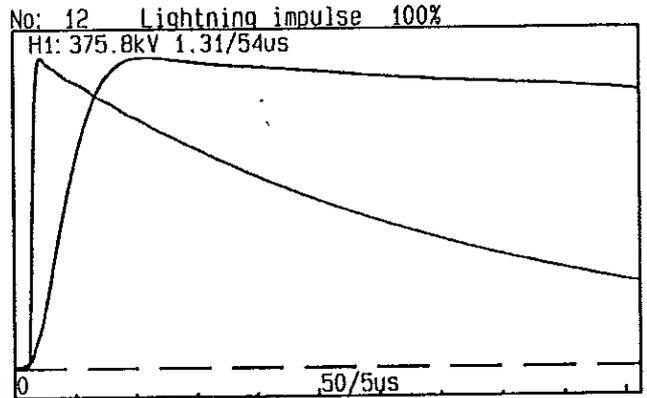
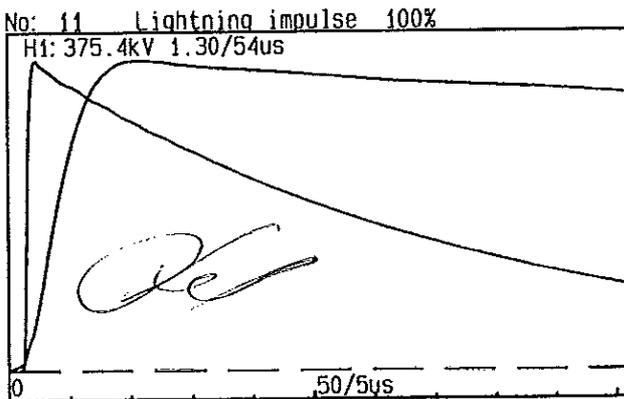
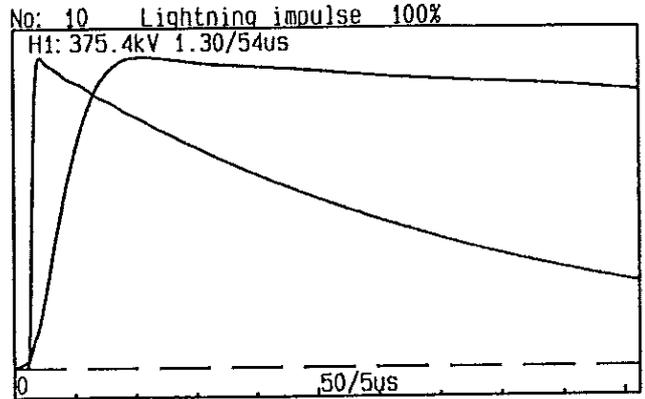
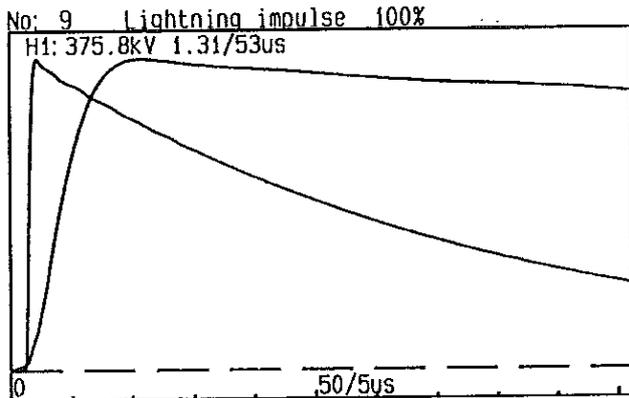




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ВЯРНО С  
ОРИГИНАЛА



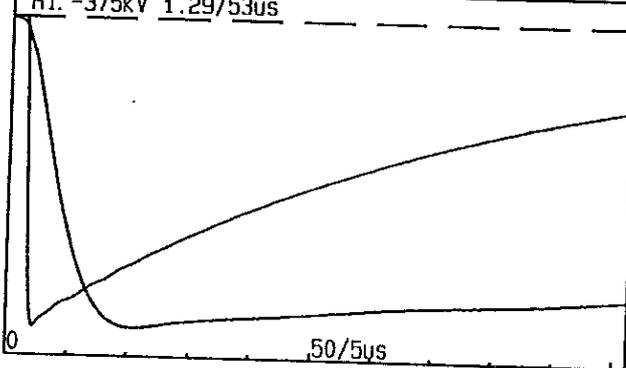


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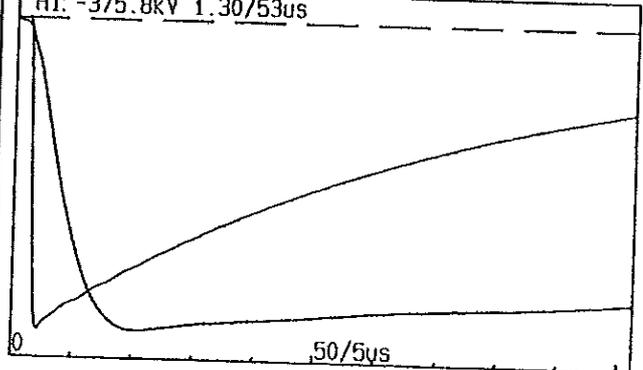
ВЕРНА С  
ОРИГИНАЛА



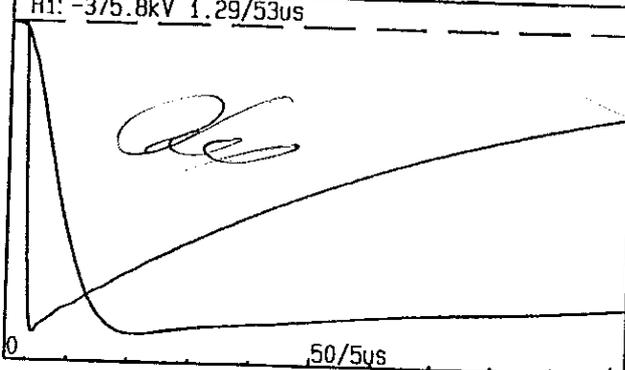
No: 17 Lightning impulse 100%  
H1: -375kV 1.29/53us



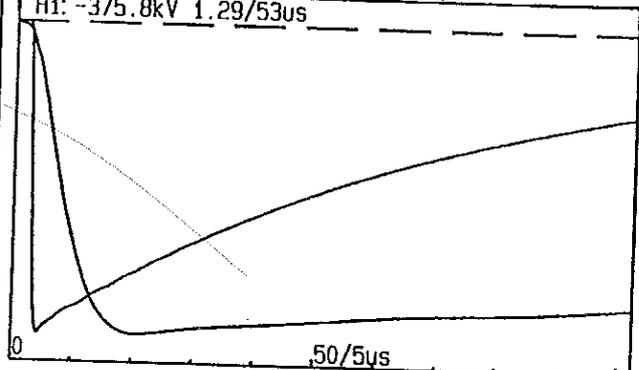
No: 18 Lightning impulse 100%  
H1: -375.8kV 1.30/53us



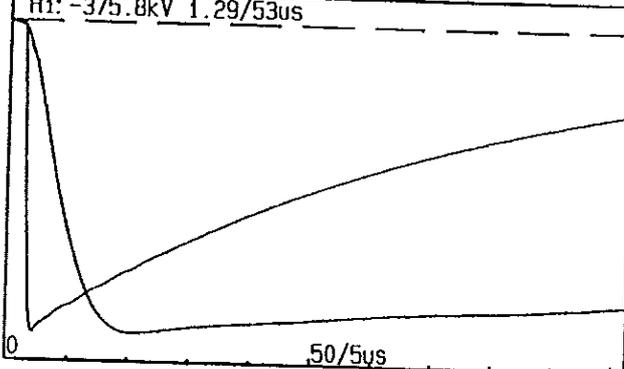
No: 19 Lightning impulse 100%  
H1: -375.8kV 1.29/53us



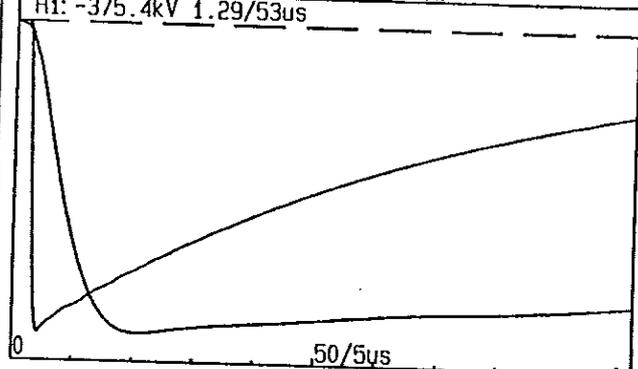
No: 20 Lightning impulse 100%  
H1: -375.8kV 1.29/53us



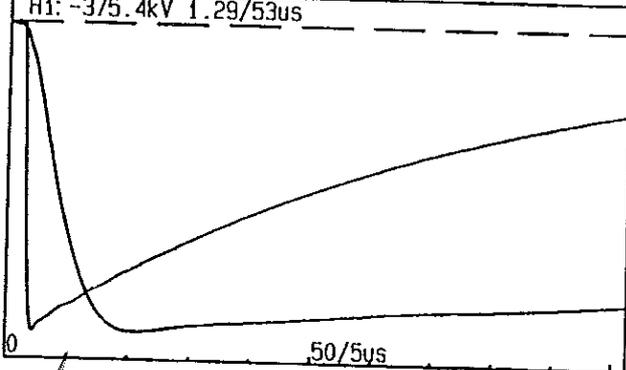
No: 21 Lightning impulse 100%  
H1: -375.8kV 1.29/53us



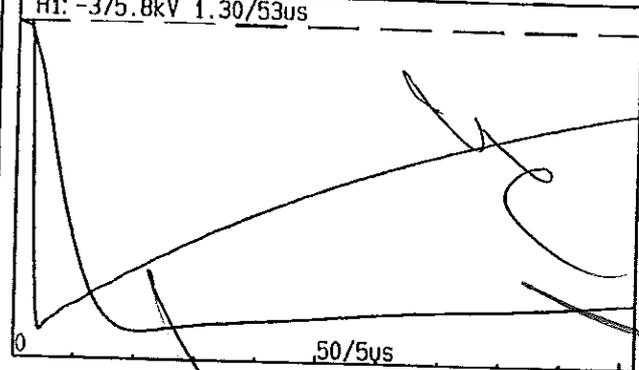
No: 22 Lightning impulse 100%  
H1: -375.4kV 1.29/53us



No: 23 Lightning impulse 100%  
H1: -375.4kV 1.29/53us



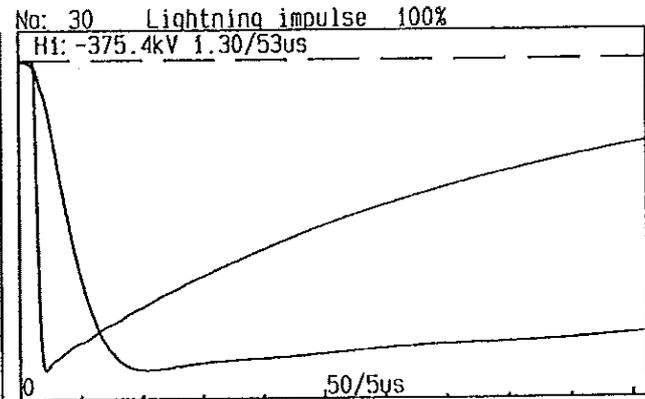
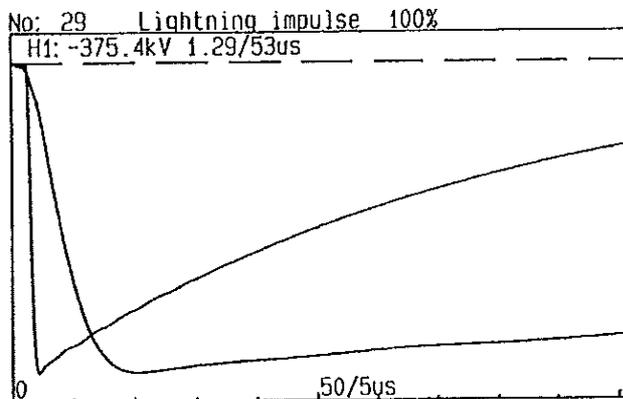
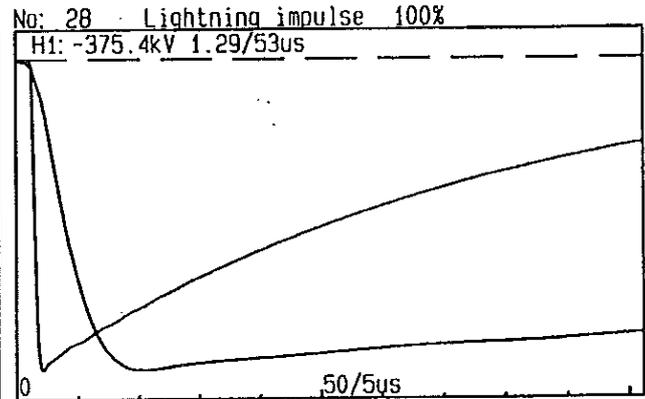
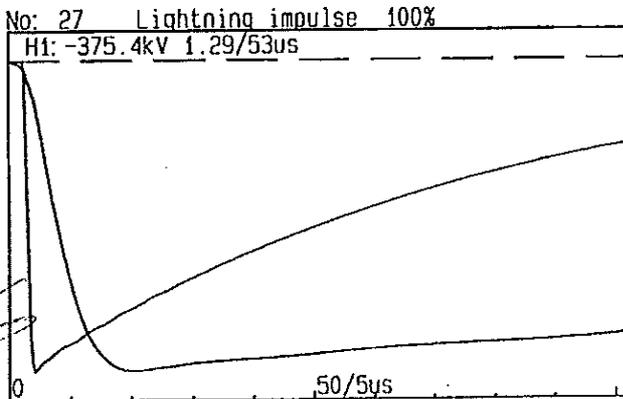
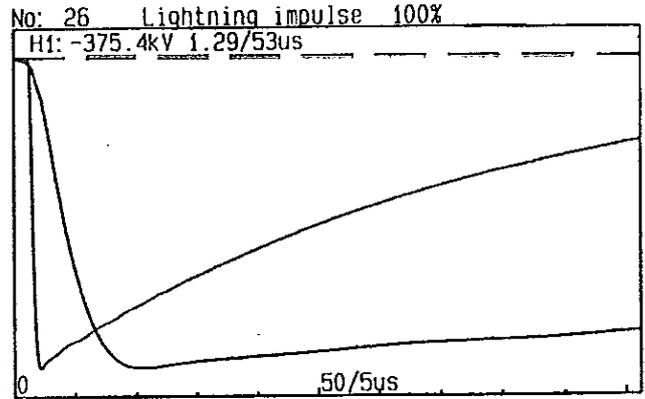
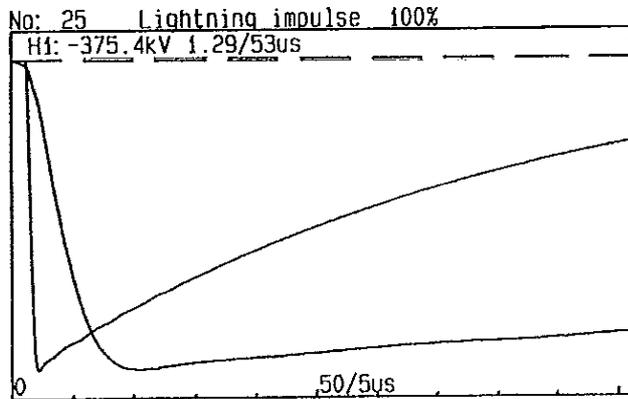
No: 24 Lightning impulse 100%  
H1: -375.8kV 1.30/53us



000200

ВАЖНО С  
ОРИГИНАЛА





000201

ВЕРНО С  
ОРИГИНАЛА



Test Record

Test date 20 Oct 1999

Serial nbr. Q72

IMPULSE VOLTAGE TEST

MEASUREMENTS

SWITCHING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage 328kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	328	272/2920	31
100	327	280/2930	32
100	327	274/2921	33
100	326	260/2925	34
100	327	264/2924	35
100	328	268/2924	36
100	327	265/2912	37
100	327	281/2927	38
100	327	263/2920	39
100	328	265/2919	40
100	327	269/789	41
100	327	259/585	42
100	327	265/2928	43
100	327	261/2930	44
100	327	266/2918	45

*Dep*

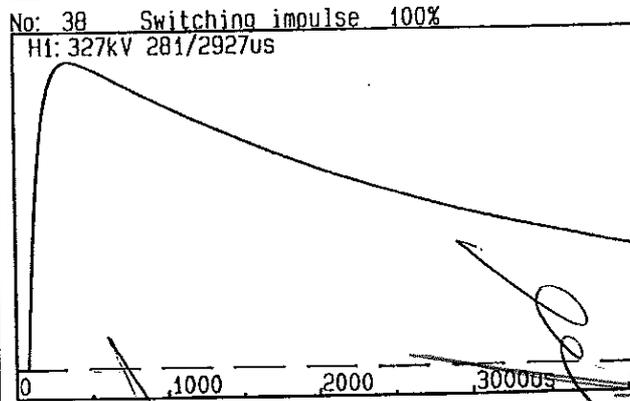
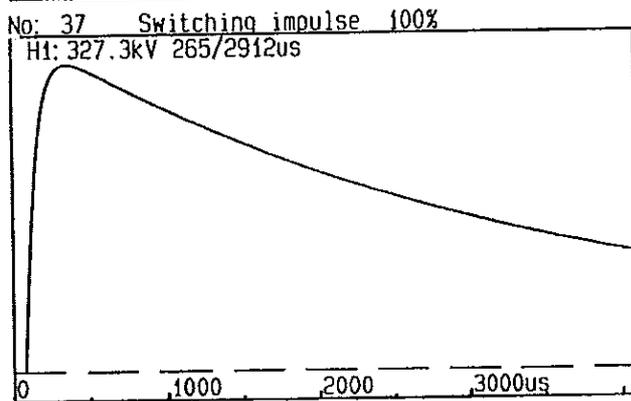
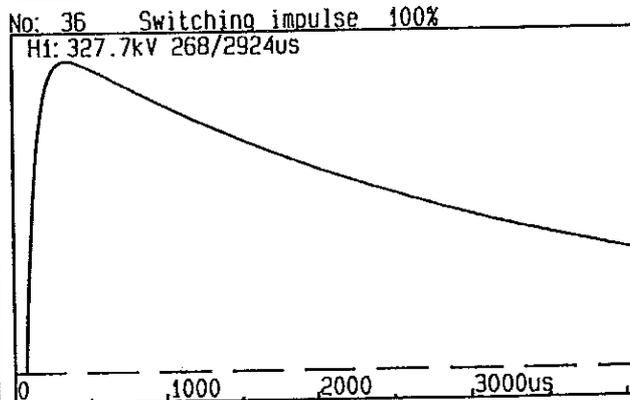
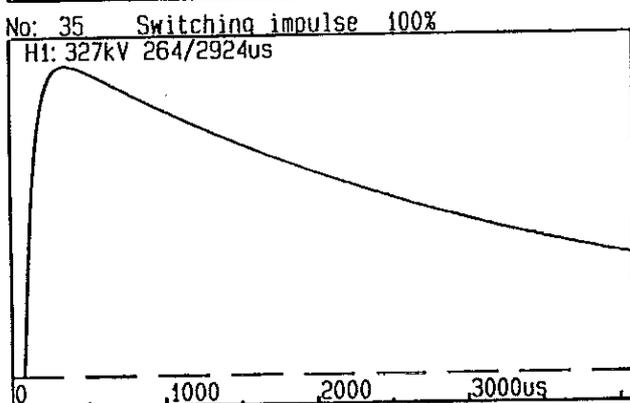
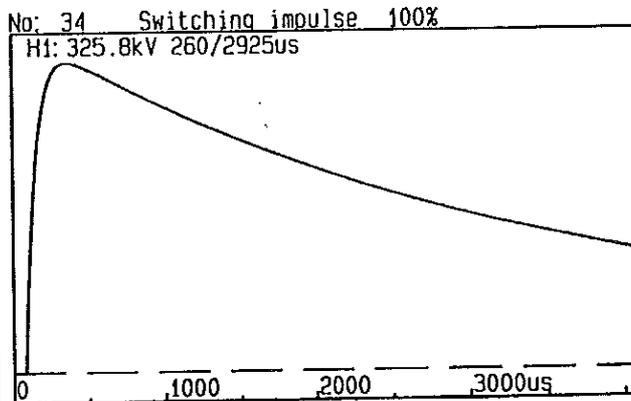
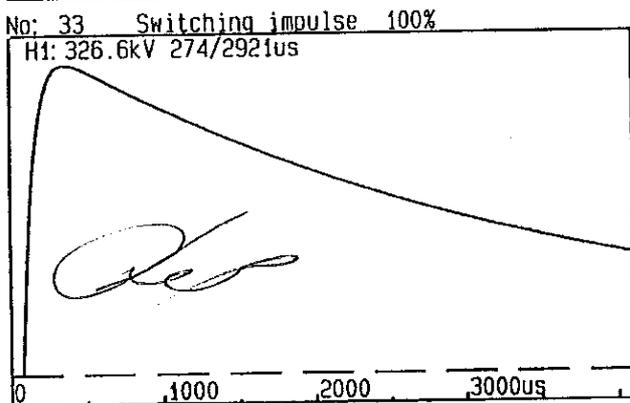
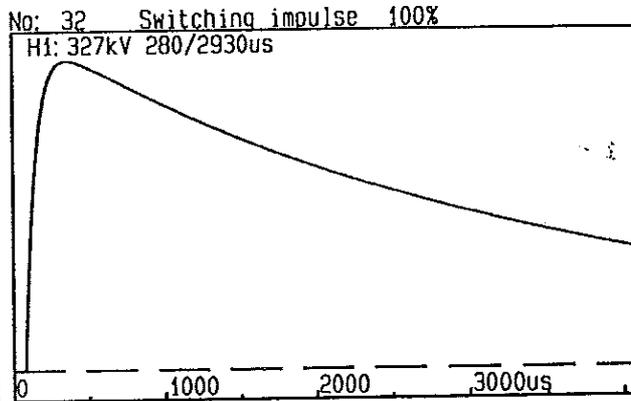
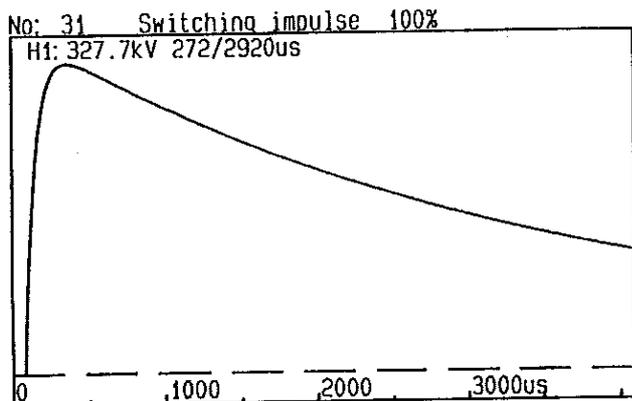
SWITCHING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage: -328kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	-325	277/2914	46
100	-328	260/2915	47
100	-327	274/2918	48
100	-328	258/2935	49
100	-325	260/2918	50
100	-329	268/2919	51
100	-329	272/2918	52
100	-328	261/2932	53
100	-329	267/2905	54
100	-329	270/2922	55
100	-328	260/2914	56
100	-328	261/2916	57
100	-329	262/2904	58
100	-328	263/2908	59
100	-329	264/2920	60

000202

ВЯНО С  
ОРИГИНАЛА

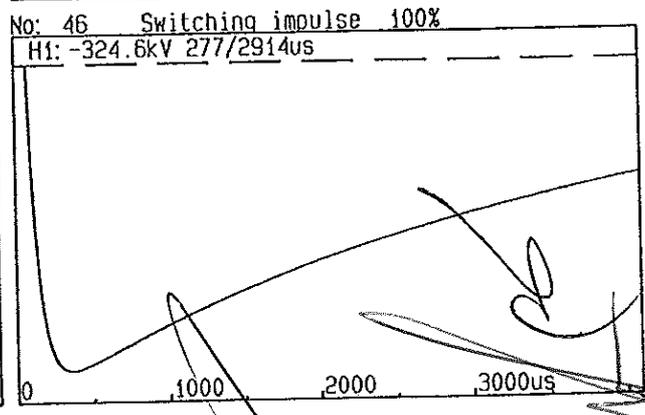
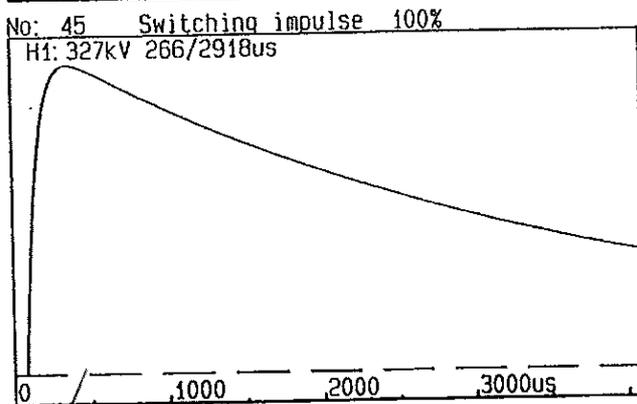
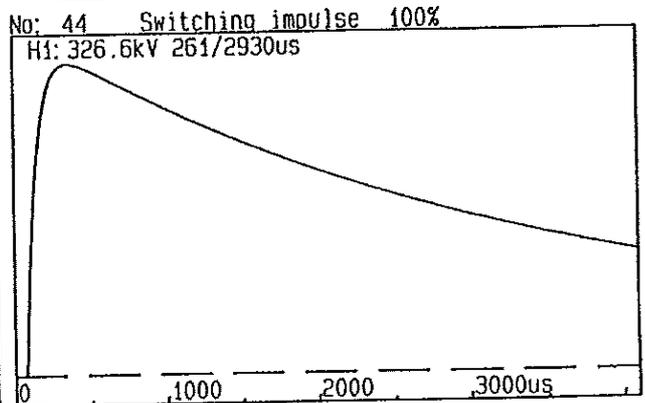
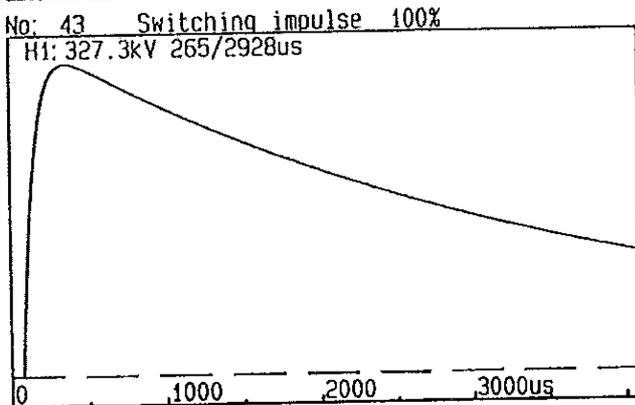
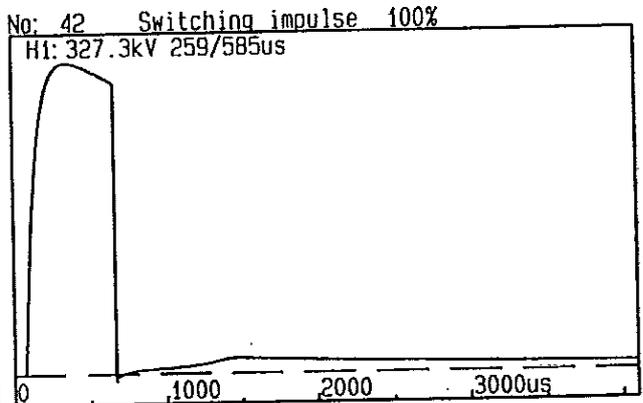
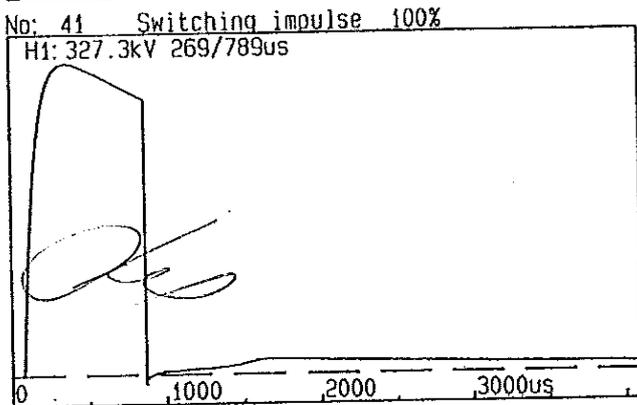
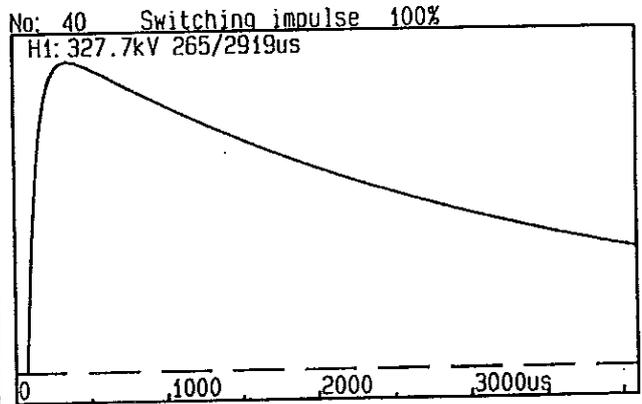
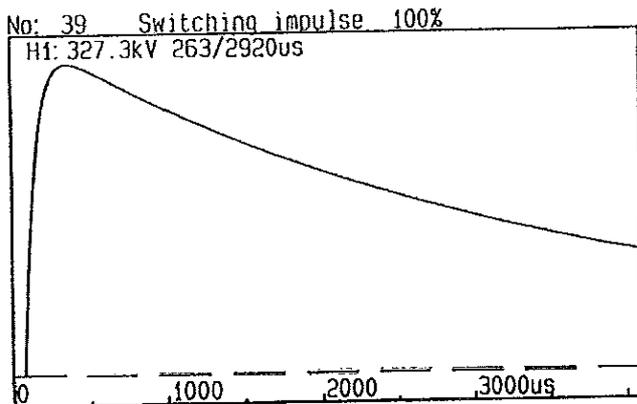




000203

ВЯЖО С  
ОРИГИНАЛА

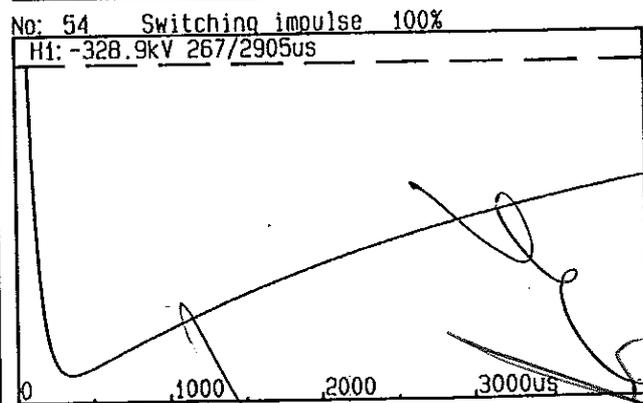
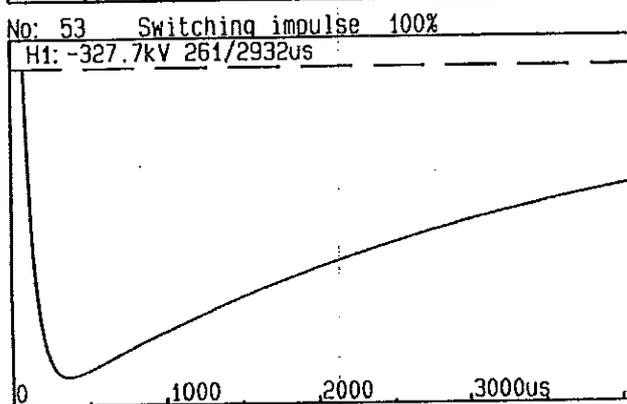
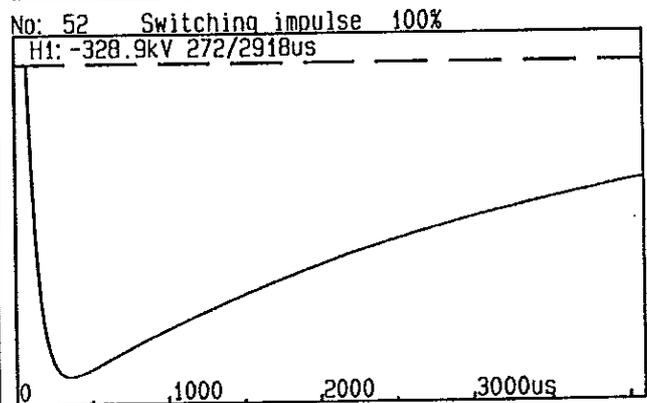
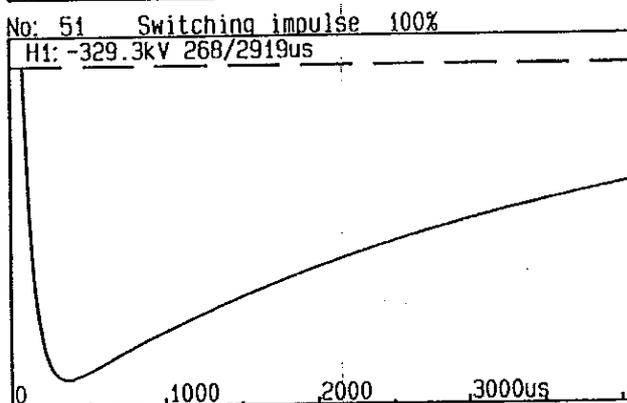
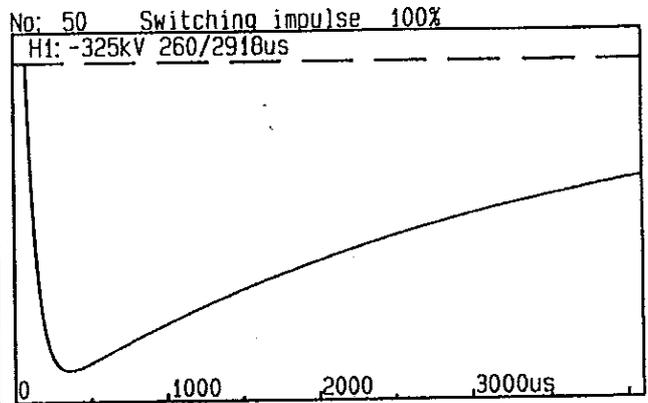
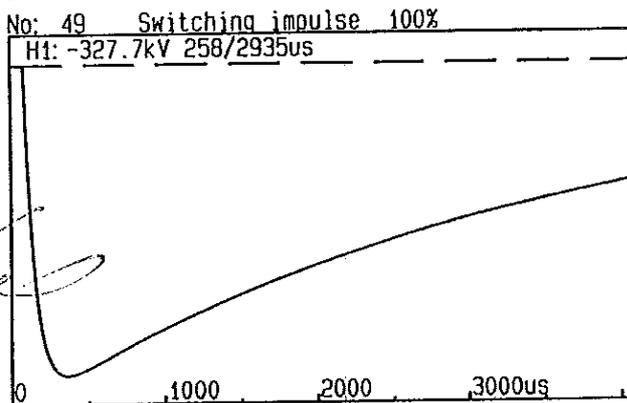
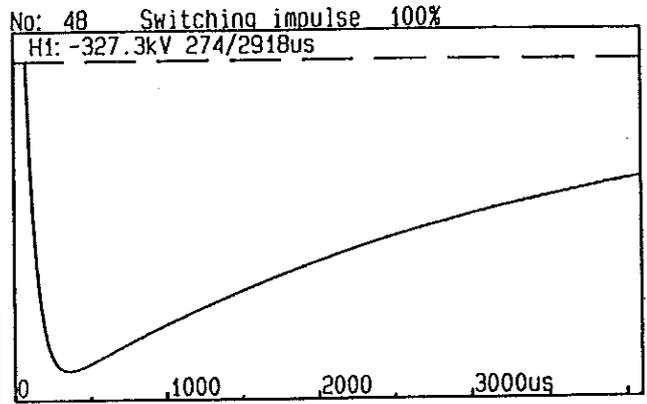
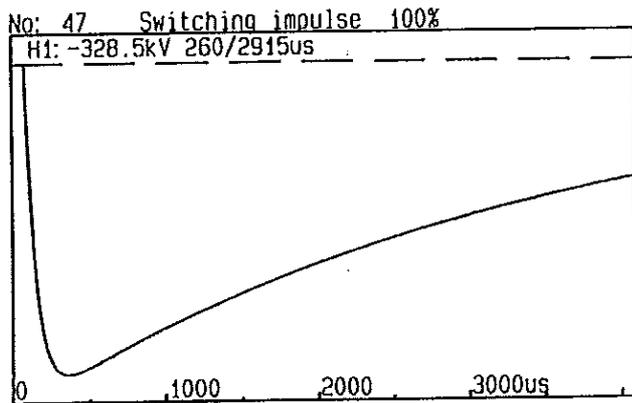




000204

БЯРНОС  
ОРИГІНАЛ

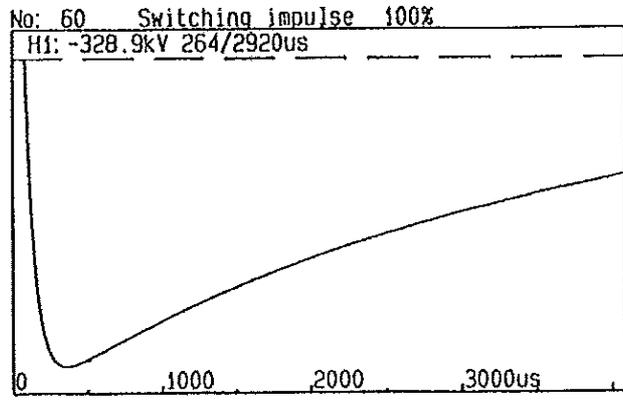
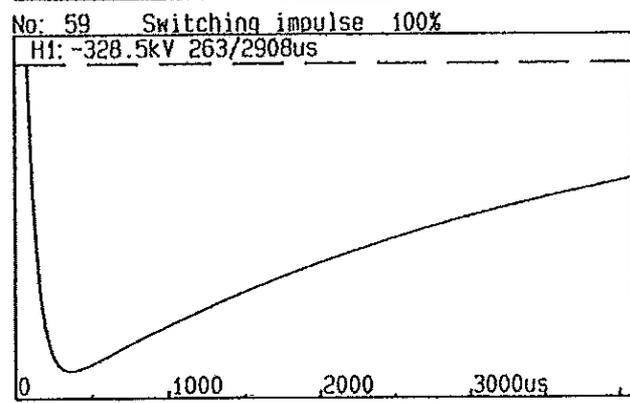
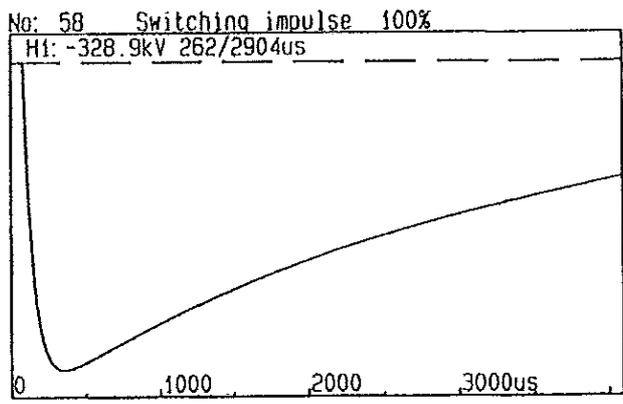
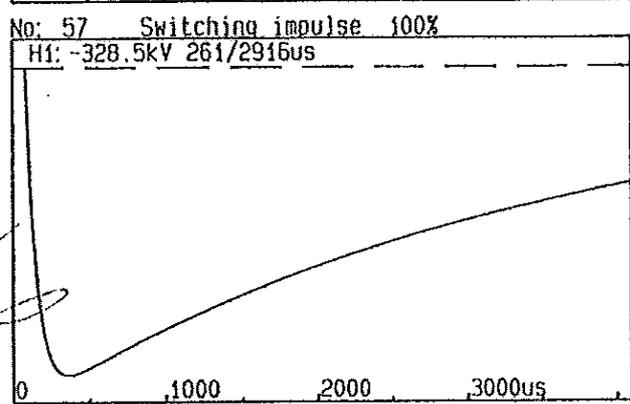
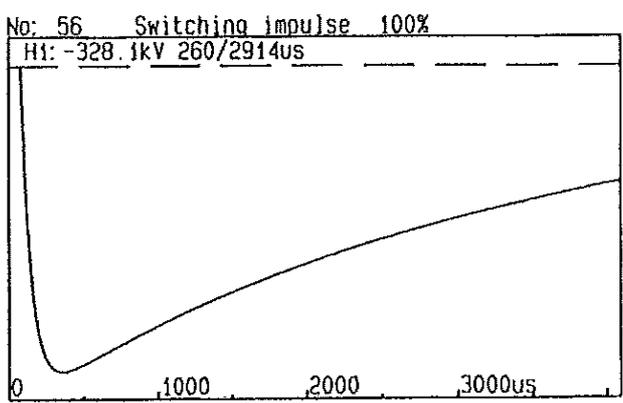
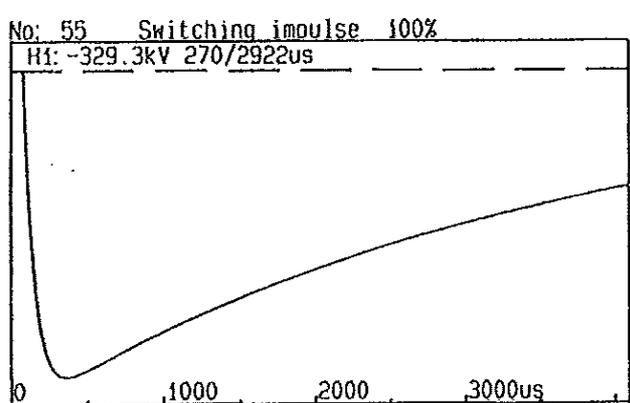




000205

ВЕРНО С  
ОРИГИНАЛА





000206

~~ВЯРНО С  
ОРИГИНАЛА~~



Test Record

Test date 26 Aug 1999

Serial nbr. : Q143

IMPULSE VOLTAGE TEST

MEASUREMENTS

LIGHTNING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage 600kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	557	1.33/54	1
100	542	1.34/54	2
100	542	1.33/54	3
100	543	1.34/54	4
100	542	1.33/54	5
100	543	1.34/54	6
100	542	1.33/54	7
100	544	1.34/54	8
100	544	1.33/54	9
100	544	1.33/54	10
100	544	1.34/54	11
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100	544	1.34/54	13
100	544	1.34/54	14
100	544	1.33/54	15

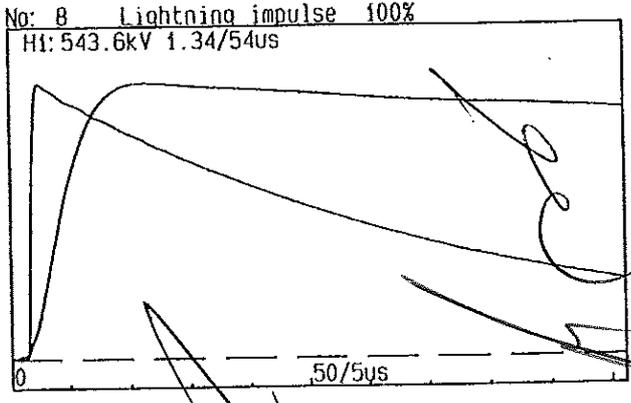
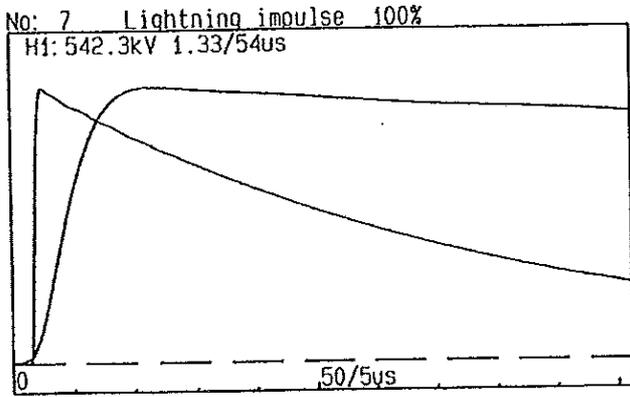
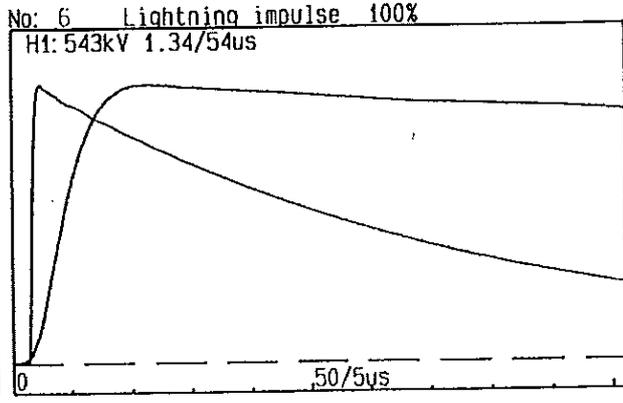
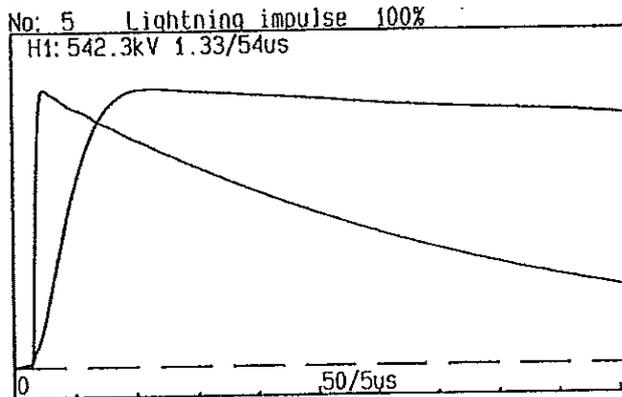
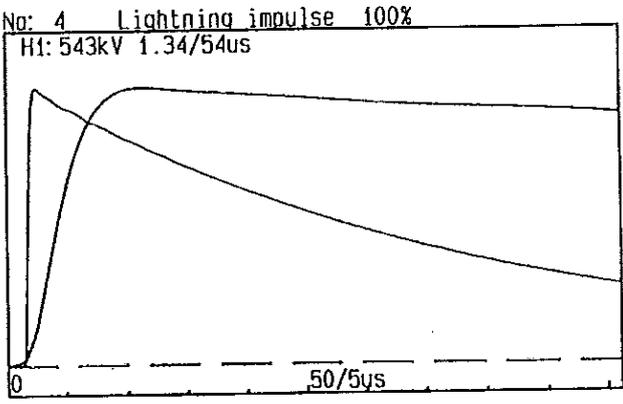
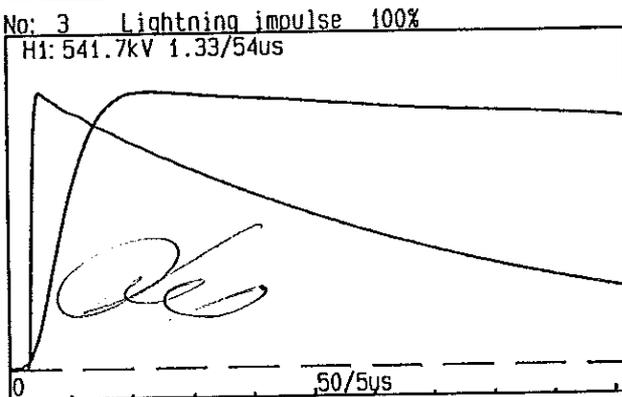
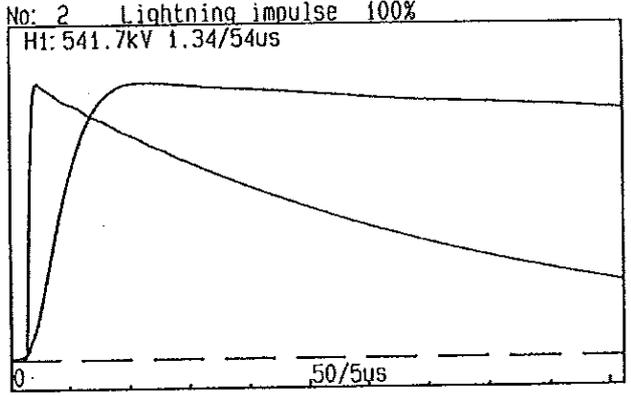
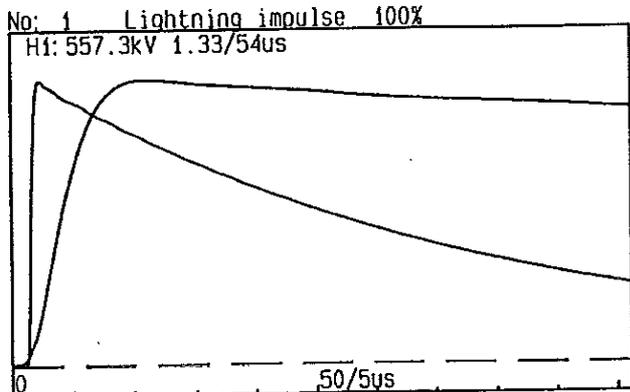
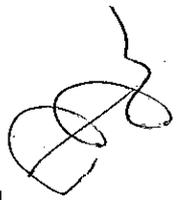
LIGHTNING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage -600kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	-542	1.33/54	16
100	-544	1.33/54	17
100	-544	1.33/54	18
100	-544	1.33/54	19
100	-544	1.32/54	20
100	-544	1.32/54	21
100	-544	1.32/54	22
100	-544	1.32/54	23
100	-544	1.33/54	24
100	-544	1.32/54	25
100	-544	1.32/54	26
100	-544	1.32/54	27
100	-544	1.33/54	28
100	-544	1.32/54	29
100	-543	1.32/54	30

000207

ЗЯРНС  
ОРИГОНАЛ

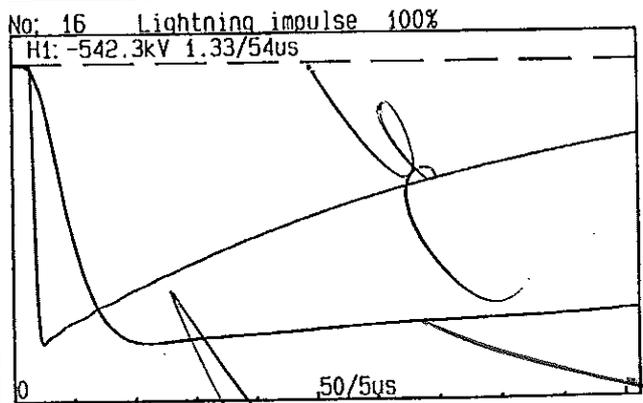
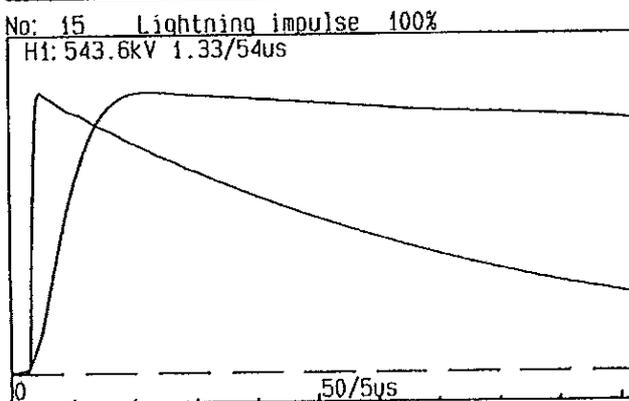
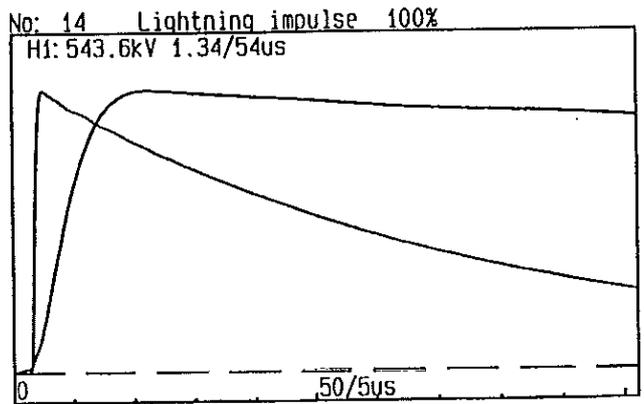
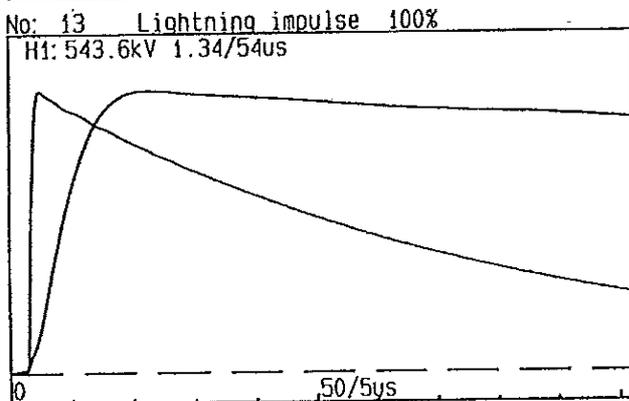
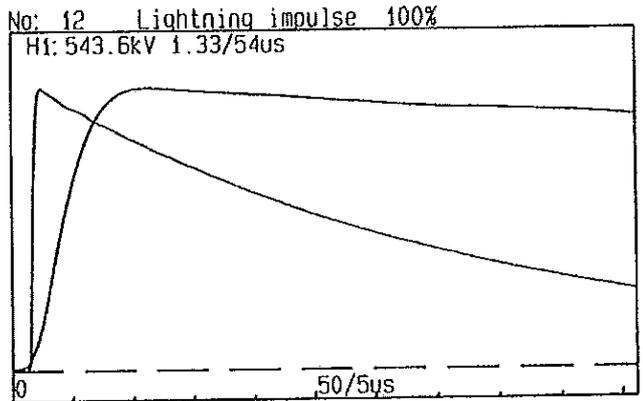
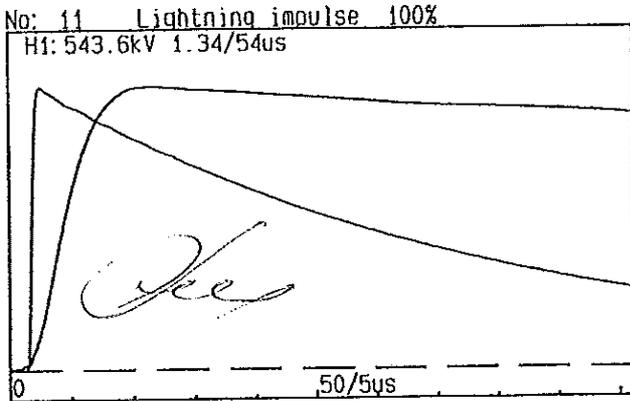
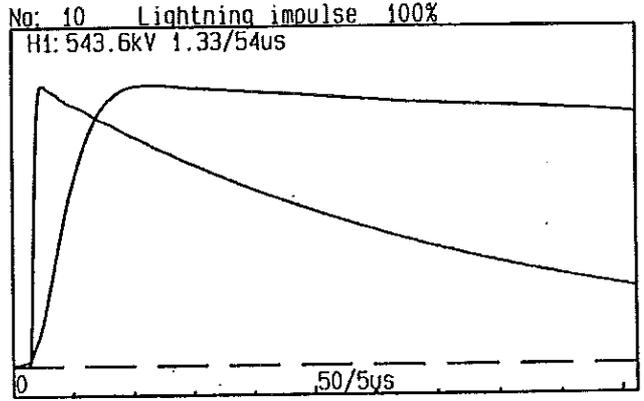
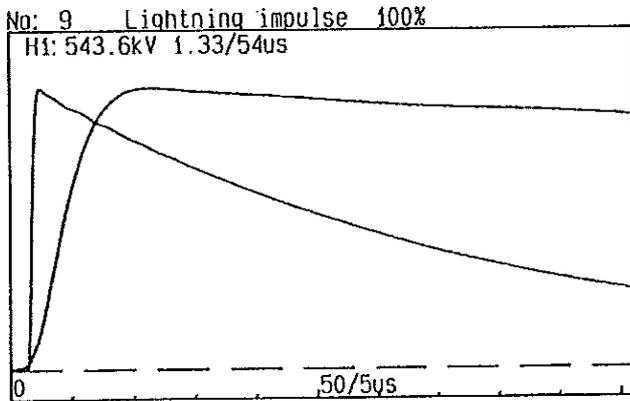




000208

ВЯНО С  
ОРИГИНАЛА

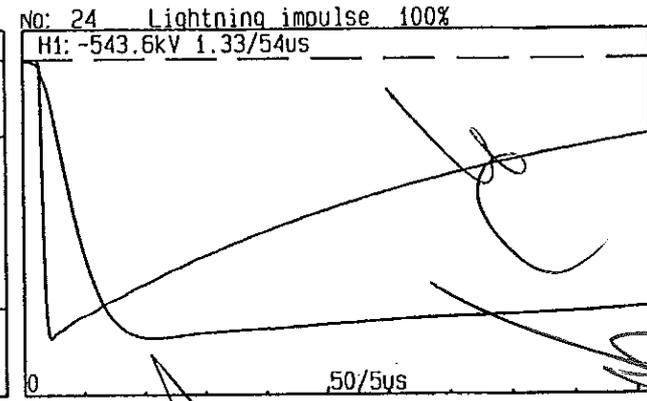
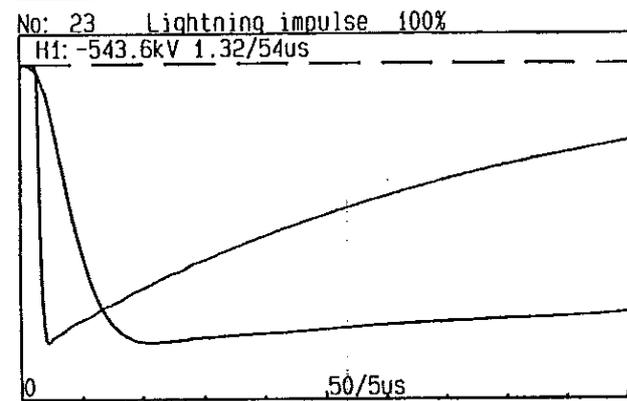
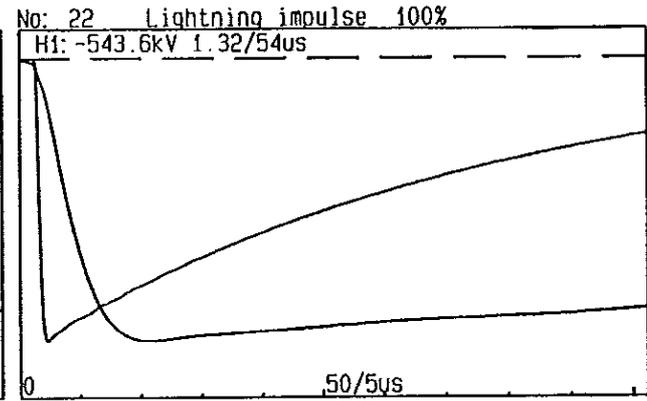
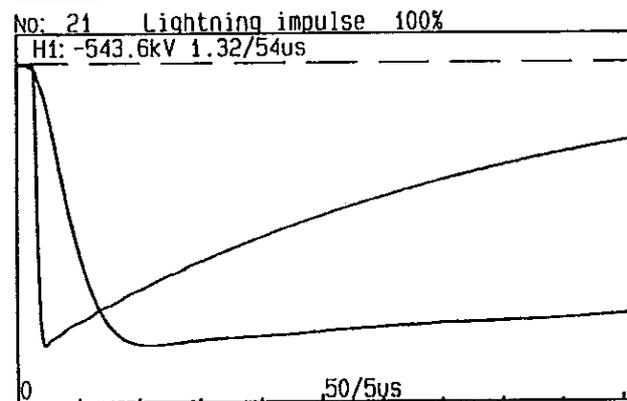
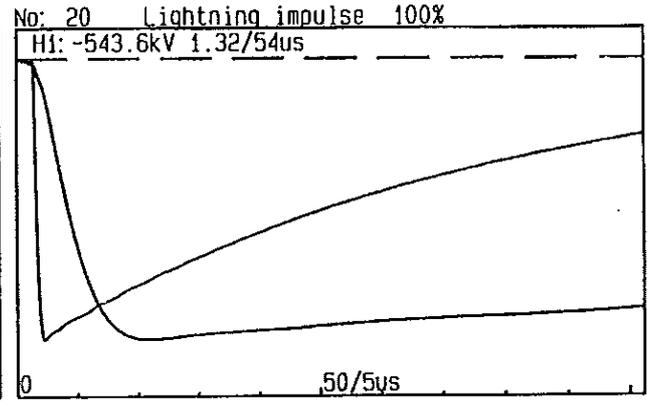
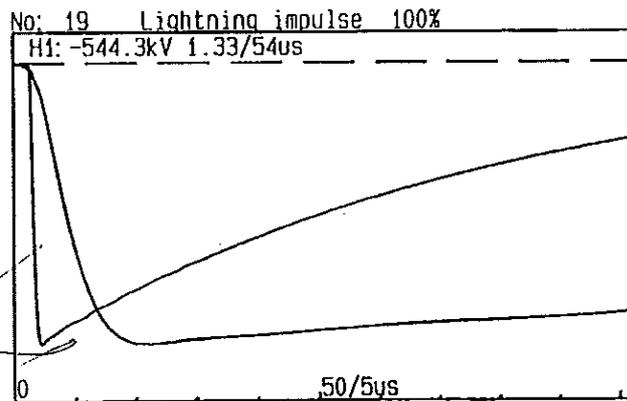
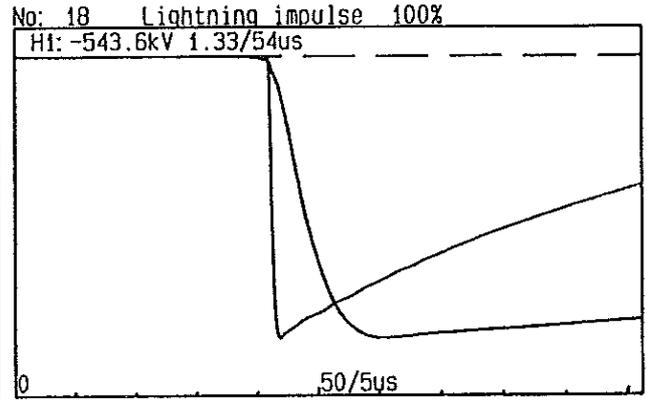
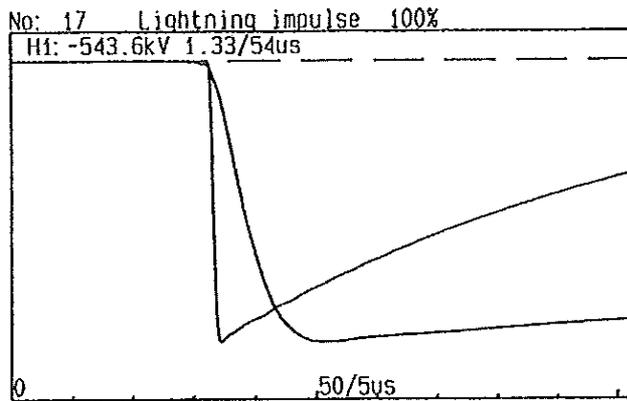




000209

ВЯРНО С  
ОРИГИНАЛА

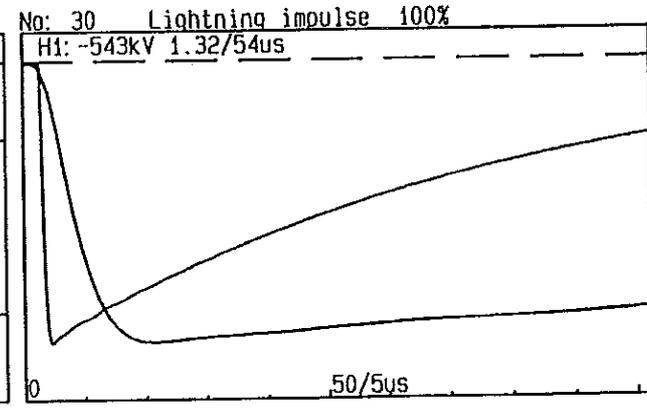
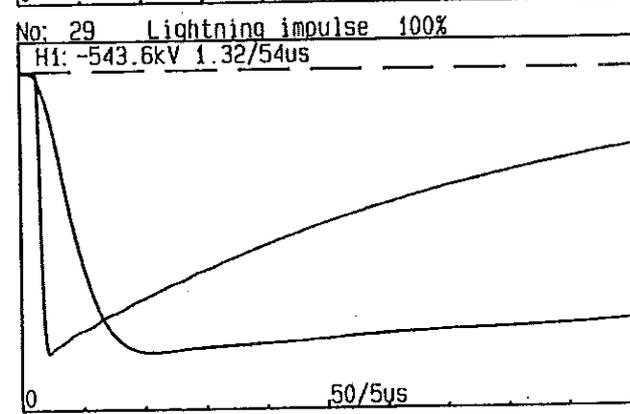
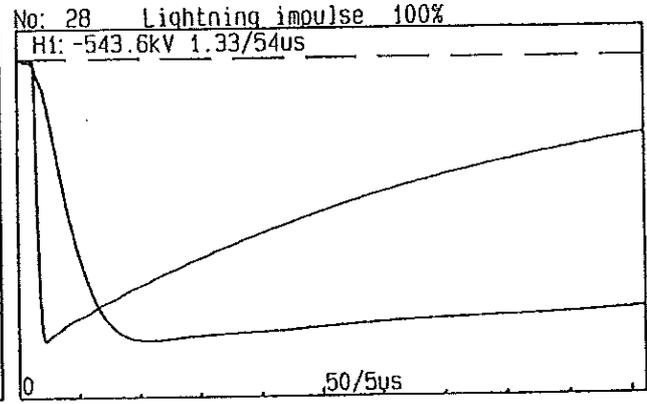
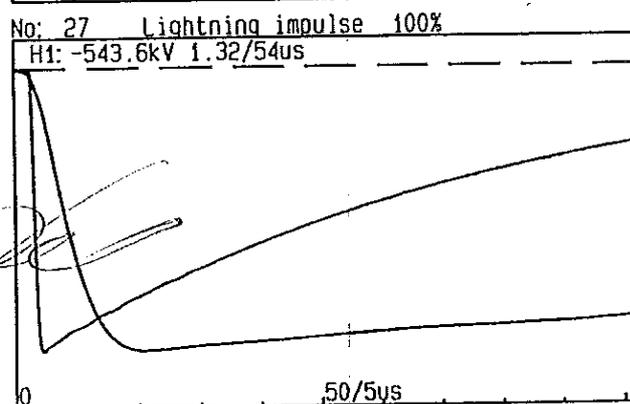
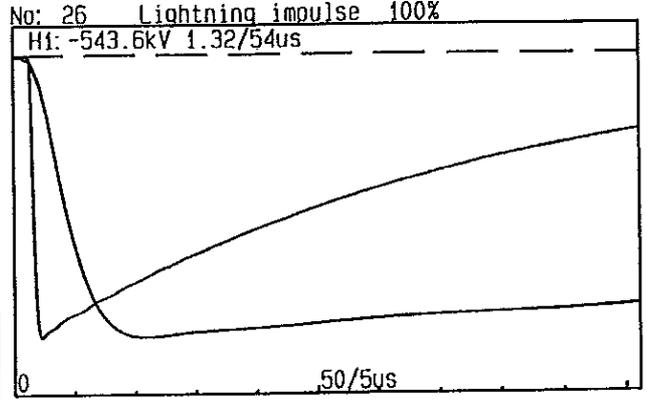
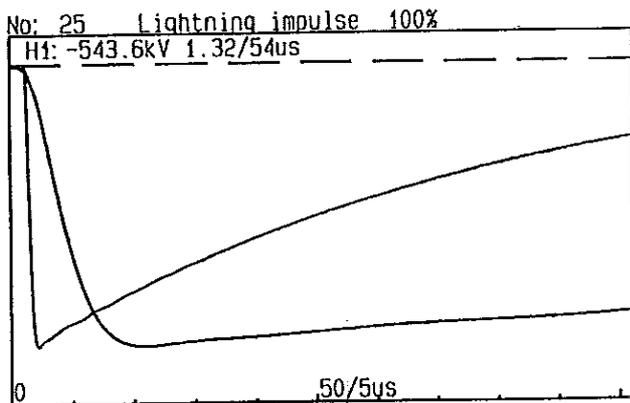




000210

ВЯНО С  
ОРИГИНАЛА

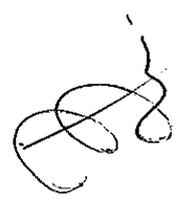




000211

ВЯРНО С  
ОРИГИНАЛА





Test Record

Test date 20 Oct 1999

Serial nbr. : Q143

IMPULSE VOLTAGE TEST

MEASUREMENTS

SWITCHING IMPULSE VOLTAGE TEST on terminal H1  
Nominal test voltage 458kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	460	267/2923	42
100	457	267/2918	43
100	451	200/204	44
100	459	263/2926	45
100	459	258/274	46
100	459	268/2929	47
100	459	273/2920	48
100	459	256/2923	49
100	459	270/2921	50
100	459	266/2922	51
100	459	269/2926	52
100	459	271/2923	53
100	459	265/2926	54
100	459	266/2925	55
100	459	258/2925	56

SWITCHING IMPULSE VOLTAGE TEST on terminal H1.  
Nominal test voltage -458kV.

Amplitude %	kV	Impulse shape $\mu$ s	Oscillogram number
100	-458	262/2912	57
100	-458	265/2921	58
100	-458	280/2923	59
100	-458	262/2919	60
100	-458	273/2909	61
100	-458	275/2915	62
100	-459	275/2912	63
100	-458	269/2913	64
100	-459	287/2908	65
100	-459	280/2909	66
100	-458	282/2917	67
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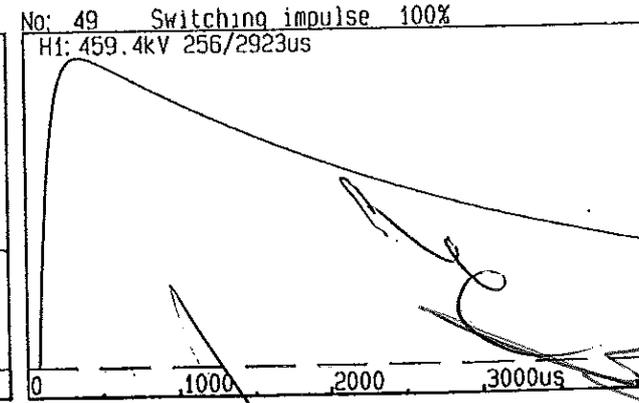
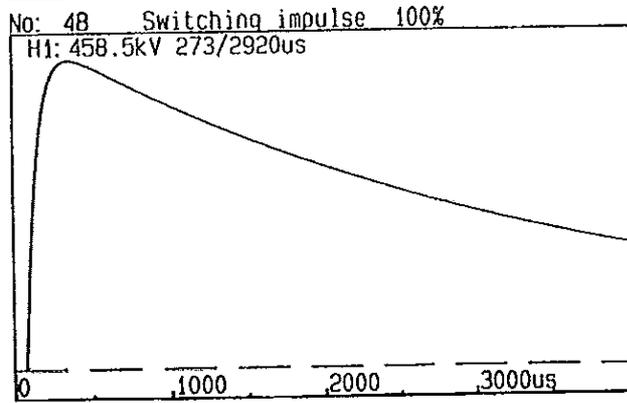
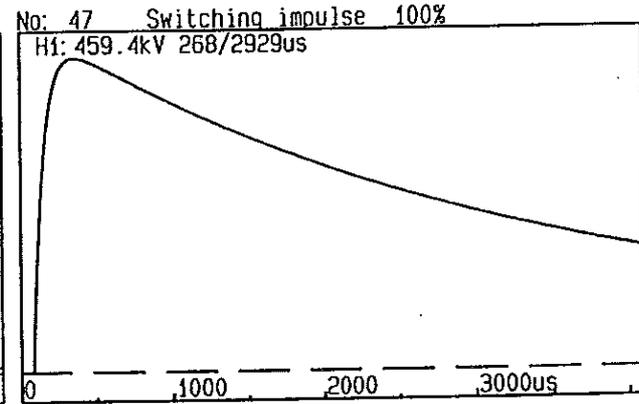
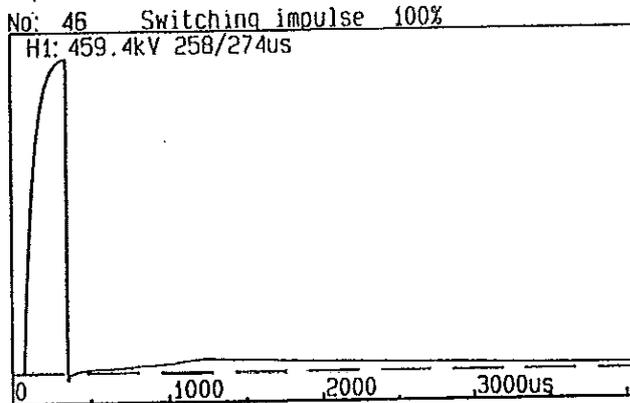
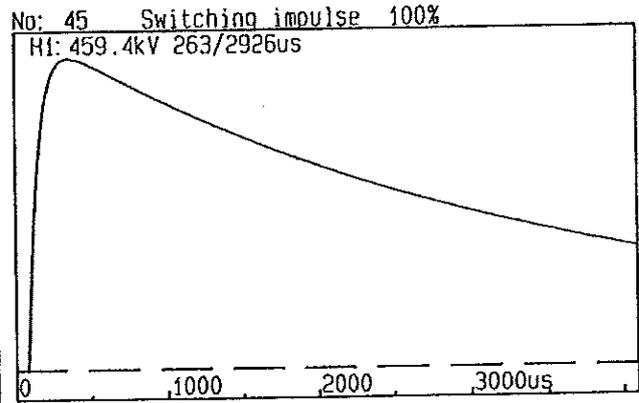
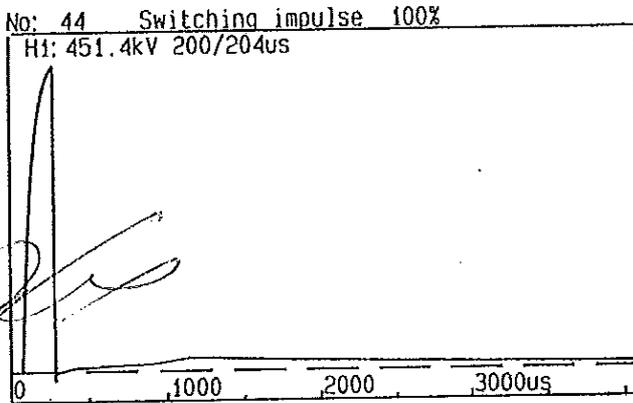
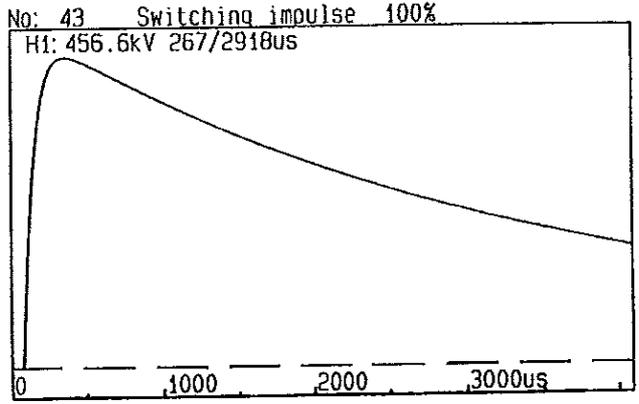
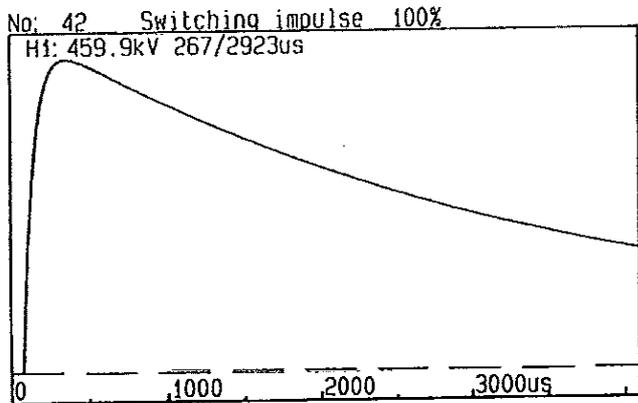
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000212

ВЯРНО С  
ОРМОНАЛА



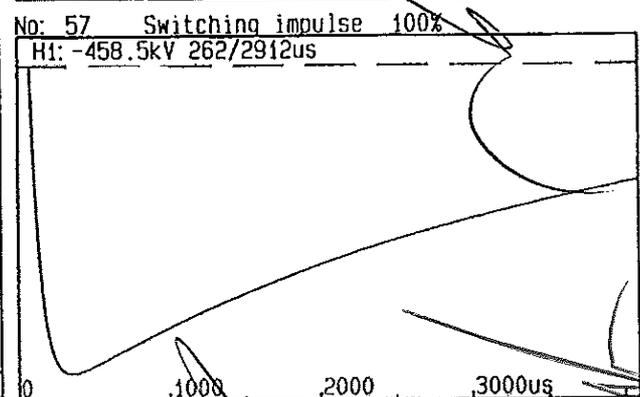
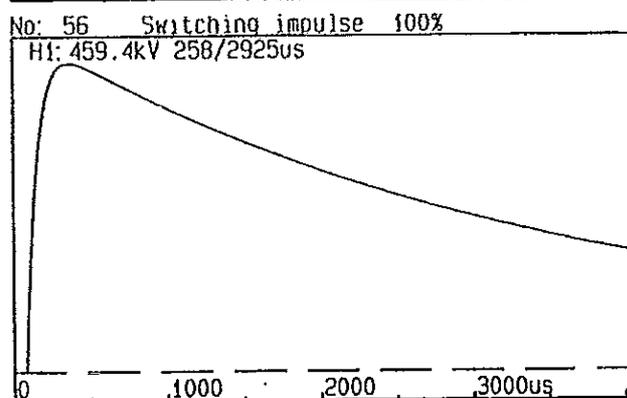
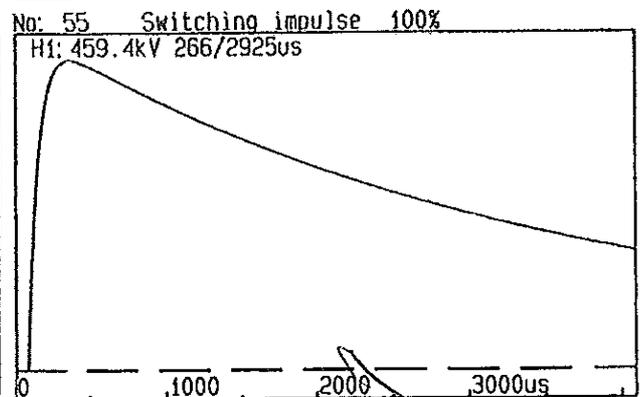
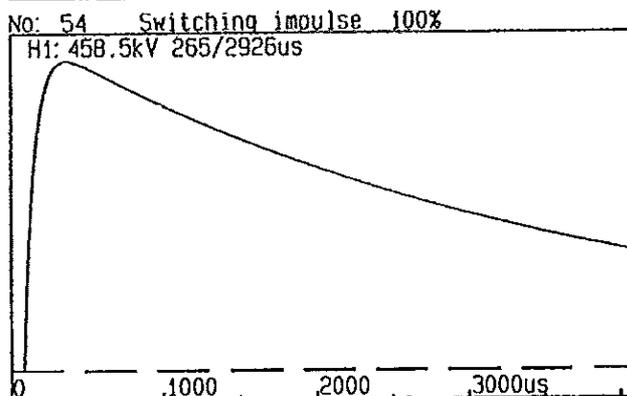
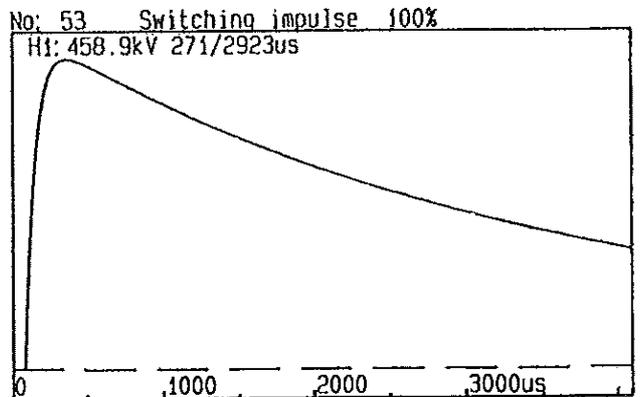
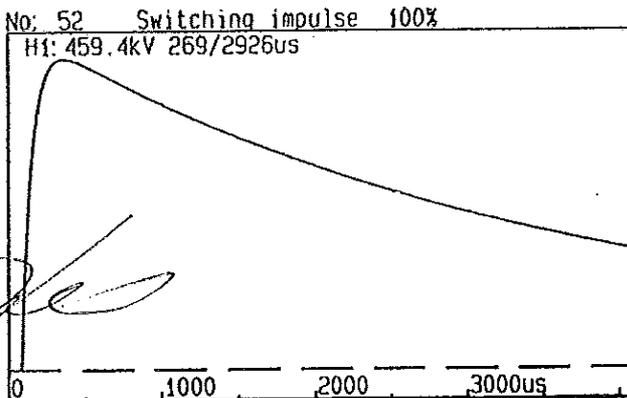
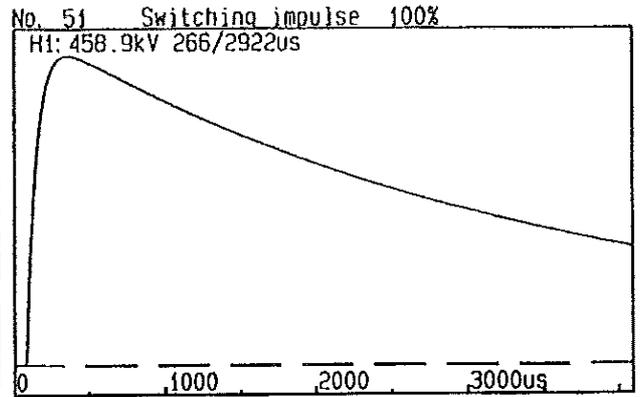
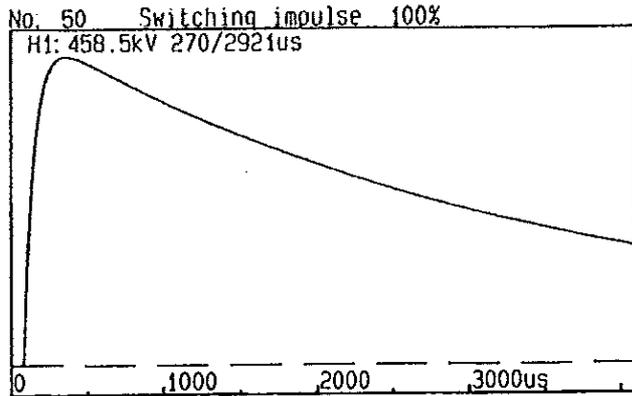
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000213

ВЯРНО С  
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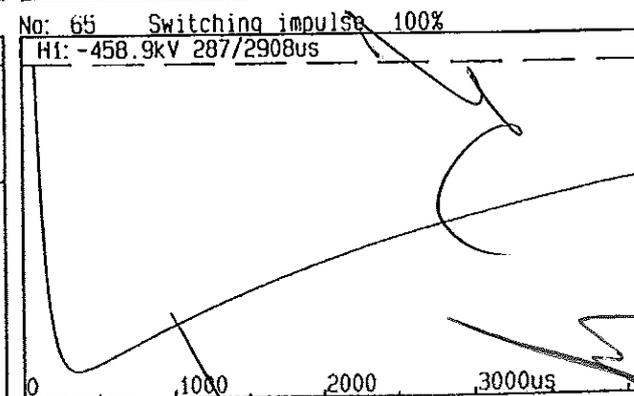
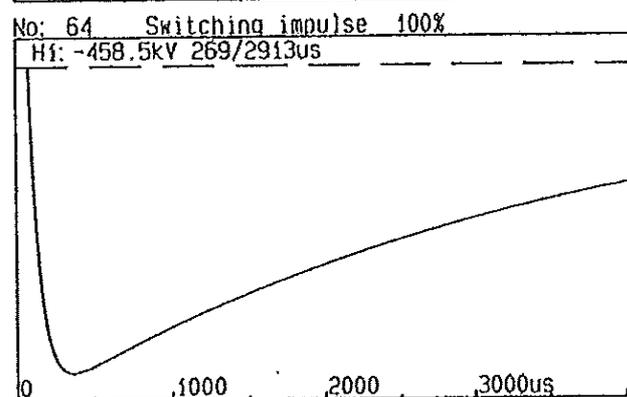
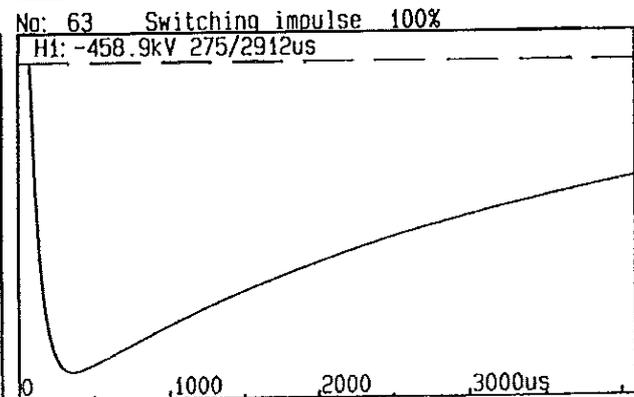
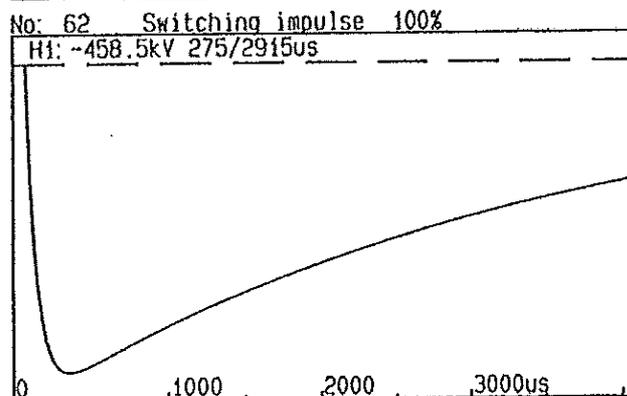
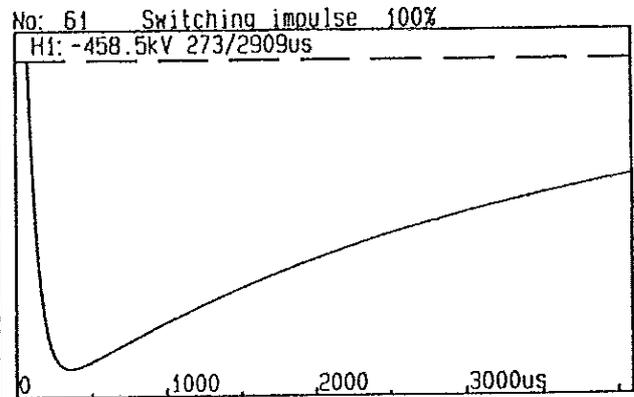
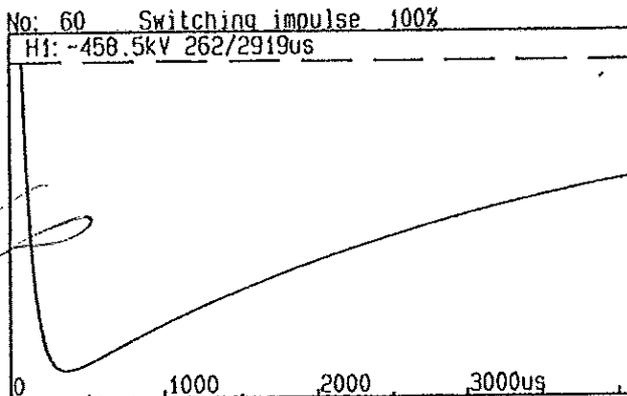
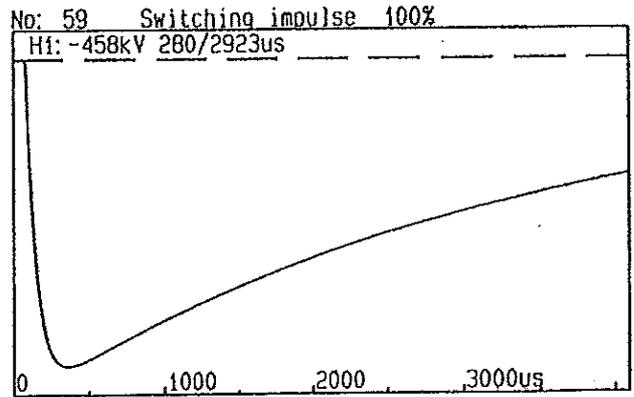
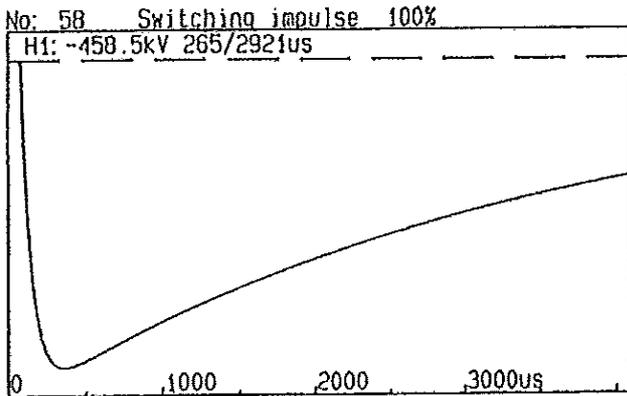




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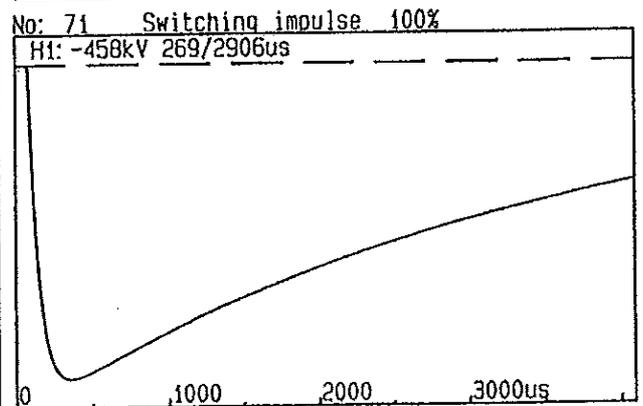
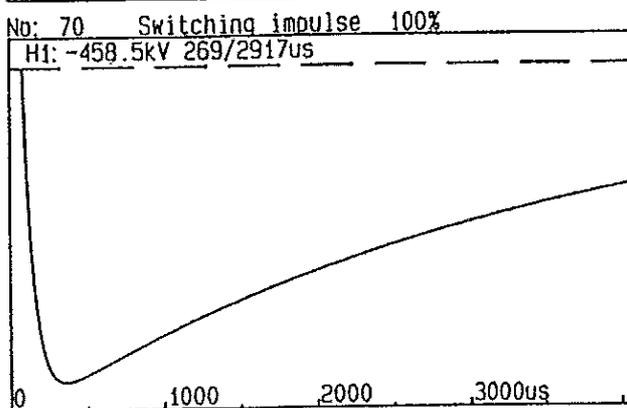
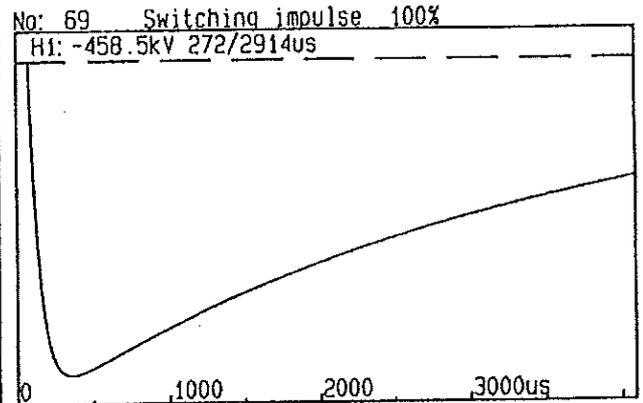
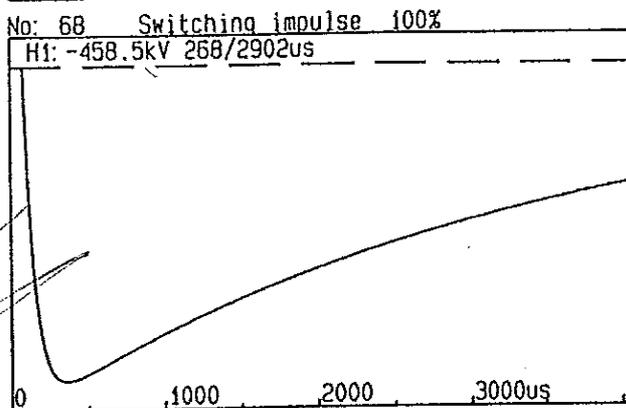
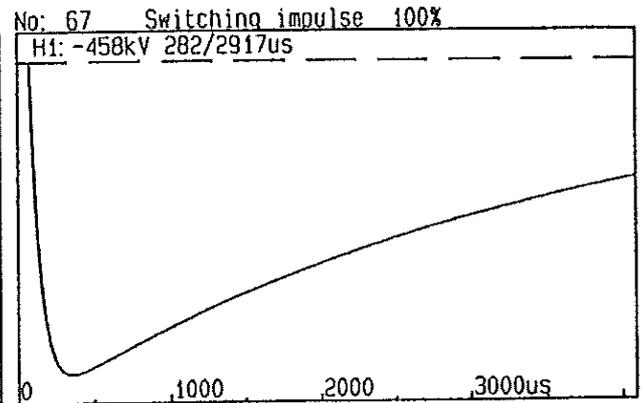
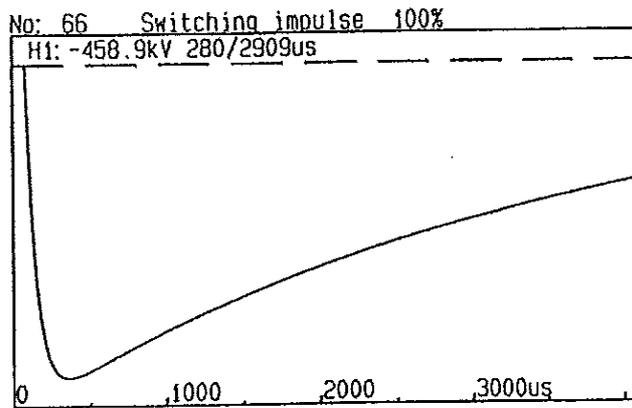




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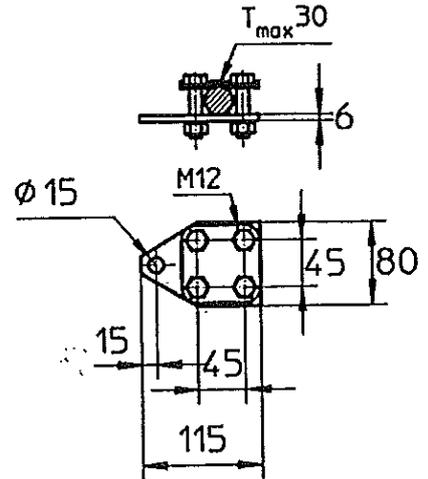
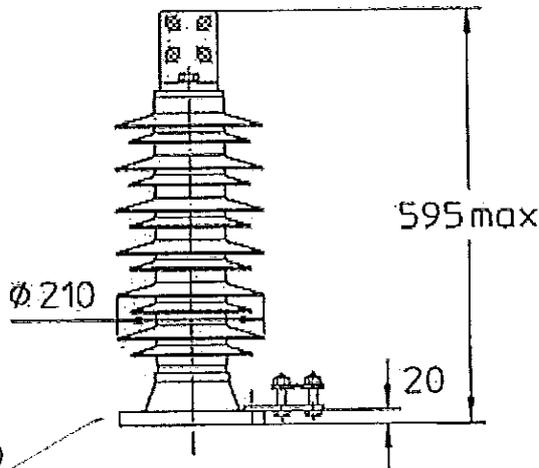
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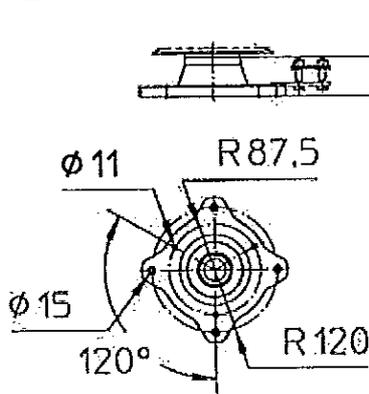


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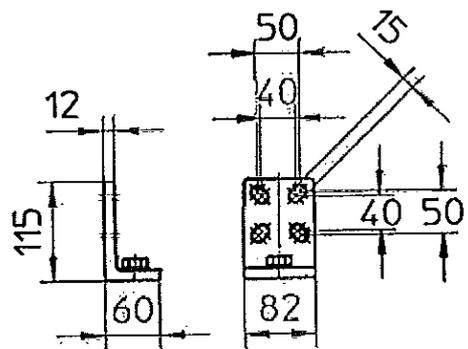
Outer dimension of a PEXLIM Q36/R36 arrester module, used in insulation withstand tests.



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LB 910 408-D



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Approved ROGER SILJEHOLM 99-08-27	Take over department		
Division <b>ABB</b> ABB Switchgear		Document no. LAK 5476	

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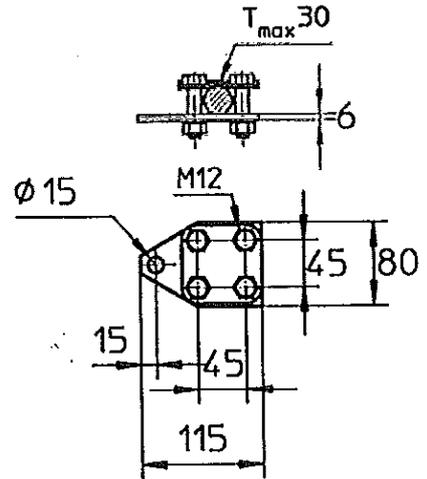
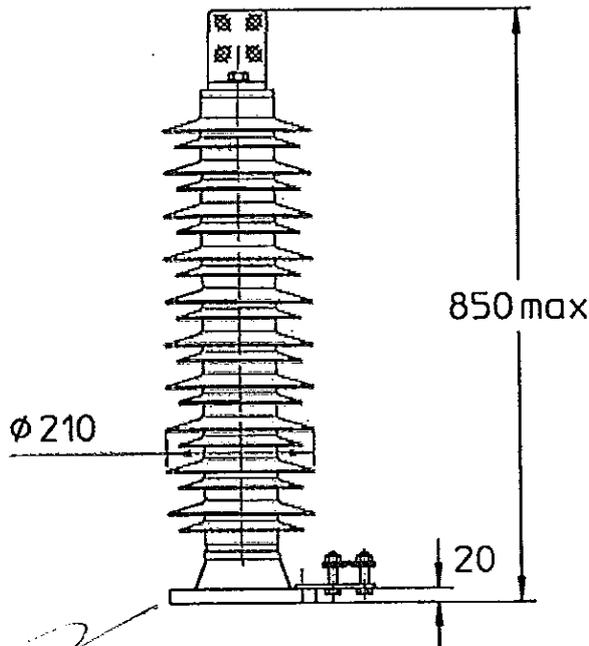
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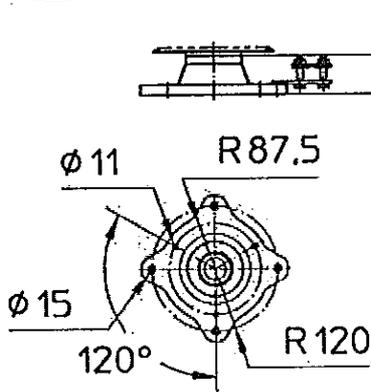
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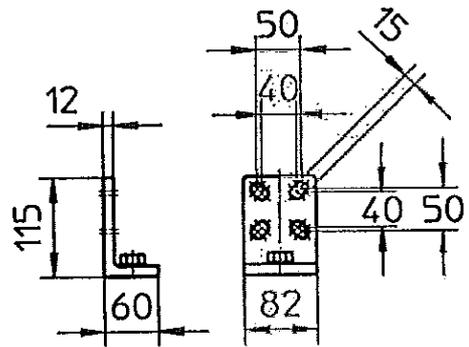
Outer dimension of a PEXLIM Q72/R72 arrester module, used in insulation withstand tests.



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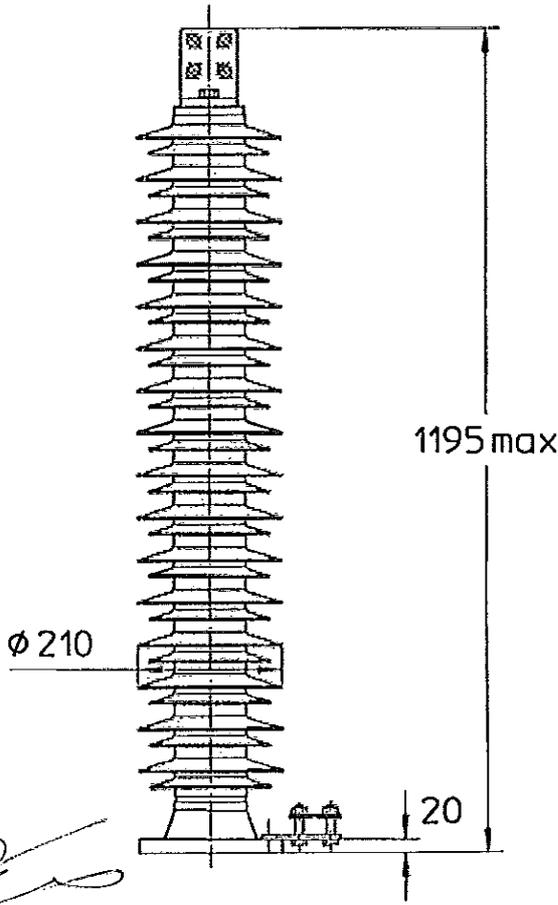
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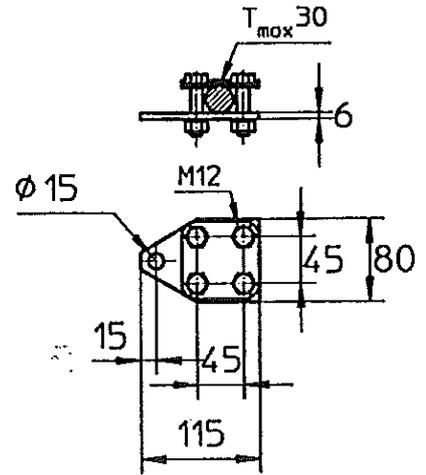


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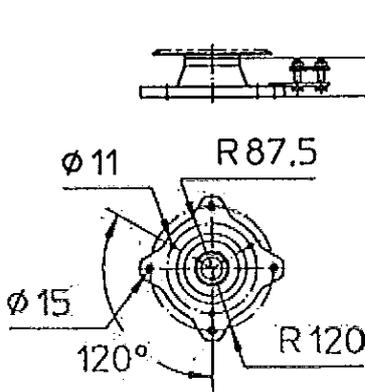
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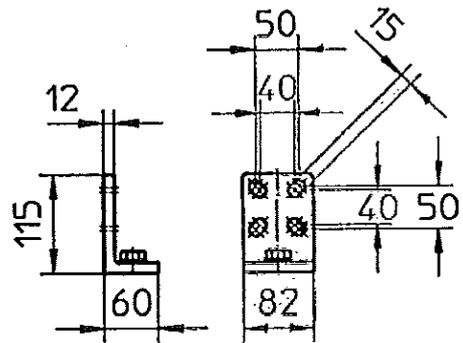
Outer dimension of a PEXLIM Q120/R120 arrester module, used in insulation withstand tests.



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ВАРФОТ  
КОМПЛЕКС  
ОРИГИНАЛ



Type tests on PEXLIM P-X surge arresters.

Test objects: Prorated arrester sections acc. to IEC, rated voltage 6.29 to 10.85 kV

Standard: IEC 60099-4, Edition 1.2, 2001-12

Test performed: Residual voltage test  
Long duration current impulse withstand test, class 4  
Operating duty test, nominal current 20 kA

Tests completed: 2004-04-23

Tests performed at: ABB Power Technologies AB - Surge Arrester Laboratory

Tests reported by: Jan-Erik Almén

Report approved by: Lennart Stenström

Report consists of: 69 pages  
Witnessing: The tests were witnessed by SATS Inspector Mr. Minoo Mobejdina.

About SATS: SATS "Scandinavian Certification" is a member of EOTC, European Group No. 0001. SATS is a member of IEC and a member of SECOC, Agreement Group No. 0001. SATS has passed the test herein.

We hereby certify that the objects specified in this report have passed the test herein.

на основании чл. 2 от 33ЛД

на основании чл. 2 от 33ЛД

CONTENTS

1 GENERAL

2 POWER FREQUENCY REFERENCE VOLTAGE TEST

3 RESIDUAL VOLTAGE TESTS

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3.3 Switching Impulse Residual Voltage Test

3.4 Summary of Residual Voltage Tests

4 LONG DURATION CURRENT IMPULSE WITHSTAND TEST

5 OPERATING DUTY TEST

5.1 Conditioning test

5.2 Switching Surge Operating Duty Test

OSCILLOGRAM PAGES  
ENCLOSURES

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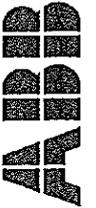
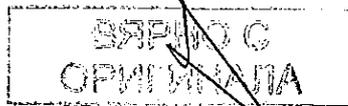


ABB Power Technologies AB

1 GENERAL

Type tests on prorated sections of ZnO arresters type PEXLIM P-X have been performed. The sections were tested in accordance with the standard for metal-oxide surge arresters, IEC 60099-4, Edition 1.2, 2001-12.

The following tests have been performed. (Clause Nos refer to the above mentioned Standard):

- Power Frequency Reference Voltage Test (this test is included in the Long Duration Current Impulse Withstand Test and the Operating Duty Test and used to determine the rated voltage of the test sections).
- Residual Voltage Tests. Clause 9.7.3.
- Long Duration Current Impulse Withstand Test. Clause 9.7.4.
- Operating Duty Test. Clause 9.7.5.

Tables and oscillograms are presented from the different tests. Representative oscillograms from tests of one section are shown from the Residual Voltage Tests. For the Long Duration Current Impulse Withstand Test and the Operating Duty Test oscillograms from tests of all sections are presented.

2 POWER FREQUENCY REFERENCE VOLTAGE TEST

The reference current for PEXLIM P-X surge arresters is defined at a peak value of 3 mA of the resistive component of power frequency current. The reference voltage ( $U_{ref}$ ) is the peak value of power frequency voltage divided by  $\sqrt{2}$  measured at the reference current. The resistive current may be slightly asymmetrical in this current region. The reference voltage, therefore, always is defined as the minimum voltage measured at the reference current independent of polarity.

The reference voltage, measured at  $23 \pm 5$  °C is checked on all complete assembled arrester units and must be equal to or higher than the nominal rated voltage, ( $U_r$ ). Furthermore, the reference voltage test is used to determine rated voltage of prorated test sections. The rated voltage of a prorated section is determined as  $U_r = U_{ref}$  in order to ensure that the prorated section is exposed to higher than or equal stresses than any complete arrester.

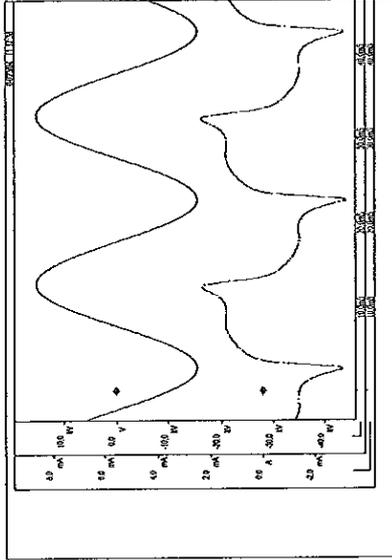
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An oscillogram from a Power Frequency Reference Voltage Test is shown below. Section rated 10.85 kVrms. (Maximum resistive current occurs by definition at the peak of the voltage wave and maximum capacitive component at voltage zero).



Voltage: 10.0 kV/div  
(10.85 kVrms)  
Current: 2.0 mA/div  
(3.0 mA resistive peak)  
Time scale: 10.0 ms/div

In Table 1 electrical data for the 9 used test sections are shown. The sections 1 to 3 consisted of one non-encapsulated varistor element (one 6 kV ZnO) block. Sections 4 to 9 consisted of two varistor elements in series (one 4.5 kV and one 6 kV block) on to which an insulator had been moulded like for the real surge arrester. Sections 4 to 9 therefore represent cross sections of a complete arrester.

Drawings for the blocks are 5681 018-501 (4.5 kV block) and 5681 018-601 (6 kV block)

Section No	Reference voltage at 3 mA peak KV rms	Rated voltage KV rms	ZnO block volume cm <sup>3</sup>	ZnO block diameter mm	Switching Impulse Residual Voltage at 500 A KV peak
1	6.30	6.30	181.8	73.8	11.27
2	6.29	6.29	"	"	11.24
3	6.30	6.30	"	"	11.25
4	10.82	10.82	318.2	73.8	19.31
5	10.82	10.82	"	"	19.33
6	10.85	10.85	"	"	19.29
7	10.83	10.83	318.2	73.8	19.29
8	10.83	10.83	"	"	19.26
9	10.83	10.83	"	"	19.39

Table 1. Electrical data for test sections

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3.3 RESIDUAL VOLTAGE TESTS

All varistor elements intended for use in PEXLIM P-X surge arresters are in routine tests classified according to their residual voltage at an impulse current of 10 kA with wave shape 8/20 μs. For the complete arresters, the varistor elements are chosen in such a way that the protective level at 10 kA 8/20 μs current wave is equal to or below 2.275 times the rated voltage of the arrester. Specified protection values for other current amplitudes and wave shapes valid for PEXLIM P-X arresters are shown in Diagram 1 on page 8 given as percentage of the residual voltage at 10 kA 8/20 μs.

The purpose of the residual voltage type test is to verify the specified protection values by establishing the ratio between the residual voltages at specified impulse currents and the voltage checked in routine tests i.e. the discharge voltage at 10 kA 8/20 μs. In order to compare with specified values in Diagram 1 all measured discharge voltages were normalized to the measured residual voltages at 10 kA 8/20 μs current impulse for each test section. The highest ratios independent of test section were thereafter plotted in Diagram 1.

3.1 Steep Current Impulse Residual Voltage Test

The test was performed on the 3 sections 1, 2 and 3 as per Table 1. Four current impulses were applied to each section with current amplitudes of approximately 1, 5, 10 and 20 kA. The virtual current front time was 1.0 μs. Before the residual voltage test, as per clause 7.3.1 of the IEC standard, a steep current impulse was applied to a metal block of the same dimensions as the ZnO varistor elements. The peak voltage measured was less than 2% of the residual voltage measured on the ZnO varistor elements, thus no correction for inductive effect was necessary.

Test results are shown in Table 2 and on osc. pages 1 and 2.

Section No	1 kA readings kA	5 kA readings kA	10 kA readings kA	10 kA readings kV	%*)
1	1.00	11.99	86.88	4.94	13.40
2	1.02	11.88	86.46	5.00	13.36
3	1.00	11.89	86.41	4.98	13.38

Section No	20 kA readings kA	20 kA readings kV	%*)
1	20.43	15.58	112.90
2	20.07	15.44	112.37
3	19.94	15.46	112.35

Table 2

\*) Percentage of the residual voltage at 10 kA 8/20 μs

3.2 Lightning Impulse Residual Voltage Test

The test was carried out on the same sections as for the Steep Current Impulse Residual Voltage Test. Six current impulses were applied to each test section with current amplitudes of approximately 0.5, 1, 5, 10, 20, 40, 50 and 65 kA and with wave shape 8/20 μs. Test results are shown in Table 3 and on osc pages 3, 4, 5 and 6.

Section No	0.5 kA readings kA	1 kA readings kA	5 kA readings kA	5 kA readings kV	%*)
1	0.50	11.38	82.46	1.02	11.76
2	0.50	11.33	82.46	1.05	11.73
3	0.51	11.34	82.41	1.02	11.73

Section No	10 kA readings kA	20 kA readings kA	40 kA readings kA	40 kA readings kV	%*)
1	9.86	13.80	100	19.86	14.85
2	9.93	13.74	100	19.97	14.79
3	9.96	13.76	100	20.01	14.81

Section No	50 kA readings kA	65 kA readings kA	65 kA readings kV	%*)
1	50.51	16.80	121.74	64.90
2	50.35	16.70	121.54	65.42
3	50.03	16.71	121.44	64.80

Table 3

\*) Percentage of the residual voltage at 10 kA 8/20 μs

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3.3 Switching Impulse Residual Voltage Test

The test was carried out on the same section as used for tests according to clauses 3.1 and 3.2. Six current impulses were applied to each section with current amplitudes of approximately 0.125, 0.25, 0.5, 1, 2 and 3 kA and with a virtual front time of 32.0 μs. Test results are shown in Table 4 and on osc pages 7, 8 and 9.

Section No	0.125 kA readings		0.25 kA readings		0.5 kA readings	
	kA	kV	kA	kV	kA	kV
1	0.121	10.71	0.249	10.97	0.496	11.27
2	0.130	10.68	0.261	10.94	0.505	11.24
3	0.121	10.71	0.255	10.96	0.501	11.25

Section No	1 kA readings		2 kA readings		3 kA readings	
	kA	kV	kA	kV	kA	kV
1	1.016	11.65	1.968	12.07	3.019	12.39
2	1.023	11.62	2.003	12.04	3.037	12.36
3	1.012	11.62	2.000	12.05	3.038	12.37

Table 4

\*) Percentage of the residual voltage at 10 kA 8/20 μs

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3.4 Summary of Residual Voltage Tests

The highest ratios in percentage of the measured 10 kA 8/20 μs residual voltage for each current amplitude and wave shape and for any of the three test sections were plotted in Diagram 1. As seen from the diagram the specified values for PEXLIM P-X surge arresters are verified since the measured ratios do not exceed the presented curves.

RESIDUAL VOLTAGES FOR ARRESTERS TYPE PEXLIM P-X

Specified protection levels and test results. Test result shown as markers

Percentage of residual voltage at 10kA 8/20 impulse

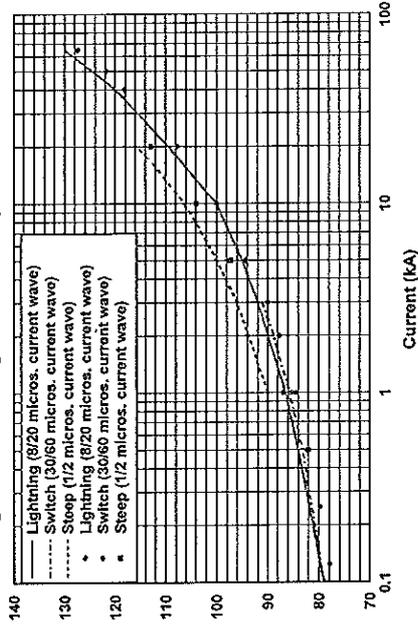


Diagram 1

4. LONG DURATION CURRENT IMPULSE WITHSTAND TEST

The three prated sections 4, 5 and 6 used in the Long Duration Current Impulse Withstand Test each consisted of two varistor elements in series on to which an insulator had been moulded. The dimensions of the varistor elements were D=73.8 mm, H=31.9 mm (4.5 kV block) and D=73.8 mm, H=42.5 mm (6 kV block). The varistor elements had not been subjected previously to any tests except that for evaluation purposes i.e. the Lightning Impulse Residual Voltage Test at nominal discharge current. Switching Impulse Residual Voltage Test and the Power Frequency Reference Voltage Test. The rated voltages of the test sections were set to 10.85 kVrms equal to the maximum reference voltage as per clause 2 for any of the sections 4 to 6. The test was run in open air at a temperature of 23 ± 5 °C. Each Long Duration Current Impulse Withstand Test was in accordance with line discharge class 4, and consisted of 18 discharge operations divided into 6 groups of 3 operations. Intervals between operations were 50-60 s and between groups sufficiently long to permit the sections to cool to near ambient temperature. Oscillographic records of the voltage across and the current through the test samples were made on the 1st and 18th operation of each test sequence.

Since the varistor elements could not be dismantled for inspection an additional Long Duration Current Impulse was applied as per the requirements in clause 9.7.4.

For test results see Table 5 and 6 and osc.pages 10 to 15.

Section No	Application No	Current peak A	Voltage peak kV	Energy kJ
4	1	953.3	19.81	57.47
4	18	921.8	20.32	56.93
5	1	934.4	19.79	57.64
5	18	915.5	20.32	56.73
6	1	956.4	19.81	57.68
6	18	918.6	20.33	56.79

Table 5. Long Duration Current Impulse Withstand Test on PEXLIM P-X sections rated 10.85 kVrms. Actual charging voltage 28.44 kV.

Note: According to clause 9.7.4 in the IEC standard the test energy must be higher than or equal to a value determined by a formula based on specified test parameters and the switching impulse residual voltage of the test sections. With the lowest relative residual voltage for any of the test sections as per Table 1 the formula results in a minimum required energy of 5.15 kJ/kV rated voltage which for a rated voltage of 10.85 kVrms corresponds to 55.92 kJ. Actual test energies exceed this value.

Section No	Application No	Current peak A	Voltage peak kV	Energy kJ
4	19	930.4	19.93	56.57
5	19	932.8	19.93	56.58
6	19	932.0	19.93	56.54

Table 6. Additional Long Duration Current Impulse Withstand Test on PEXLIM P-X sections rated 10.85 kVrms. Actual charging voltage 28.23 kV.

Parameters for the line discharge test according to class 4 on 10.85 rated test section are.

Surge impedance : 0.8 x 10.85 = 8.68 Ω

Virtual duration : 2800 μs

Charging voltage : 2.6 x 10.85 = 28.21 kV

A calibration oscillogram from the actual test circuit used with short-circuit test section is shown in Figure 1.

Current scale : 200.0 A/Div

Time scale : 1000.0 μs/div

Charging voltage : 3.0 kV

Virtual duration of current peak : 2800 μs

Transmission line length (Corresponding to virtual duration) : 420.0 km/261.03 miles

Transmission line surge impedance: 8.63 Ω

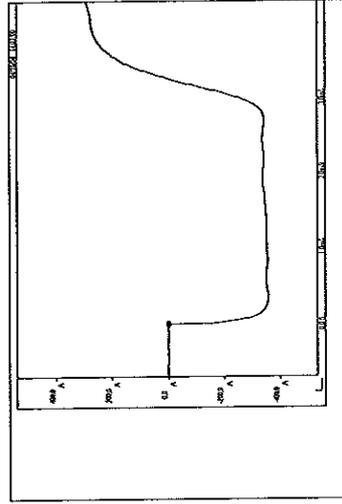


Figure 1. Calibration of test circuit with short-circuited test section

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Before and after the complete Long Duration Current Impulse Withstand Test the residual voltage at 20 kA 8/20  $\mu$ s and the reference voltage were checked to indicate any possible changes in the arrester performance. Test result is shown in Table 7.

Section	Difference after/before in residual voltage at 20 kA (%)	Difference after/before in reference voltage at 3.0 mA (%)
No		
4	+ 0.1	+ 0.6
5	+ 0.1	+ 1.2
6	+ 0.1	+ 0.7

Table 7

Examination of the test samples after the test revealed no evidence of puncture, flashover, cracking or other significant damage of the varistor elements.

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5 OPERATING DUTY TEST

The three prated sections 7, 8 and 9 used in the Operating Duty Test each consisted of two varistor elements in series on to which an insulator had been moulded. The dimensions of the varistors elements were D=73.8 mm, H=31.9 mm (4.5 kV block) and D=73.8 mm, H=42.5 mm (6kV block). The test was carried out on new varistor elements which had not been subjected to any previous tests except that for evaluation purposes, i.e. Lightning Impulse Residual Voltage Test at nominal discharge current, Switching Impulse Residual Voltage Test and the Power Frequency Reference Voltage Test. The series of stresses which the sections were exposed to are illustrated in Figure 2 on page 19. Some of these tests as shown in figure 2 were performed on the test sections thermally insulated at top and bottom ends as shown in Enclosure 1:1 in order to represent true thermal models of the complete arrester. The thermally prated sections for arresters type PEXLIM P-X are verified in test report HVPIAK 04-24. The rated voltages of the test sections were set to 10.83 kVrms equal to the maximum reference voltage for any of the sections 7 to 9 as per clause 2.

5.1 Conditioning test

The three test sections were first exposed to 20 current impulses with peak values of 20 kA and wave shape 8/20  $\mu$ s in four groups of 5 impulses. The impulses were superimposed on a power frequency voltage not less than the reference voltage of the samples<sup>\*)</sup>. The interval between the impulses was 50-60 s and the interval between groups 25-30 minutes. Between groups of impulses the test samples were not energized. The polarity of the current impulse was the same as that of the half cycle of power frequency voltage during which it occurred and it was applied 60  $\pm$  15 electrical degrees before the peak of the power frequency voltage. The test was carried out on the sections without thermal insulation at top and bottom ends in open air at a temperature of 23  $\pm$  5°C. This test was followed by two high current impulses with an impulse shape of 4/10  $\mu$ s and a peak value of 100 kA. The sections were allowed to cool to ambient temperature between the impulses. The sections were not preheated and the test was carried out at an ambient temperature of 23  $\pm$  5°C. The test result from the conditioning test is shown in Tables 8 and 9 and on osc. pages 16 to 21.

\*) The required voltage as per IEC 60099-4 is the Continuous Operating Voltage,  $U_c$ , +20%. With a maximum  $U_c$  for PEXLIM P-X arresters of 80% of rated voltage the applied voltage represents  $U_c$  +25%.

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Section No	Application No	Impulse Current kA peak	Power frequency voltage kV rms
7	1	20.22	10.83
7	20	20.74	10.84
8	1	20.21	10.83
8	20	20.74	10.86
9	1	20.23	10.83
9	20	20.48	10.86

Table 8. Conditioning test with 20 kA, 8/20  $\mu$ s impulse. Sections rated 10.83 kVrms. impulse current shape 8/20  $\mu$ s

Section No	Application No	Current peak kA	Voltage peak kV
7	1	101.11	33.47
7	2	101.43	33.51
8	1	101.04	33.47
8	2	100.85	33.39
9	1	100.66	33.46
9	2	100.27	33.39

Table 9. High current conditioning test. Sections rated 10.83 kVrms. Current wave shape 4/10  $\mu$ s.

5.2 Switching Surge Operating Duty Test

At the beginning of the Switching Surge Operating Duty Test the test sections were equipped with thermally insulating covers at the top and bottom ends as shown in Enclosure 1.11 in order to represent true thermal models of the complete arrester and preheated to  $60 \pm 3$  °C. Thereafter the sections were rapidly brought to the test chamber which had an ambient temperature of  $23 \pm 5$  °C and subjected to two long duration current impulses according to class 4 with a time interval between the impulses of 50-60 seconds. In less than 100 ms (actually 66.9 ms) after the second current impulse a power frequency voltage not less than the rated voltage was applied for 10 seconds. After 10 seconds the voltage was decreased to 0.87 times the rated voltage<sup>7)</sup> and applied during 30 minutes before the sections were disconnected from the voltage source and permitted to cool to ambient temperature  $23 \pm 5$  °C. Leakage current and temperature were measured during the test sequence to prove thermal stability and ability of the test sections to cool after the switching surges and overvoltage application against 0.87 times the rated voltage. Oscillograms from the test are shown on osc pages 22 to 30. Temperature increase and cooling are shown in Figure 3, 4 and 5 for test sections No.7, 8 and 9. The test result from the two long duration current impulses is given in Table 10.

Section No	Application No	Current peak A	Voltage peak kV	Energy kJ
7	1	1077.0	20.36	66.40
7	2	1064.0	20.71	66.65
8	1	1080.0	20.35	66.68
8	2	1066.0	20.70	66.67
9	1	1075.0	20.43	66.55
9	2	1057.0	20.76	66.26

Table 10. Long Duration Current Impulse Withstand Test on PEXLIM P-X sections rated 10.83 kVrms. Actual charging voltage 30.08 kV. The total energy in the two line discharges corresponds to at least 12.2 kJ/kV rated voltage.

<sup>7)</sup> With a maximum  $U_c$  for PEXLIM P-X arresters of 80% of rated voltage the applied voltage is 1.10 times higher.

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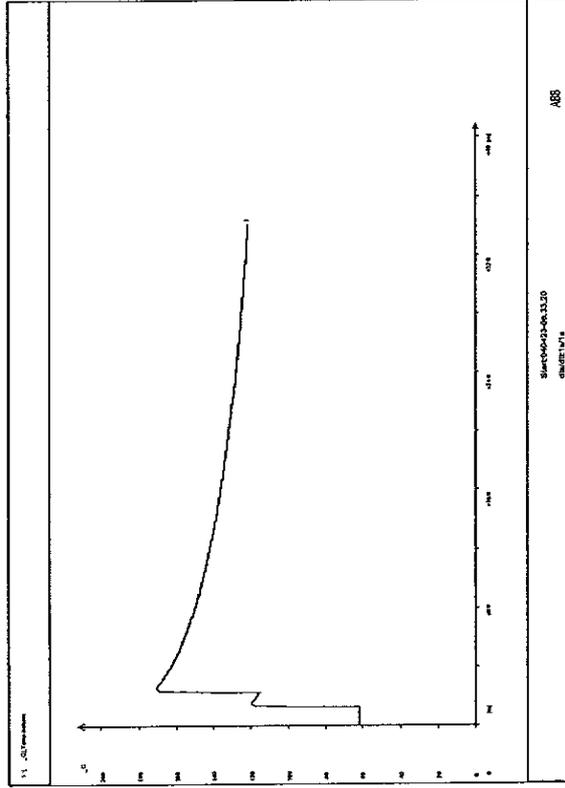


Figure 4. Temperature increase and cooling during the test sequence on section No. 8.  
(Temperature measured on the surface of the bottom varistor in the test section.)

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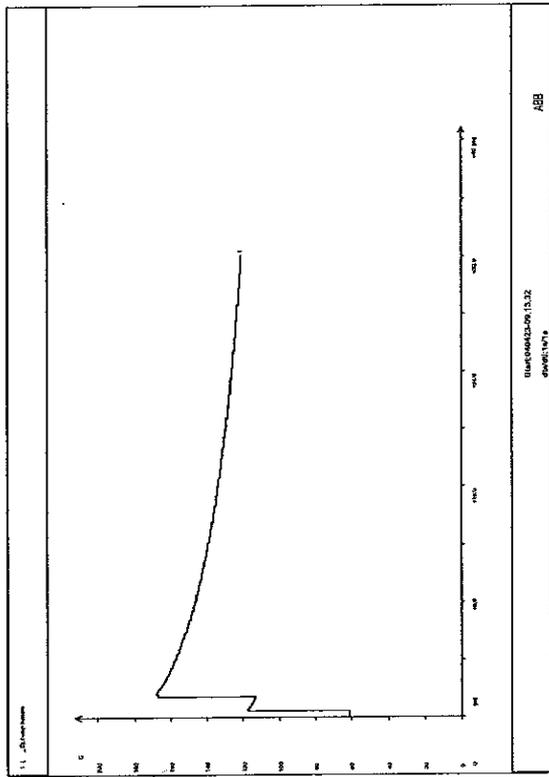


Figure 3. Temperature increase and cooling during the test sequence on section No. 7.  
(Temperature measured on the surface of the bottom varistor in the test section.)

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Since the varistor elements could not be dismantled for inspection an additional Long Duration Current Impulse was applied, after the complete operating duty test as per the requirements in clause 5.7.5

Test results are shown in table 12 and on oscillogram pages 31 to 32.

Section No	Application No	Current peak A	Voltage peak kV	Energy kJ
7	3	917.8	20.03	55.93
8	3	928.1	19.98	56.52
9	3	919.4	20.05	56.00

Table 12. Additional Long Duration Current Impulse Withstand Test on PEXLIM P-X sections rated 10.83 kVrms. Actual charging voltage 28.30 kV.

Before the complete operating duty test the residual voltage at 20 kA 8/20  $\mu$ s and the reference voltage were measured. After the tests as per the requirements in clause 9.7.5 two shots at 20 kA 8/20  $\mu$ s were applied on the sections after they had been permitted to cool to ambient temperature, and the second shot in less than 60 seconds after the first shot. The reference voltages also were measured to check if any possible changes in the arrester performance had occurred.

Test results are shown in tables 13 and 14 and on oscillogram pages 33 to 38.

Section No	Application No	Current peak kA	Voltage peak kV
7	1*)	20.22	25.64
7	2	19.81	25.95
7	3	19.93	25.98
8	1*)	20.22	25.60
8	2	19.94	25.92
8	3	20.06	25.95
9	1*)	20.15	25.67
9	2	20.01	25.95
9	3	19.97	25.97

Table 13

\*) Application No.1 was measured before operating duty test.

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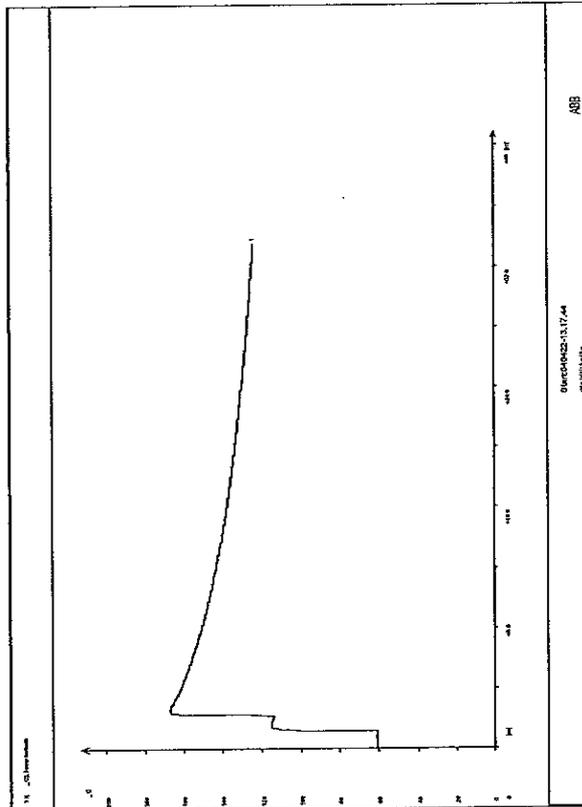


Figure 5. Temperature increase and cooling during the test sequence on section No.9. (Temperature measured on the surface of the bottom varistor in the test section.)

ВЕРНО С  
ОРИГИНАЛА



Section No	Difference after/before in residual voltage at 20 kA (%)	Difference after/before in reference voltage at 3.0 mA (%)
7	+ 1.2	+ 2.0
8	+ 1.3	+ 2.2
9	+ 1.1	+ 2.3

Table 14

Examination of the test samples after the test revealed no evidence of puncture, flashover, cracking or other significant damage of the varistor elements.

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OPERATING DUTY TEST ON PEXLIM P-X - COMPLETE SEQUENCE

SEQUENCE No	EXPLANATION OF PROCEDURE
1	Reference voltage measurement at 3.0 mA resistive current
2	Residual voltage measurement at 20 kA 8/20 $\mu$ s
3	Conditioning test: 4 groups of 5 impulses at 20 kA 8/20 $\mu$ s superimposed on rated voltage (continuous operating voltage, $U_b$ , +25% ) (Required as per IEC: $U_c$ +20% )
4	High current impulse (100 kA, 4/10 $\mu$ s) Cooling to ambient temperature High current impulse (100 kA, 4/10 $\mu$ s)
5	Sections mounted in thermally prorated sections
6	Preheating to $60 \pm 3$ °C
7	Rapidly brought to test chamber ( $23 \pm 5$ °C)
8	Long duration current impulse Class 4
9	50 - 60 seconds
10	Long duration current impulse Class 4
11	Time space less than 100 milliseconds
12	Rated voltage, 10 seconds
13	0.87 times rated voltage ( $1.10 \cdot U_c$ ), 30 minutes (Required as per IEC: $U_c$ )
14	Cooling to ambient temperature, ( $23 \pm 5$ °C)
15	Additional long duration current impulse - Class 4, and examination of test samples
16	cooling to ambient temperature, ( $23 \pm 5$ °C)
17	Reference voltage measurement at 3.0 mA resistive current
18	Residual voltage measurement at 20 kA, 8/20 $\mu$ s Less than 60 seconds Residual voltage measurement at 20 kA, 8/20 $\mu$ s
19	Examination of test samples and oscillographic records from residual voltage measurements

Figure 2.  
Sequence No.

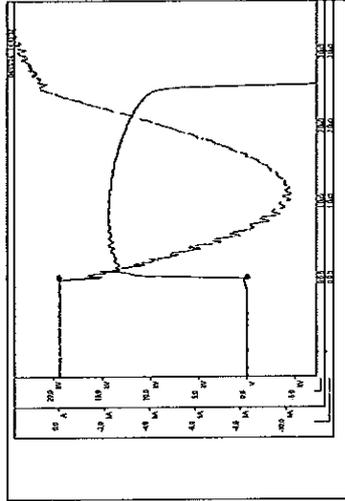
- 1 - 2 : Initial measurement - sections not thermally insulated
- 3 - 4 : Conditioning - sections not thermally insulated
- 5 - 13 : Switching surge operating duty test
- 14 - 19 : Measurement and examination - sections not thermally insulated.

Steep current impulse residual voltage test

Section rated 6.30 kV/rms

Section No. 1

Time scale: 1.0  $\mu$ s/div



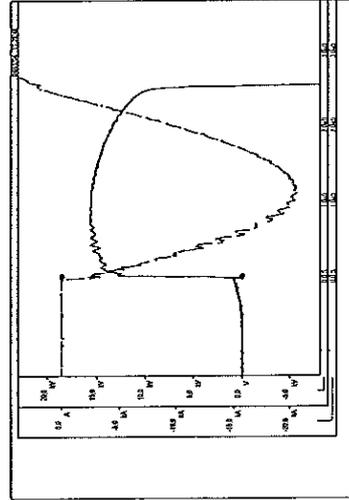
Voltage: 5.00 kV/div  
(14.34 kV)

Current: 2.00 kA/div  
(10.06 kA)

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Voltage: 5.00 kV/div  
(15.58 kV)

Current: 5.00 kA/div  
(20.43 kA)



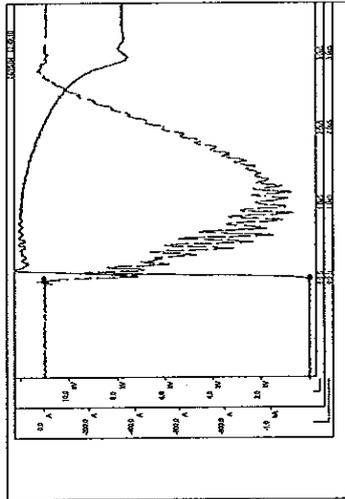
OSCILLOGRAM PAGES

Steep current impulse residual voltage test

Section rated 6.30 kV/rms

Section No. 1

Time scale: 1.0  $\mu$ s/div



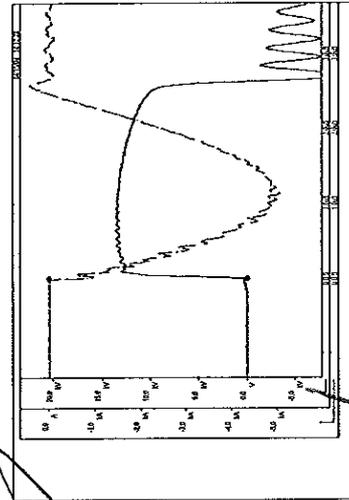
Voltage: 2.00 kV/div  
(11.99 kV)

Current: 200.0 A/div  
(1.00 kA)

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Voltage: 5.00 kV/div  
(13.40 kV)

Current: 1.00 kA/div  
(4.94 kA)



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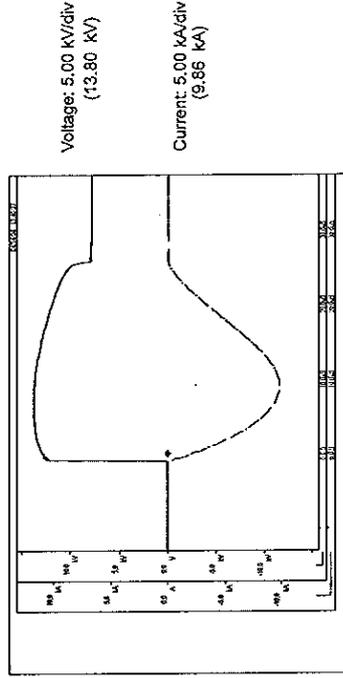
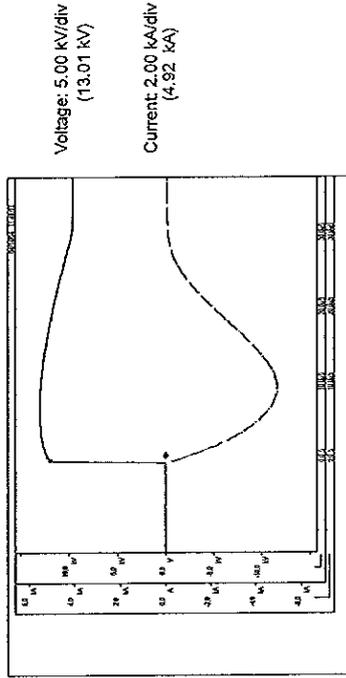
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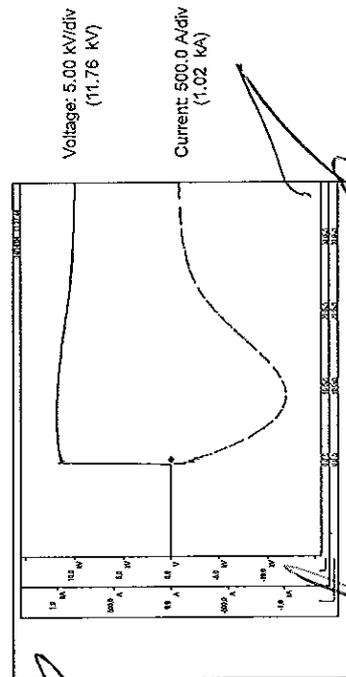
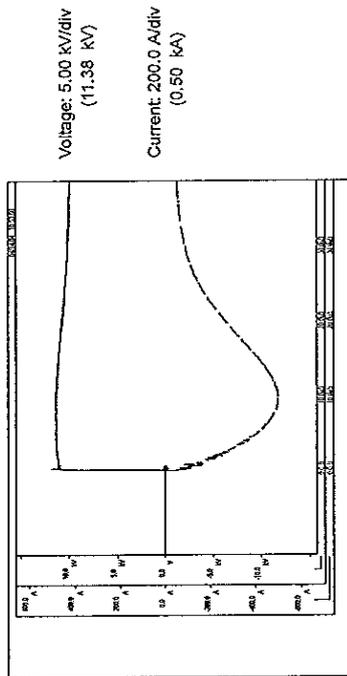
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Lighting impulse residual voltage test  
Section rated 6.30 kV/rms  
Section No. 1  
Time scale: 10.0  $\mu$ s/div



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Lighting impulse residual voltage test  
Section rated 6.30 kV/rms  
Section No. 1  
Time scale: 10.0  $\mu$ s/div



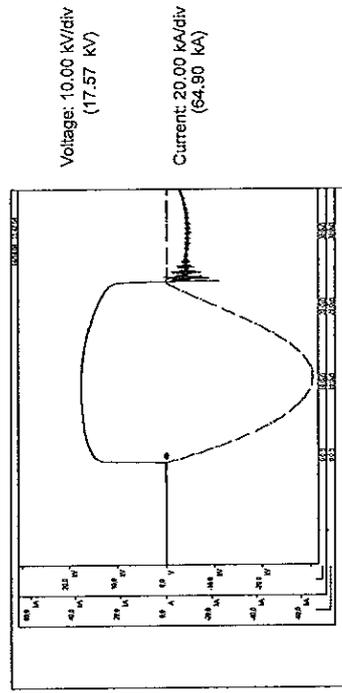
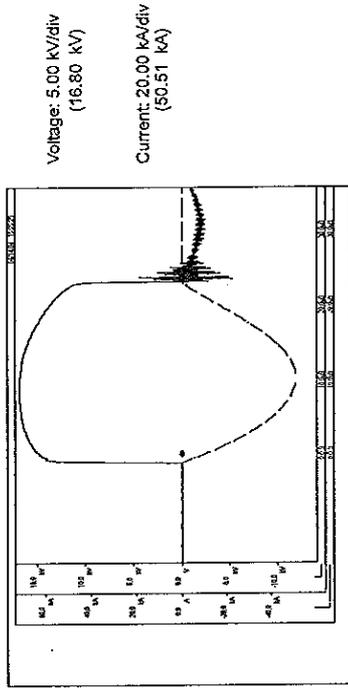
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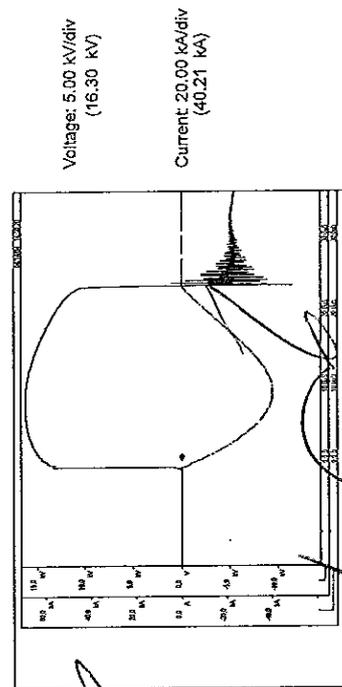
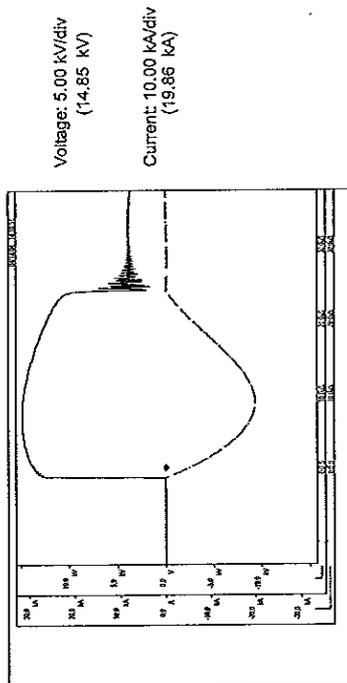


Lightning impulse residual voltage test  
Section rated 6.30 kVrms  
Section No. 1  
Time scale: 10.0  $\mu$ s/div



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Lightning impulse residual voltage test  
Section rated 6.30 kVrms  
Section No. 1  
Time scale: 10.0  $\mu$ s/div



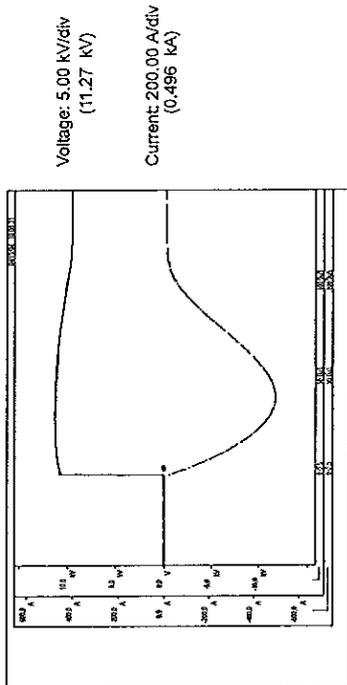
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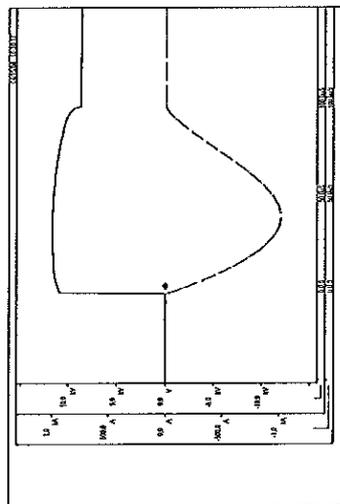
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Switching impulse residual voltage test  
Section rated 6.30 kVrms  
Section No. 1  
Time scale: 50.0  $\mu$ s/div

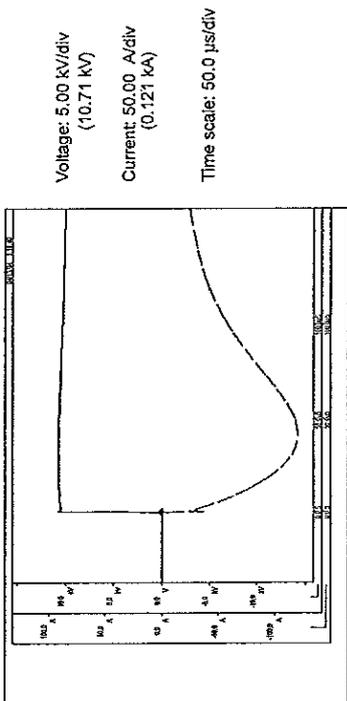


Voltage: 5.00 kV/div  
(11.65 kV)  
Current: 500.0 A/div  
(1.016 kA)

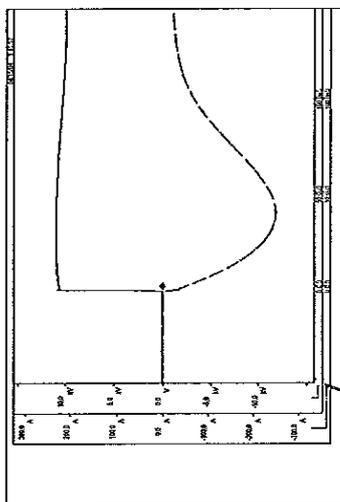


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Switching impulse residual voltage test  
Section rated 6.30 kVrms  
Section No. 1



Voltage: 5.00 kV/div  
(10.97 kV)  
Current: 100.00 A/div  
(0.249 kA)  
Time scale: 50.0  $\mu$ s/div



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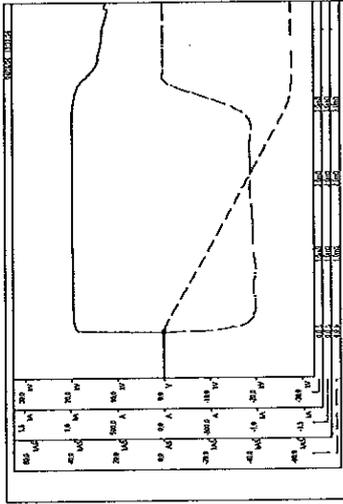
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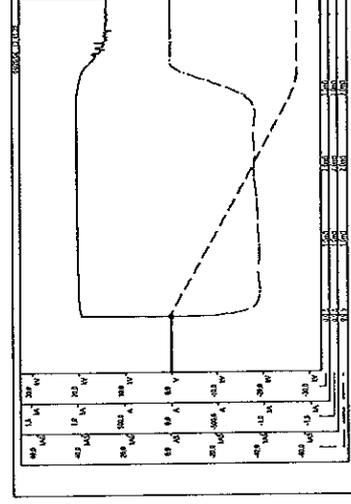
Long duration current impulse withstand test  
Section rated 10.82 kVrms

Section No. 4  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div

1st application  
Voltage: 19.81 kV  
Current: 953.3 A  
Energy: 57.47 kJ



18th application  
Voltage: 20.32 kV  
Current: 921.8 A  
Energy: 56.93 kJ



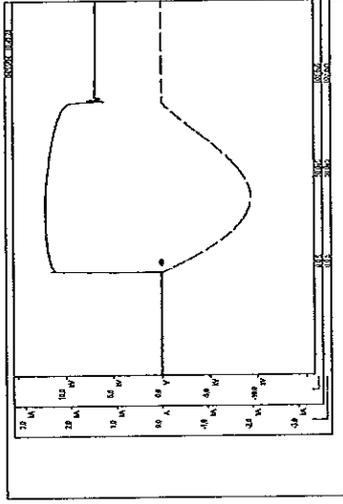
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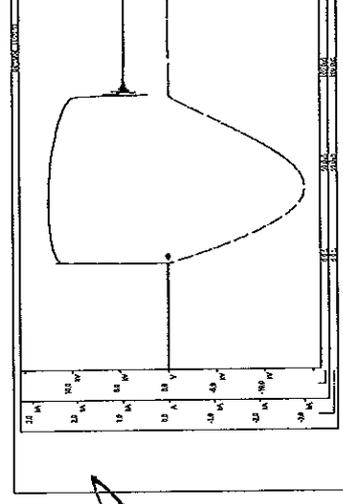
Switching impulse residual voltage test  
Section rated 6.30 kVrms

Section No. 1  
Time scale: 50.0  $\mu$ s/div

Voltage: 5.00 kV/div  
(12.07 kV)  
Current: 1.00 kA/div  
(1.968 kA)



Voltage: 5.00 kV/div  
(12.39 kV)  
Current: 1.00 kA/div  
(3.019 kA)



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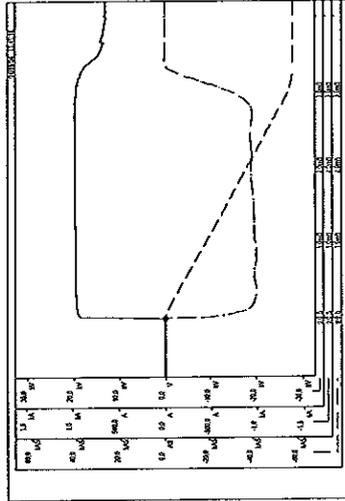
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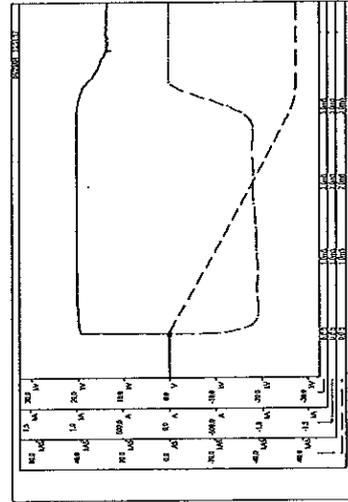


Long duration current impulse withstand test  
Section rated 10.82 kVrms

Section No. 5  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div



1st application  
Voltage: 19.79 kV  
Current: 934.4 A  
Energy: 57.64 kJ

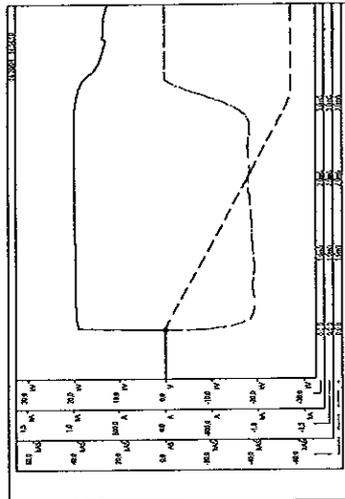


18th application  
Voltage: 20.32 kV  
Current: 915.5 A  
Energy: 56.73 kJ

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Long duration current impulse withstand test  
Section rated 10.82 kVrms

Section No. 4  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div



19th application  
Voltage: 19.93 kV  
Current: 930.4 A  
Energy: 56.57 kJ

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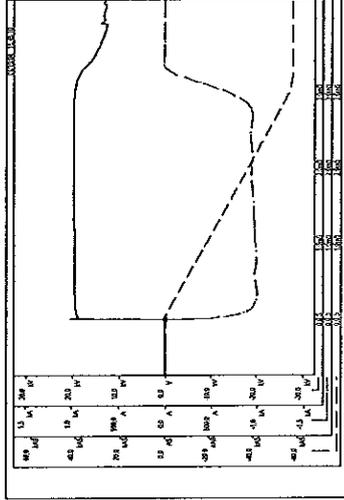
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Long duration current impulse withstand test  
Section rated 10.85 kVrms

Section No. 6  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div

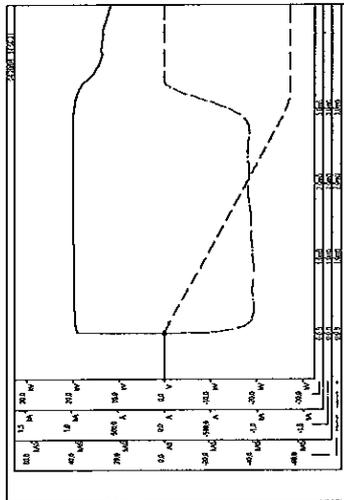


1st application  
Voltage: 19.81 kV  
Current: 956.4 A  
Energy: 57.68 kJ

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Long duration current impulse withstand test  
Section rated 10.82 kVrms

Section No. 5  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div



19th application  
Voltage: 19.93 kV  
Current: 932.8 A  
Energy: 56.68 kJ

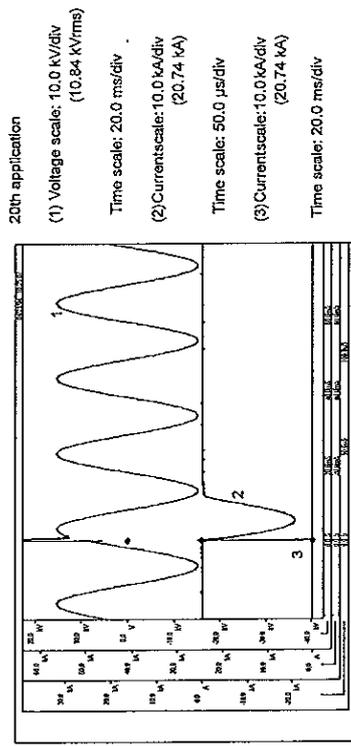
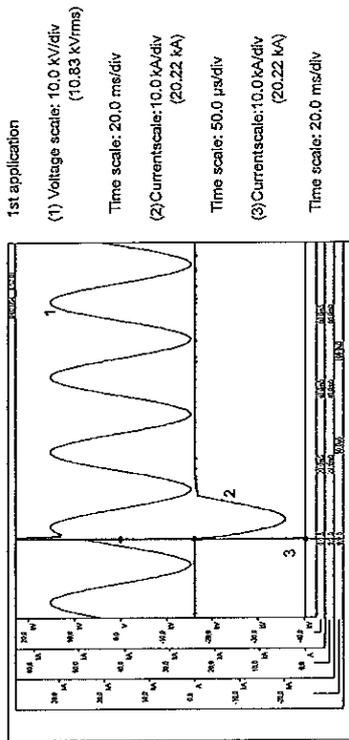
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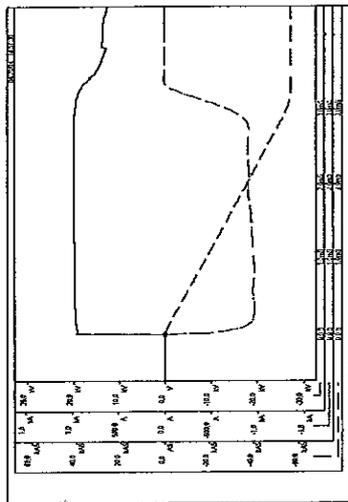
Operating duty test  
Conditioning test with 20 kA 8/20  $\mu$ s superimposed  
on continuous operating voltage +25%  
Section No.7. rated 10.83 kV/rms



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Long duration current impulse withstand test  
Section rated 10.85 kV/rms

Section No. 6  
Time scale: 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale: 20.0 kJ/div



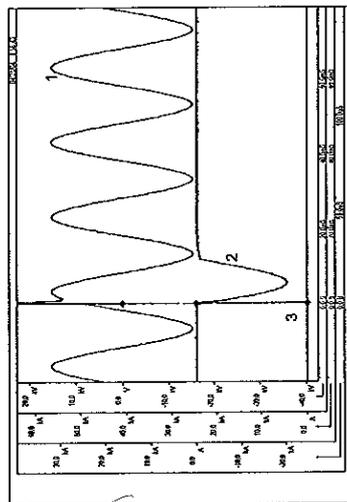
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Operating duty test  
Conditioning test with 20 kA 8/20  $\mu$ s superimposed  
on continuous operating voltage +25%  
Section No.8. rated 10.83 kVrms



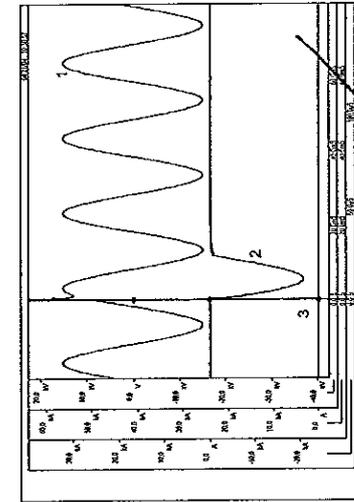
1st application  
(1) Voltage scale: 10.0 kV/div  
(10.83 kVrms)  
Time scale: 20.0 ms/div  
(2) Current scale: 10.0 kA/div  
(20.22 kA)  
Time scale: 50.0  $\mu$ s/div  
(3) Current scale: 10.0 kA/div  
(20.22 kA)  
Time scale: 20.0 ms/div

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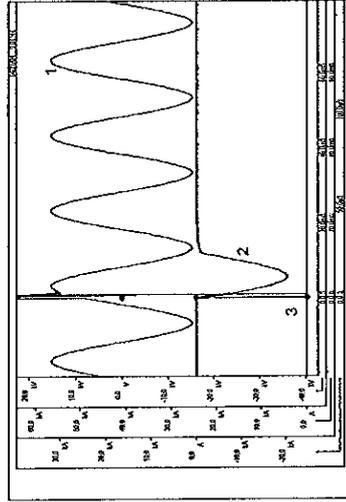
000238

20th application

(1) Voltage scale: 10.0 kV/div  
(10.86 kVrms)  
Time scale: 20.0 ms/div  
(2) Current scale: 10.0 kA/div  
(20.74 kA)  
Time scale: 50.0  $\mu$ s/div  
(3) Current scale: 10.0 kA/div  
(20.74 kA)  
Time scale: 20.0 ms/div



Operating duty test  
Conditioning test with 20 kA 8/20  $\mu$ s superimposed  
on continuous operating voltage +25%  
Section No.9. rated 10.83 kVrms

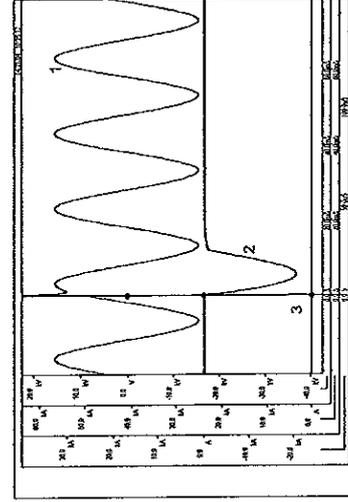


1st application  
(1) Voltage scale: 10.0 kV/div  
(10.83 kVrms)  
Time scale: 20.0 ms/div  
(2) Current scale: 10.0 kA/div  
(20.23 kA)  
Time scale: 50.0  $\mu$ s/div  
(3) Current scale: 10.0 kA/div  
(20.23 kA)  
Time scale: 20.0 ms/div

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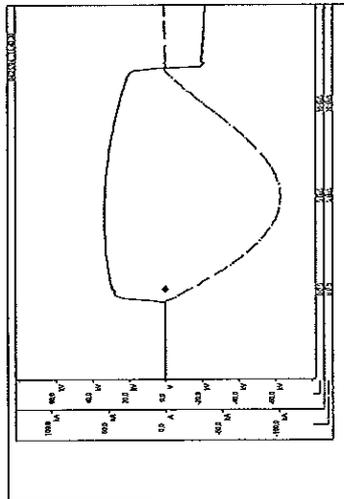
20th application

(1) Voltage scale: 10.0 kV/div  
(10.86 kVrms)  
Time scale: 20.0 ms/div  
(2) Current scale: 10.0 kA/div  
(20.48 kA)  
Time scale: 50.0  $\mu$ s/div  
(3) Current scale: 10.0 kA/div  
(20.48 kA)  
Time scale: 20.0 ms/div



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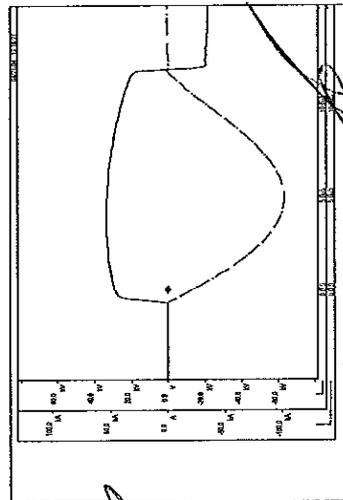
Operating duty test  
Conditioning test with high current impulse (100 kA 4/10  $\mu$ s)  
Section No.7 rated 10.83 kVrms  
Time scale : 5.0  $\mu$ s/div  
Voltage scale: 20.0 kV/div  
Current scale: 50.0 kA/div



1st application  
Voltage: 33.47 kV  
Current: 101.11 kA

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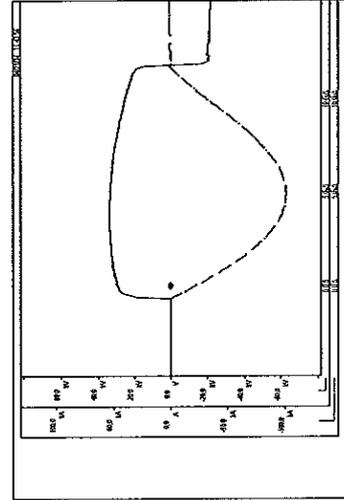
2nd application  
Voltage: 33.51 kV  
Current: 101.43 kA



ВЯРНО С  
ОРИГИНАЛА

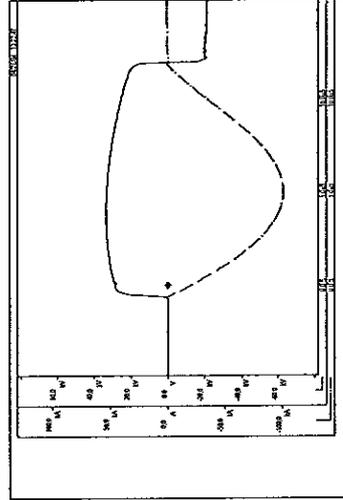


Operating duty test  
Conditioning test with high current impulse (100 kA 4/10  $\mu$ s)  
Section No.8 rated 10.83 kVrms  
Time scale : 5.0  $\mu$ s/div  
Voltage scale: 20.0 kV/div  
Current scale: 50.0 kA/div



1st application  
Voltage: 33.47 kV  
Current: 101.04 kA

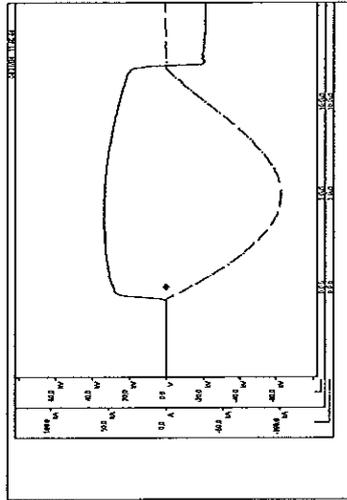
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2nd application  
Voltage: 33.39 kV  
Current: 100.85 kA



Operating duty test  
Conditioning test with high current impulse (100 kA 4/10  $\mu$ s)  
Section No.9 rated 10.83 kVrms  
Time scale : 5.0  $\mu$ s/div  
Voltage scale: 20.0 kV/div  
Current scale: 50.0 kA/div



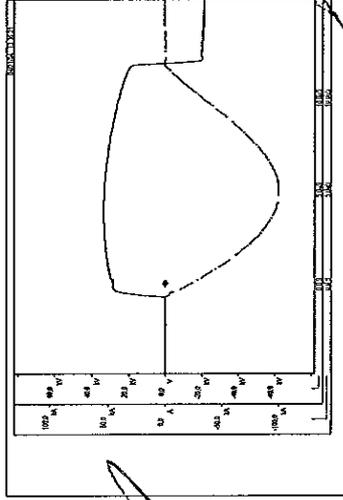
1st application

Voltage: 33.47 kV

Current: 100.66 kA

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2nd application

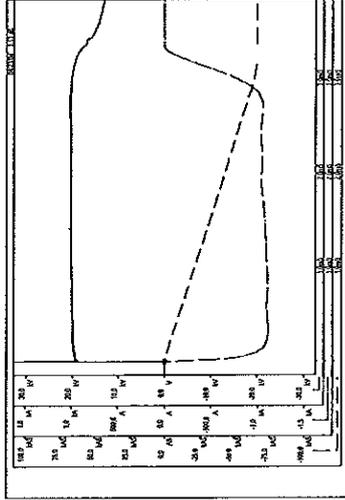
Voltage: 33.39 kV

Current: 100.27 kA

ВЯРНІС  
ОРИГІНАЛ



Switching surge operating duty test  
Long duration current impulse  
Section No.7, rated 10.83 kVrms  
Time scale : 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale : 25.0 kJ/div



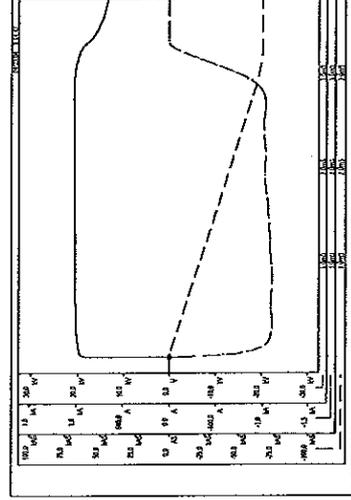
1st application

Voltage: 20.96 kV

Current: 1077.0 A

Energy: 66.40 kJ

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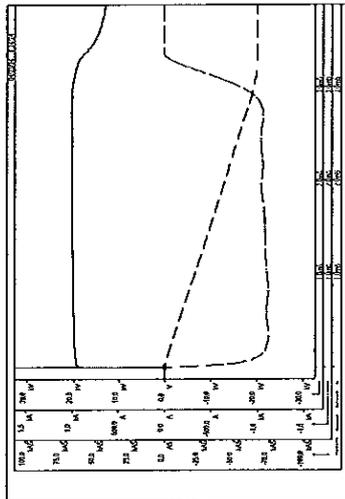
2nd application

Voltage: 20.71 kV

Current: 1064.0 kA

Energy : 66.65 kJ

Switching surge operating duty test  
Long duration current impulse  
Section No.8., rated 10.83 kVrms  
Time scale : 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale : 25.0 kJ/div



1st application  
Voltage: 20.35 kV  
Current: 1080.0 kA  
Energy : 66.68 kJ

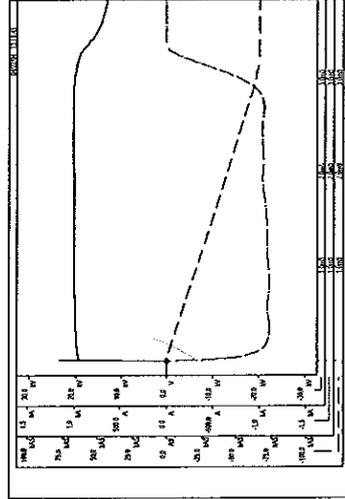
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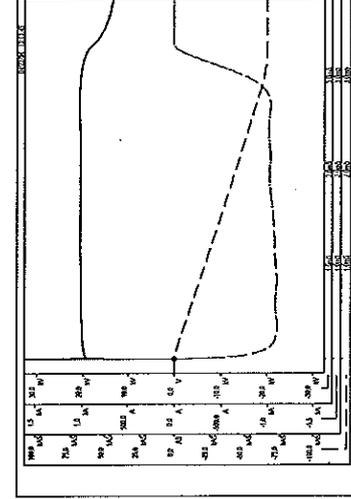
ВЯРНІЕ  
ОРИГІНАЛА



Switching surge operating duty test  
Long duration current impulse  
Section No.9., rated 10.83 kVrms  
Time scale : 1000.0  $\mu$ s/div  
Voltage scale: 10.0 kV/div  
Current scale: 500.0 A/div  
Energy scale : 25.0 kJ/div



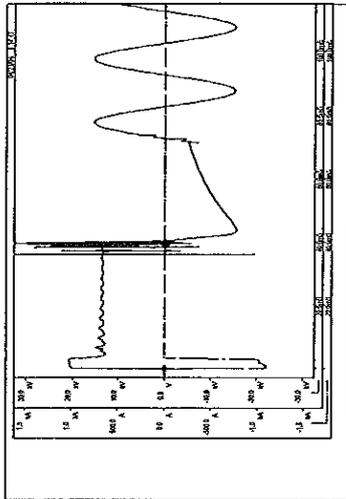
1st application  
Voltage: 20.43 kV  
Current: 1075.0 kA  
Energy: 66.55 kJ



2nd application  
Voltage: 20.78 kV  
Current: 1057.0 kA  
Energy: 66.26 kJ

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Switching surge operating duty test  
Section No.7., rated 10.83 kVrms



Second long duration current  
impulse followed by TOV

Time scale: 20.0 ms/div

Voltage scale: 10.0 kV/div

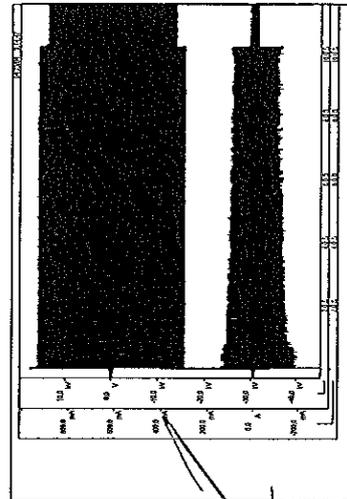
Current scale: 500.0 A/div

Temporary overvoltage  
(TOV)  
during 10 sec followed by  
0.87 x rated voltage.

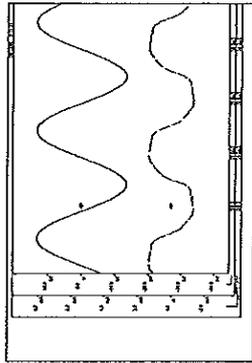
Time scale: 2.0 sec/div

Voltage scale: 10.0 kV/div  
(10.86 kVrms,  
9.53 kVrms)

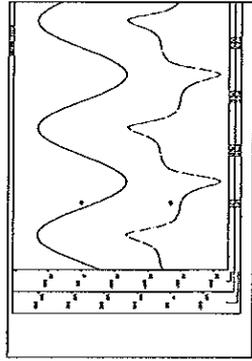
Current scale: 200.0 mA/div



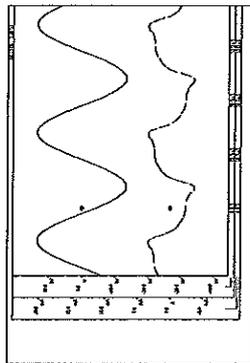
Switching surge operating duty test  
Leakage current measurements  
Power frequency voltage 9.53 kVrms  
Section No.7., rated 10.83 kVrms  
Time scale : 10.0 ms/div  
Voltage scale: 10.0 kV/div



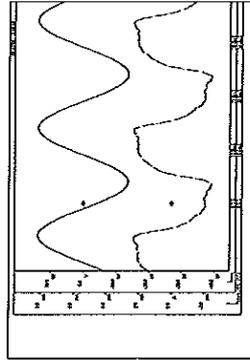
Current scale: 2.0 mA/div  
Before 1st discharge at 60.9 °C.



Current scale: 10.0 mA/div  
Immediately after 2nd discharge.



Current scale: 5.0 mA/div  
10 min after 2nd discharge.



Current scale: 2.0 mA/div  
30 min after 2nd discharge.

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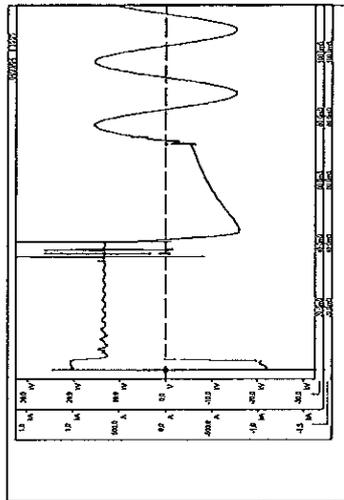
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ВЕРНО С  
ОРИГИНАЛА



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Switching surge operating duty test  
Section No.8., rated 10.83 kVrms



Second long duration current  
impulse followed by TOV

Time scale: 20.0 ms/div

Voltage scale: 10.0 kV/div

Current scale: 500.0 A/div

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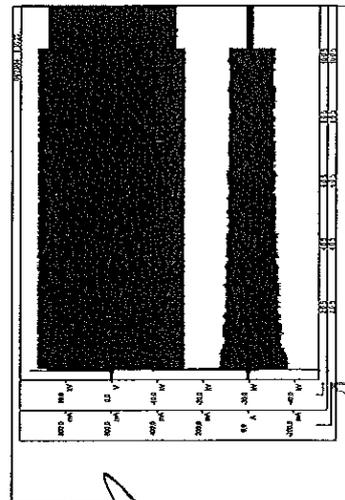
000243

Temporary overvoltage  
(TOV)  
during 10 sec followed by  
0.87 x rated voltage.

Time scale: 2.0 sec/div

Voltage scale: 10.0 kV/div  
(10.94 kVrms,  
9.62 kVrms)

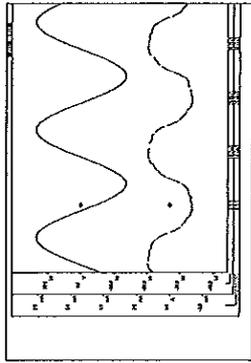
Current scale: 200.0 mA/div



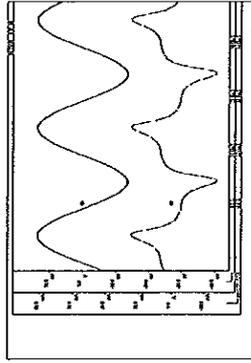
ВЕРНО С  
ОРИГИНАЛА



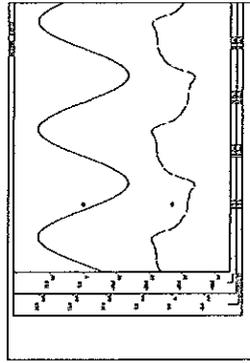
Switching surge operating duty test  
Leakage current measurements  
Power frequency voltage 9.62 kVrms  
Section No.8., rated 10.83 kVrms  
Time scale : 10.0 ms/div  
Voltage scale: 10.0 kV/div



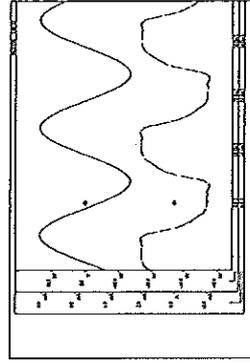
Current scale: 2.0 mA/div  
Before 1st discharge at 61.7 °C.



Current scale: 10.0 mA/div  
Immediately after 2nd discharge.



Current scale: 5.0 mA/div  
10 min after 2nd discharge.



Current scale: 2.0 mA/div  
30 min after 2nd discharge.

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